## DRAFT

# Bay Delta Drinking Water Quality Criteria

December, 1996

CALIFORNIA URBAN WATER AGENCIES

## Table of Contents

LETTER OF TRANSMITTAL
PREFACE
EXPERT PANEL LETTER
EXECUTIVE SUMMARY ES-
INTRODUCTION
POTENTIAL REGULATORY SCENARIO AND SCHEDULE
TREATMENT PROCESSES REQUIRED TO MEET FUTURE REGULATIONS
EVALUATION OF SOURCE WATER QUALITY AND TREATMENT EFFICIENCY 4-
REFERENCES
LIST OF TABLES  Table 2.1
APPENDIX A - Predictive Models for Disinfection By-Products
APPENDIX B - CUWA Member Treatment Data
APPENDIX C - Delta Water Quality and Treatment Limitations for Currently Available Advanced Water Treatment Technology

#### CC:

CUWA Board of Directors CUWA Water Quality Advisory Committee Elaine Archibald, Consultant Gary Bobker, The Bay Institute Thomas Clark, K C W D Ronnie Cohen, NRDC David Cottingham, Counselor David Fullerton, N H I Richard Golb, NCWA Robert Hultquist, DHS David Kennedy, DWR Gail Louis, EPA Steven Macaulay, State Water Contractors Bruce Mackler, EPA Felicia Marcus, EPA Dan Nelson, S L/D M W A Dante Nomellini, C D W A Erik Olson, NRDC Roger Patterson, USBR Jason Peltier, CVPWA Robert Perciasepe, US E P A Robert Potter, DWR Allen Short, MID Lester Snow, CALFED David Spath, D H S Phillip Wendt, DWR Rick Woodard, DWR Steven Yeager, DWR Thomas Zuckerman, Attorney

### Preface by California Urban Water Agencies

One objective of the CALFED Bay-Delta Program is to provide good water quality in Delta water diverted or exported to meet drinking water needs. To accomplish this, CALFED must select a long-term solution that provides a quality of source water that urban water providers can treat at reasonable cost to meet current and future federal and state health-based drinking water standards. To enable a quantitative assessment of the impact of alternative Bay-Delta solutions, specific water quality criteria must be chosen for analysis. Although there are numerous water quality constituents of concern in meeting drinking water standards, the major constituents of health concern in Delta water are pathogens (Giardia and Cryptosporidium) and disinfection by product (DBP) precursors (bromide and total organic carbon). The quality of water diverted from the Delta will bear heavily on the treatment technology which needs to be employed to meet increasingly stringent drinking water standards.

Setting water quality criteria requires knowledge about both the future regulatory setting under the Safe Drinking Water Act and the relative performance characteristics of currently available treatment technologies under a variety of actual conditions. Rather than asking its treatment experts to make this assessment, CUWA convened a panel of nationally recognized drinking water quality experts to determine the required criteria for total organic carbon (TOC) and bromide that will allow utilities treating Delta water to comply with current and probable future drinking water regulations utilizing available advanced technology. The expert panel consists of Douglas Owen, P.E. Vice President at Malcolm Pirnie, Inc., Phillippe Daniel, P.E. Associate at Camp Dresser & McKee and R. Scott Summers, PhD, Professor at the University of Cincinnati. The purpose of the expert panel report, which follows, is to identify Delta drinking water quality criteria based upon specified assumptions with which CALFED staff can evaluate the relative performance of Bay-Delta alternatives in meeting program objectives. These criteria have been developed in recognition of the interaction between source water quality, treatment efficacy and probable regulatory outcomes, as developed by the panel. This report does not represent CUWA's or any of its members endorsement of a specific regulatory outcome.

This report concludes that for currently available advanced water treatment technology to be able to meet probable future drinking water quality standards with water diverted from the Delta, the source water quality should have concentrations less than 3.0 mg/L for TOC and less than  $50\mu\text{g/L}$  for bromide. CUWA recognizes that based upon historic concentrations of these constituents measured at Clifton Court Forebay in the Delta, it is unlikely that the criteria for bromide could be met under existing conditions, even in wet years. Therefore, CALFED must carefully analyze a variety of actions within its alternatives analysis to determine which combination of actions can assure the achievement of the program's drinking water quality objective in concert with other important objectives. These actions should include at least the following:

#### **EXECUTIVE SUMMARY**

The California Urban Water Agencies (CUWA) retained the assistance of three water quality and treatment specialists who have specific expertise in the formation of disinfection by-products (DBPs). These three individuals -- the expert panel -- evaluated specific source water quality characteristics which would be necessary to permit diverted water from the San Francisco Bay/Sacramento-San Joaquin River Delta (Delta) to be used for meeting future water quality standards under defined treatment conditions. Specifically, the expert panel was charged with 1) developing an anticipated future regulatory scenario, 2) defining treatment criteria for coagulation and ozonation processes which potentially could be implemented by users of Delta water, and 3) estimating source water quality diverted from the Delta which would allow users implementing the defined treatment technologies to comply with the regulatory scenario. The source water quality characteristics were framed in the context of total organic carbon (TOC) and bromide concentrations, both constituents which have the potential to be controlled by different management strategies for the Delta.

The potential regulatory scenario includes specific limits for two organic classifications of DBPs recently proposed in rulemaking by EPA; 40  $\mu$ g/L for total trihalomethanes and 30  $\mu$ g/L for the sum of five haloacetic acids. In addition, a potential limit of 5  $\mu$ g/L was projected for bromate, an inorganic by-product formed by the ozonation of bromide-containing waters.

The treatment criteria specified by the expert panel included: 1) the use of 40 mg/L of alum at a pH of 7.0 and possibly as low as 6.5 in the coagulation process, followed by chlorine disinfection with a chloramine residual in the distribution system, and 2) the use of ozone at specific ozone:TOC ratios followed by a chloramine residual. The chlorine and ozone disinfection criteria were proposed to meet potential 1 or 2 log *Giardia* inactivation requirements. Only the ozone disinfection strategy was considered to provide potential 1 log *Cryptosporidium* inactivation.

The expert panel used data submitted by CUWA members, available literature and ongoing research, as well as their own experience and best professional judgement to arrive at potential source water quality requirements. Available models for DBP formation were evaluated to investigate threshold DBP formation behavior and to support the initial conclusions reached by the expert panel.

Specific combinations for TOC and bromide necessary in the water diverted from the Delta can vary depending upon the treatment technology implemented and microbiological inactivation required. Further, the conservatively plausible bromate level of 5 µg/L is significant in establishing limiting bromide levels in this evaluation. The rationale for this level in this analysis ultimately may be modified by a variety of factors including allowing for trade-offs for disinfection and the formation of organically-based brominated DBPs (e.g., THMs or HAAs) or evidence of a cancer threshold for bromate (investigations underway). On the other hand, there are other potential regulatory outcomes involving 1) the regulation of individual DBPs due to the potentially more severe health effects associated with brominated compounds, 2) the addition of other regulated haloacetic acids as analytical methods develop, and 3) the concerns over reproductive defects associated with DBPs, which may lower the regulatory levels and/or peak permissible concentrations.

#### 1.0 INTRODUCTION

The California Urban Water Agencies (CUWA) engaged the services of three water quality experts to assist in providing input to the CALFED process regarding potential management alternatives in the San Francisco Bay/Sacramento-San Joaquin River Delta (Delta). The expert panel was charged with determining the required raw water quality diverted from the Delta which would permit the effective implementation of specific drinking water treatment processes to meet potential future drinking water quality standards. The expert panel was comprised of Douglas M. Owen, P.E., Vice President at Malcolm Pirnie, Inc., Phillippe A. Daniel, P.E., Associate at Camp, Dresser & McKee, and R. Scott Summers, PhD, Professor at the University of Cincinnati.

The expert panel used data submitted by CUWA members, available literature and ongoing research, as well as their own experience and best professional judgement to arrive at potential source water quality requirements. Available models for DBP formation were evaluated to investigate threshold DBP formation behavior and to support the preliminary conclusions reached by the expert panel. This report presents the best professional judgement from this expert panel.

This report is subdivided into the following chapters:

Chapter 2 - Regulatory Scenario and Schedule

Chapter 3 - Treatment Processes to Meet Regulatory Requirements

Chapter 4 - Evaluation of Source Water Quality and Treatment Efficiency

In Chapter 2, the general trends in drinking water regulations are discussed and plausible, future regulatory criteria are presented. Treatment processes relevant to users of water diverted from the Delta are presented in Chapter 3, together with general assumptions regarding the design and application of these processes. In Chapter 4, source water quality is projected which allows the treatment processes defined in Chapter 3 to be used to meet the potential regulatory scenario presented in Chapter 2.

Other water quality contaminants, such as pesticides, herbicides, and metals, are of concern but are not likely to constrain treatment requirements as significantly as the microbial and DBP regulations, based upon occurrence in water currently diverted from the Delta.

There are other potential regulatory outcomes involving 1) the regulation of individual DBPs (rather than the groups of compounds represented by TTHM and HAA5 due to the potentially more severe health effects associated with brominated compounds, 2) the addition of other regulated HAAs (there are nine total) as analytical methods develop, and 3) the concerns over reproductive and developmental effects that may be associated with DBPs, which may lower the regulatory levels and/or the permissible peak concentration (i.e., annual averaging may no longer be the basis for determining compliance).

Further, because of the analytical difficulty in accurately characterizing microbial contamination in water, EPA is considering a treatment optimization rule, at least on an initial basis, as opposed to specific criteria for pathogenic organisms. In such a rule, "optimization" may be defined as an improvement in treatment process efficiency which minimizes the risk of microbial contamination in treated water sources.

While there are many factors that contribute to the uncertainty surrounding the anticpated regulatory scenario, it is the selected bromate level of 5  $\mu$ g/L that most keenly influences the analysis. The rationale for this level (i.e., advances in detection limit, the weight of the carcinogenic evidence, the precedence for THM and HAA5 limits in Stage 2 at half the Stage 1 levels) in this analysis could ultimately be modified by a variety of factors including:

- An allowance for disinfection bromate trade-offs (this is the World Health Organization rationale for a 25 μg/L standard). This may be critical if an inactivation requirement for *Cryptosporidium* emerges.
- A bromate versus brominated organic compound trade-off (i.e., addressing the difference between DBPs formed with ozone versus those formed with chlorine).
- Evidence of a cancer threshold for bromate (investigations underway).

Nevertheless, in the absence of more definitive direction, the panel considers a 5  $\mu$ g/L value to be both prudent and plausible.

For the purposes of this evaluation, the anticipated regulatory scenario summarized in Table 2.1 was used as the basis for evaluating source water quality and treatment requirements in this report:

TABLE 2.1
POTENTIAL REGULATORY SCENARIO

Regulation	Parameter	Treatment Requirement or MCL
ESWTR	Giardia	Additional 1 or 2 log inactivation by disinfection, after treatment removal credit
	Cryptosporidium	Additional 1 log inactivation by disinfection, after treatment removal credit
D/DBP Rule	TTHMs	40 μg/L
	HAA5	30 μg/L
	Bromate	5 μg/L

#### 2.2 REGULATORY SCHEDULE

The recently-enacted 1996 Amendments to the Safe Drinking Water Act (SDWA) have caused EPA to adopt a more ambitious schedule than EPA presented in June 1996 (see Table 2.2). The June 1996 dates were based upon a scenario in which EPA would not be "pushed" to develop an Interim ESWTR, and promulgate Stage 1 of the D/DBP Rule and the Interim ESWTR, until pathogen data were available from the Information Collection Rule (ICR).

TABLE 2.2

COMPARISON OF OLD AND NEW REGULATORY
SCHEDULE REGULATION

	Promulg	gation Date
Regulation	Initial (June 1996)	Revised (August 1996)
Interim ESWTR	June 2000	November 1998
Final ESWTR	NA (1)	November 2000
Stage 1 D/DBP Rule	June 2000	November 1998
Stage 2 D/DBP Rule	June 2003	May 2002

Notes: (1) NA = Not available

EPA understands, however, that the Final ESWTR and Stage 2 of the D/DBP Rule, at a minimum, are linked to data availability through the ICR. Monitoring for the 18-month ICR won't begin until February 1997. Consequently, EPA is pressed between the statutory requirements and the recognition that a longer time frame would be required [e.g., promulgation (final) Stage 1 of the D/DBP Rule and Interim ESWTR in 2000 with final and effective dates for Stage 2 in 2003 and 2006 to 2008, respectively]. One possible alternative for EPA is to proceed with interim regulations for microbial and DBP control (i.e., an ESWTR focusing on "optimization" and potential elements of the Stage 1 D/DBP Rule) that would be promulgated in November 1998. In any case, both the ESWTR and Stage 2 of the D/DBP Rule would ultimately need to be finalized and become effective by the dates given in the reauthorized SDWA (November 2000 and May 2002, respectively).

Given this projected time frame, it is anticipated that the selected option for management alternatives in the Delta will be known, with construction underway, by the time the entities using Delta water need to implement required treatment technologies. Consequently, these agencies will be in a position to plan for the projected water quality from the Delta "fix" in coordination with their efforts for facility modifications to meet the regulatory requirements of the final ESWTR and Stage 2 of the D/DBP Rule.

# 3.0 TREATMENT PROCESSES REQUIRED TO MEET FUTURE REGULATIONS

In this chapter, general process criteria are defined to characterize specific treatment processes relevant to users of water diverted from the Delta. Source water quality is determined in Chapter 4 which permits these treatment processes to meet the regulatory scenario discussed in Chapter 2.

#### 3.1 SELECTION OF TREATMENT PROCESSES TO BE EVALUATED

As a part of this effort, CUWA requested that the expert panel focus on those treatment processes which were considered to be the most cost-effective for simultaneously meeting the requirements of the D/DBP Rule and the ESWTR when treating water diverted from the Delta. These processes were defined as enhanced coagulation, a treatment technique proposed for Stage 1 of the D/DBP Rule, and ozone disinfection. These processes are also relevant for Stage 2 of the D/DBP Rule and were considered appropriate because they can be implemented into facilities currently owned and operated by the CUWA agencies (as well as a majority of conventional filtration facilities across the country). For example, the majority of filtration systems across the country use conventional treatment including sedimentation, which allows for increased coagulation dosages to meet proposed enhanced coagulation requirements. In addition, some CUWA facilities already use ozone disinfection. The most cost-effective option(s) for meeting potential future regulations is specific for each water purveyor, depending upon water source and quality.

There are entities which currently treat much higher quality water than that currently diverted from the Delta. These entities are able to use in-line filtration or simply disinfection without filtration to produce high quality drinking water. It should be emphasized that the determination of feasible treatment processes is dependent upon the existing source and that this evaluation is based only upon those entities currently using water diverted from the Delta as a source.

The use of post-filter granular activated carbon (GAC) adsorbers and membranes were not considered a part of this evaluation. The focus in this study was to define the source water quality needs for technologies currently applicable to large scale water treatment facilities in California. Post-filter GAC adsorbers and membranes can be at least an order of magnitude more expensive than

ozone and the feasibility of these technologies is much more uncertain based upon cost, environmental permitting constraints, and availability of residual handling alternatives. This position is shared by much of the water industry. For reference, only one treatment plant in the country at the size comparable to many of the CUWA members uses post-filter GAC as a treatment technique. There are no membrane plants in operation in the country which are used for DBP precursor removal at the facility sizes representative of the CUWA members.

It should be noted, however, that source water quality constraints from the Delta could be modified if GAC and membrane treatment ultimately were considered to be feasible treatment technologies.

#### 3.2 GENERAL ASSUMPTIONS FOR SELECTED TREATMENT PROCESSES

#### 3.2.1 Enhanced Coagulation

Enhanced coagulation offers the advantages of removing naturally-occurring organic material, thereby removing DBP precursors which, upon disinfection, form DBPs. As such, MCLs for TTHMs and HAA5 can be addressed by enhanced coagulation, when followed by chlorine disinfection. Upon review of the potential for DBP formation, it was determined that enhanced coagulation would only be required under conditions in which free chlorine is used for primary disinfection (pathogen inactivation), followed by chloramines for secondary disinfection to maintain a distribution system residual. Further, this treatment option is only applicable to instances in which either 1 or 2 log *Giardia* inactivation is required to demonstrate microbial control, as discussed in Chapter 2. It was assumed that *Cryptosporidium* inactivation could not be achieved by free chlorine disinfection under treatment conditions feasible for drinking water systems.

The conditions for enhanced coagulation were defined according to the specific percent removal requirements for Total Organic Carbon (TOC), as dictated in Stage 1 of the proposed D/DBP Rule (USEPA, 1994), by raw water TOC and alkalinity. Given the specific TOC removal percentages in the proposed D/DBP Rule, this translated to a projected 40 mg/L dosage of alum at a coagulation pH of 7.0, and possibly as low as 6.5. Consequently, acid addition may be required since the 40 mg/L dosage will likely only lower the pH to a value between 7.0 and 7.2. These coagulant dosages are not atypical of those currently being used by some CUWA members (e.g., Alameda County, Contra Costa, and Santa Clara Valley Water Districts), although 1) these systems

do not reduce pH with acid to improve precursor removal, and 2) many systems still prechlorinate, which cannot be used to obtain disinfection credit in the proposed D/DBP rule when using enhanced coagulation. It was assumed that a chlorine:TOC ratio of 1:1 and 60 minutes of free chlorine contact (t<sub>50</sub>) would be required to achieve 1 log inactivation of *Giardia*. For 2 log *Giardia* inactivation, 120 minutes of free chlorine contact would be required.

#### 3.2.2 Ozone Disinfection

The use of ozone disinfection offers the opportunity to meet the MCLs for TTHM and HAA5 in the potential regulatory scenario by again using chloramines as the secondary disinfectant. Therefore, additional removal of naturally-occurring organic matter may not be necessary. That is, enhanced coagulation may not have to be coupled with ozone disinfection, as long as the source water TOC is  $\leq 4.0$  mg/L and alkalinity is > 60 mg/L as CaCO<sub>3</sub>. Implementing ozone and chloramines under the Stage 1 timeframe to meet both Stage 1 and Stage 2 MCLs is one strategy for water utilities to avoid implementing enhanced coagulation when treating source waters with TOC concentrations  $\leq 4.0$  mg/L and alkalinity > 60 mg/L as CaCO<sub>3</sub>. Many entities using water diverted from the Delta, however, treat source water TOC concentrations > 4 mg/L.

For the purposes of evaluating bromate formation for 1 log *Giardia*, 2 log *Giardia*, and 1 log *Cryptosporidium* inactivation, ozone doses were projected based upon the expert panel's experience, current research, and data submitted by the CUWA members. The ratios were adjusted for pH effects (i.e., greater ozone residual persistence as pH decreases resulting in lower ozone requirements). For example, to meet 1 log *Giardia* inactivation at ambient pH, Alameda County Water District routinely requires an ozone to TOC ratio of 0.8 (ambient pH for entities using water diverted from the Delta can range from 7.5 to 9.5, a "typical" value of 7.8 was used in this analysis). At pH 7, MWD's demonstration plant results indicated roughly a 0.7 ozone:TOC ratio for achieving 2 log *Giardia* inactivation. Pilot results from the Santa Clara Valley Water District indicated that at pH 6.6 to 6.8, an ozone:TOC ratio of 0.7 to 0.9 was required for 1 log *Cryptosporidium* inactivation (the data were variable, however, and the lower pH did not necessarily correspond to lower ozone:TOC ratios for the pilot results).

Based upon the ozone dosage and inactivation data from the CUWA members and the expert panel's experience, possible ozone:TOC ratios which may be required to achieve pathogen inactivation were evaluated to take into account potential lower ozone dosages to achieve a given inactivation under conditions of lower TOC (for example, settled water ozonation). It is important to note that CT compliance needs to be achieved continuously, and therefore an approximate 20 percent safety factor was applied to the CUWA member data. This also partially accounts for EPA's approach in setting CT values based upon 90 percentile values versus median, or 50 percentile values which are represented by the CUWA member data. The selection of ozone:TOC ratios also considered operational issues, for which it was assumed that there would be a certain "overshoot" of specific dosage targets to ensure continual CT compliance. Based upon these assumptions, bromate formation was evaluated at a range of ozone:TOC ratios and pH values, as indicated in Table 3.1.

TABLE 3.1

OZONE:TOC RATIO AND PH CONDITIONS FOR BROMATE EVALUATION

рН	Ozone:TOC Ratios
7.8	0.8, 1.2, 1.5
7.2	0.7, 1.0, 1.3
6.8	0.6, 0.9, 1.1
6.5	0.5, 0.75, 1.0

The ozone:TOC ratios at each pH were considered to inactivate 1 log *Giardia*, 2 log *Giardia*, and 1 log *Cryptosporidium*.

# 4.0 EVALUATION OF SOURCE WATER QUALITY AND TREATMENT EFFICIENCY

#### 4.1 WATER QUALITY IMPACTS AND VARIABILITY

In this section, water quality constraints are described which will allow implementation of specific treatment processes to meet potential regulatory goals. In general, the water quality constraints will be described in terms of two measurable surrogate parameters which affect DBP formation; TOC and bromide. In evaluating these water quality variables and interpreting the results, it is important to recognize that:

- 1. TOC is a heterogeneous mixture, and is comprised of humic and fulvic acids and other naturally-occurring organic material which varies from source to source and from location to location within a source. Consequently, TOC from different regions of the Delta will not have an identical impact on DBP formation. In this effort, it was necessary to assume that TOC could be a unifying variable for organic DBP precursor material, even given the inherent variability in the material which comprises this parameter.
- 2. The extent to which bromide participates in DBP reactions is dependent upon its oxidation state as well as its relative concentration with other competing oxidants (e.g., chlorine). The following analysis is not stoichiometrically-based, but rather is empirical in nature based upon measured formation rates and other data available to the Panel.
- 3. The formation of DBPs is dependent upon many other water quality parameters beyond TOC and bromide, alone. Some of these include temperature and pH. The Panel focused on TOC and bromide because it was assumed that management alternatives for the Delta had the opportunity to affect these variables, and therefore their control will influence subsequent DBP formation through treatment processes.

#### 4.2 ENHANCED COAGULATION

For enhanced coagulation, source water TOC concentrations of 3, 4 and 5 mg/L and bromide concentrations of 50, 100, 150, 200 and 300  $\mu$ g/L were evaluated. As discussed in Chapter 3, an alum dose of 40 mg/L at a coagulation pH of 7.0, and possibly as low as 6.5, was projected to be required to meet the 30% TOC removal requirement for a raw water TOC of  $\leq$  4 mg/L and 35% TOC removal requirement for a raw water TOC of > 4 mg/L. These removals result in the treated water TOC values listed in Table 4.1. Using free chlorine as a disinfectant, a chlorine-to-TOC ratio

of 1:1 and contact times of 1 and 2 hours were projected to yield 1 and 2 log *Giardia* inactivation, respectively. To assist in assessing the TTHMs formed under these conditions, a THM formation model developed for the Metropolitan Water District of Southern California was used (Malcolm Pirnie Inc., 1993). The model was developed from 648 data observations under bench-scale conditions using various blends of water diverted from the Delta. The conditions used in this evaluation were within the experimental boundaries of the model. A more detailed description of the model is provided in Appendix A. The predicted TTHM values are summarized in Table 4.1.

TABLE 4.1

PROJECTED TTHM FORMATION USING ENHANCED COAGULATION

	Water Quality		TTHM Form	nation (μg/L)
Raw TOC (mg/L)	Treated TOC (mg/L)	Bromide (μg/L)	1 hr. contact	2 hr. contact
3	2.1	50	24	29
		100	27	32
		150	30	35
		200	32	38
		300	38	45
4	2.8	50	32	38
		100	35	42
		150	39	46
		200	42	50
		300	49	59
5	3.25	50	37	44
		100	40	48
		150	44	53
		200	48	57
		300	57	68

The TTHM values were compared to the data supplied by the CUWA members, those in the open literature, and with the experience of the expert panel. A summary of the data provided by the CUWA members is included in Appendix B. The available data and the expert panel's experience agreed well with values in Table 4.1.

HAAs are also formed under these reaction conditions. The Stage 2 proposed MCLs of 40 μg/L and 30 μg/L for TTHM and HAA5, respectively, yield a mass concentration TTHM-to-HAA5 ratio of 1:0.75. The DBP data supplied to the expert panel by the CUWA members indicate that the TTHM values exceed the HAA5 concentrations by greater than this ratio of 1:0.75 in 84% of the 160 cases where paired TTHM and HAA5 data were available. Other data from both research and full-scale applications in waters containing at least 50 μg/L of bromide confirm these findings (Summers, et. al., 1996, Cheng, et. al., 1995, Shukairy, et.al., 1994). Thus, it was concluded that TTHMs are the DBP of regulatory concern for this coagulation evaluation. It is important to note, however, that HAA5 represents only five of the nine bromo-chloro HAA compounds. If HAA6 or even HAA9 were to become regulated, then the controlling parameters and values could be affected.

A 20 percent safety factor on DBP production was used in determining the source water conditions which would result in the target DBP concentrations following treatment, thus a target value of 32  $\mu$ g/L was used for TTHM (80% of 40  $\mu$ g/L). Based upon this assumption, the following conclusions were drawn:

- 1) For a 1 log *Giardia* inactivation using free chlorine for 60 minutes following enhanced coagulation, it was projected that the following water quality conditions would permit compliance with the TTHM target concentrations in the regulatory scenario:
  - a raw water TOC concentration < 3.0 mg/L and a bromide concentration < 200 μg/L (0.20 mg/L)</li>
  - a raw water TOC concentration < 4.0 mg/L and a bromide concentration < 50  $\mu$ g/L (0.05 mg/L)

Certain combinations of raw TOC concentrations between 3 and 4 mg/L and bromide concentrations between 200  $\mu$ g/L and 50  $\mu$ g/L are also projected to meet the target DBP values.

For a 2 log *Giardia* inactivation using free chlorine for 120 minutes following enhanced coagulation, it was projected that a raw water TOC concentration < 3.0 mg/L and a bromide concentration < 100 µg/L (0.10 mg/L) would permit compliance with the TTHM target concentrations in the regulatory scenario.

#### 4.3 OZONATION

The formation of bromate by ozone has come into focus only recently and the ultimate MCL for this compound is of critical importance to facilities which have bromide in their source water and are currently using, or anticipating the use of, ozone for drinking water treatment. Even small concentrations of bromide (< 50 µg/L) can result in measurable concentrations of bromate after ozonation. Therefore, the Panel carefully evaluated available data from the CUWA members, other available literature, and ongoing research on bromate formation to evaluate potential source water constraints. Based upon these data, the expert panel arrived at initial conclusions regarding potential source water bromide concentrations which would be required to limit bromate formation within the potential regulatory scenario in Chapter 2.

Unfortunately, bromate formation is strongly dependent upon the nature of the experimental system design (e.g., bench versus pilot or full-scale). In addition, bromate formation depends upon ozone dosage and residual, which is often specific for full-scale facilities, making the direct comparison of these data difficult. Therefore, a bromate model (Ozekin, 1994) was utilized to systematically evaluate the impact of ozone dose, bromide, TOC and pH on the formation of bromate and thereby supplement the available literature (Shukairy et.al., 1994), data supplied by the Alameda County Water District, Contra Costa Water District, Santa Clara Valley Water District, and Metropolitan Water District of Southern California and the expert panel's experience. The model was developed from data from several source waters including water diverted from the Delta, including results from source waters containing bromide concentrations between 70 µg/L and 440 μg/L. A contact time of 12 minutes was chosen and the concentrations of TOC, bromide, ozone dose and pH were varied over representative ranges as discussed in Chapter 3. At each pH, three ozone: TOC ratios were estimated to provide the following levels of inactivation; 1 log Giardia, 2 log Giardia and 1 log Cryptosporidium. The dose of ozone estimated for these inactivations decreases with decreasing pH as a higher ozone residual is maintained at the lower pHs. The results of the modeling supported the initial conclusions reached by the Panel based upon the available literature and review of the CUWA data. A more detailed description of the model is provided in Appendix A.

Bromate formation is the limiting DBP (as opposed to TTHM and HAA5) for the ozone treatment and disinfection strategy specified in this evaluation. It is the opinion of the Panel that the controlling source water quality parameter for the formation of bromate, in the context of this evaluation, is bromide. It is recognized that higher concentrations of TOC will result in higher ozone dosages to achieve a given CT, and, as a result, may increase the concentration of bromate formed depending upon ozone residual, bromide concentration and potentially other parameters such as contactor design. Higher ozone dosages as a result of higher TOC also result in increased capital and operational costs for ozone treatment. Further, TOC can also be limiting to the extent that the biodegradable material, formed by the reaction between ozone and naturally-occuring organic mater (NOM), is not completely controlled through biofiltration, thereby creating an undesirable regrowth potential in the distribution system. The extent to which regrowth will be a problem is a function of the distribution system design, as well as disinfectant residuals maintained and other water quality parameters which are agency-specific. Nevertheless, sufficient data were not available to isolate the impact of TOC on bromate formation, in the absence of variation in bromide, pH and other water quality factors.

Based upon the data supplied by the CUWA members and other bromate formation studies and the model results, the expert panel concluded:

- 1) A bromate standard of 5 μg/L is very restrictive at pH values above 7. At pH 7.8 (ambient for some preozonated waters) it is projected that this standard will not be met and that a bromide level of 50 to possibly 100 μg/L would be needed to meet a bromate standard of 10 μg/L for 1 log *Giardia* inactivation.
- 2) If the ozonation pH were reduced to 6.8, then:
  - a 5  $\mu$ g/L level of bromate may be achievable with 1 log *Giardia* inactivation in the bromide range of 50 to possibly 150  $\mu$ g/L
  - a 10 μg/L level of bromate may be achievable with 2 log *Giardia* inactivation in the bromide range of 50 to 150 μg/L, or 1 log *Cryptosporidium* inactivation with a bromide concentration of 50 to possibly 100 μg/L.
- 3) It is projected that if the pH were depressed to 6.5, then a bromide concentration of 100 to possibly 150 μg/L could be accommodated while maintaining a bromate standard of 5 μg/L when achieving a 2 log *Giardia* inactivation. For 1 log *Cryptosporidium* inactivation, a maximum bromide concentration of 50 to possibly < 100 μg/L might be tolerated.

4) Limiting TOC concentrations were not estimated because of the limited availability and robustness of the data illustrating the impact of TOC on bromate formation, in the presence of bromide. It should be recognized, however, that higher TOC concentrations translate to higher ozone dosages to meet a given disinfection criterion and thereby can result in higher bromate formation. This is empirically validated in reviewing bromate formed during settled water ozonation as opposed to raw water ozonation. When TOC concentrations typically are lower at a given facility, ozone dosages to achieve a given disinfection requirement are lower, and measured bromate concentrations are lower. Lower pH in settled water also helps reduce bromate concentrations.

The expert panel recognizes that there are variations in bromate production data and therefore looked for indications relating to threshold behavior. That is, evaluating source water bromide concentrations which result in a clear increase in bromate concentrations for a given set of ozonation conditions. Given some variation in the formation of bromate reported at lower source water bromide concentrations ( $< 50 \mu g/L$ ), the expert panel took a position of plausible conservatism.

#### 4.3 SUMMARY

Table 4.2 summarizes projected source water quality requirements for TOC and bromide, depending upon the technology applied. In reviewing the values presented in this table, it is evident that there are various water quality constraints for TOC and bromide depending upon the technology used and the level of microbiological inactivation required. As stated previously, which technology is implemented is agency-specific, and is dependent upon a host of constraints related to cost, permitting issues and residual disposal. In some instances, lowering the ozonation pH with acid may not be feasible as a result of the inability to transport and store the chemicals necessary. Lower pH could also have an impact on the structural integrity of concrete basins, such as flocculation basins, sedimentation basins, and ozone contactors. On the other hand, ozonating at a pH of 7.0 to 7.2 may be possible without acid feed if settled water ozonation can be implemented. Existing plant hydraulic conditions and site issues affect this alternative.

TABLE 4.2
SUMMARY OF SOURCE WATER QUALITY CONSTRAINTS(1)

	M	IICROBIA	L INACT	TVATION	REQUIR	ED
TREATMENT SCENARIO /		<i>Giardia</i> ivation	_	<i>Giardia</i> ivation	Cryptos	Log <i>poridium</i> ivation
DISINFECTION STRATEGY	TOC (mg/L)	Bromide (μg/L)	TOC (mg/L)	Bromide (μg/L)	TOC (mg/L)	Bromide (μg/L)
Enhanced coagulation free	< 3.0 or	< 200 or				
chlorine/chloramines	< 4.0	< 50	< 3.0	< 100	N/A <sup>(2)</sup>	N/A <sup>(2)</sup>
Ozonation at pH 7.8 w/chloramines	N/E (4)	N/A <sup>(3)</sup>	N/E (4)	N/A <sup>(3)</sup>	N/E (4)	N/A <sup>(3)</sup>
Ozonation at pH 6.8 w/chloramines	N/E (4)	< 150	N/E (4)	< 50	N/E (4)	N/A <sup>(3)</sup>
Ozonation at pH 6.5 w/chloramines	N/E (4)	< 200 to 250	N/E (4)	<100 to 150	N/E (4)	< 50

Notes: 1.

- 1. Source water quality constraints are based upon achieving 40 μg/L of TTHM, 30 μg/L of HAA5, and 5 μg/L of bromate using the treatment and disinfection conditions presented in Chapter 3.
- 2. N/A = Not achievable. At this time, it is considered that free chlorine can not inactivate *Cryptosporidium* at dosages practical in water treatment.
- 3. N/A = Not achievable. Bromide concentrations would have to be considerably less than 50  $\mu$ g/L to achieve a bromate concentration of 5  $\mu$ g/L. Data to determine the necessary bromide concentration relevant to this study were not available.
- 4. N/E = Not estimated. Limiting TOC concentrations were not estimated because of the limited availability and robustness of the data illustrating the impact of TOC on bromate formation, in the presence of bromide. It should be recognized, however, that higher TOC concentrations translate to higher ozone dosages to meet a given disinfection criterion and thereby can result in higher bromate formation.

The Panel is also aware of the significance of bromate in establishing limiting bromide levels in this evaluation. There are many factors that contribute to the uncertainty surrounding the projected numbers, including relatively few studies which have evaluated bromate formation in low bromide waters ( $< 50 \,\mu g/L$ ), variations in treatment conditions which may reduce bromate formation (e.g., using both pre- and post-ozonation to reduce ozone dosages at any single location), and potentially lower CT values for ozone. It is the selected conservative (but plausible) level of 5  $\,\mu g/L$ , however, that most keenly influences the analysis. The rationale for this level (i.e., advances in detection limit, the weight of the carcinogenic evidence, the precedence for THM and HAA5 limits in Stage 2 at half the Stage 1 levels) in this analysis may be modified by a variety of factors including:

• An allowance for disinfection - bromate trade-offs (this is the World Health Organization rationale for a 25 μg/L standard). This may be critical if an inactivation requirement for

Cryptosporidium emerges.

- A bromate versus brominated organic compound trade-off (i.e., addressing the difference between DBPs formed with ozone versus those formed with chlorine).
- Evidence of a cancer threshold for bromate (investigations underway).

On the other hand, there are other potential regulatory outcomes involving 1) the regulation of individual DBPs (rather than the groups of compounds represented by TTHM and HAA5) due to the potentially more severe health effects associated with brominated compounds, 2) the addition of other regulated HAAs (there are nine total) as analytical methods develop, and 3) the concerns over reproductive defects associated with DBPs, which may lower the regulatory levels and/or peak permissible concentrations (i.e., annual averaging may no longer be the basis for determining compliance).

Given this understanding, if flexibility were provided to all agencies to implement any of the technologies evaluated in this study to meet the potential future regulatory scenario, then it is projected that a TOC of < 3.0 mg/L and a bromide of < 50 µg/L in water diverted from the Delta would be necessary. The TOC value is constrained by the formation of total trihalomethanes when using of enhanced coagulation for TOC removal and free chlorine to inactivate *Giardia*. The bromide value is contrained by the formation of bromate when using ozone to inactivate *Cryptosporidium*.

### REFERENCES

Cheng, R. C. et. al., 1995. "Enhanced Coagulation: A Preliminary Evaluation," *Journal AWWA*, 87:2:91 (February, 1995).

Malcolm Pirnie, Inc., 1993. Bay-Delta Water Quality Modeling, prepared for the Metropolitan Water District of Southern California, December 1993.

Ozekin, K., 1994. Modeling Bromate Formation During Ozonation and Assisting Its Control. PhD Thesis, University of Colorado, 1994.

Shukairy, H. M. et. al., 1994. "Bromide Impact on Disinfection By-Product Formation and Control: Part 1 Ozonation," *Journal AWWA*, 86:6:72 (June, 1994).

Summers, R.S. et. al., 1996. "Assessing DBP Yield: Uniform Formation Conditions," *Journal AWWA*, 88:6:80 (June 1996).

USEPA, 1994. National Primary Drinking Water Regulations; Disinfectants and Disinfection Byproducts; Proposed Rule. Fed. Reg., 59:145:38668 (July 29, 1994).

#### APPENDIX A

#### PREDICTIVE MODELS FOR DISINFECTION BY-PRODUCTS

#### A.1 THM PREDICTIVE EQUATIONS

Malcolm Pirnie, Inc. (1993) undertook a study on the formation of DBPs in chlorinated waters over a wide range of TOC and bromide concentrations for the Metropolitan Water District of Southern California. A 5 by 5 matrix of discrete samples containing incremental increases in TOC and bromide concentrations were prepared and evaluated. For this study, water was synthesized using low-TOC, low bromide Sacramento River water and high-TOC agricultural drainage water. High-bromide concentrations were achieved by adding sodium bromide.

The database used in this study, consisting of more than 900 observations, was constructed based upon the results of the source water quality monitoring program and the chlorination experiments from the 5 by 5 matrix. One portion of the database represented THM formation in jartreated waters and another portion represented THM formation in 0.45  $\mu$ m membrane filtered raw water.

Three sets of THM predictive equations were developed during this study using a non-linear power function format including total organic carbon (TOC), ultraviolet absorbance at 254 nm (UV-254), chlorine dose, bromide concentration, reaction time, temperature and pH as independent variables. The final TTHM predictive equation was based upon a portion of the database representing THM formation in 0.45 µm membrane filtered raw water (approximately 650 observations). Predictive capabilities of this equation was compared with THM formation in the jar-treated water (approximately 250 observations). The final TTHM equation developed was:

TTHM = 7.21 TOC<sup>0.004</sup> UV254<sup>0.534</sup> (C1DOSE-7.6\*NH<sub>3</sub>-N)<sup>0.224</sup> TIME<sup>0.255</sup> (Br+1)<sup>2.01</sup> (pH-2.6)<sup>0.719</sup> TEMP<sup>0.480</sup>
[
$$r^2 = 0.96$$
,  $F = 2010$ ,  $p < 0.001$ ]

This equation was developed at TOC concentrations ranging between 1.1 and 7.6 mg/L, bromide between 10 and 800  $\mu$ g/L, contact times between 1 and 48 hours, and chlorine doses between 1.0 to 16.4 mg/L. The values for UV-254 to be input into the TTHM equation were predicted using a relationship between TOC and UV-254 developed in the study as follows:

$$UV-254 = -0.0224 + (0.0374)(TOC)$$
$$(r^2 = 0.92)$$

Using free chlorine as a disinfectant, a chlorine-to-TOC ratio of 1:1 and contact times of 1 and 2 hours were projected to yield 1 and 2 log *Giardia* inactivation, respectively. A temperature of 20 °C and pH of 7 was also input to this equation to yield the values in Table 4.1 in the body of this report.

#### A.2 BROMATE PREDICTIVE EQUATION

The bromate model of Ozekin and Amy (Ozekin, 1994) was utilized to systematically evaluate the impact of ozone dose, bromide, DOC and pH on the formation of bromate. The model was developed from data from several source waters including waters diverted from the Delta. Source water bromide concentrations ranged between 70 and 440  $\mu$ g/L with bromate concentrations ranging between 2 and 314  $\mu$ g/L.

The model used has the following form:

$$BrO_3 = 1.63 \times 10^{-6} DOC^{-1.26} pH^{5.82} (O_3 dose)^{1.57} Br^{0.73} time^{0.28}$$

A contact time of 12 minutes was chosen and the concentrations of DOC, bromide, ozone dose and pH were varied over a representative range as input to the above equation. Temperature was held constant at 20 °C. The bromate formation results are shown in Table A.1.

It is important to note that the model was only used to support conclusions reached by the expert panel prior to using the model. The bromate model was evaluated to investigate threshold behavior regarding formation at specific levels and to support the initial conclusions reached by the expert panel. The results of the modeling should not be overemphasized. The results of the modeling supported the initial conclusions reached by the Panel based upon the available literature and review of the CUWA data.

TABLE A.1 PREDICTED BROMATE FORMATION

TOC	Br	O3:T	OC at p	H 7.8	O3:T	OC at p	H 7.2	O3:T	OC at p	H 6.8	O3:T	OC at p	H 6.5
(mg/L)	(µg/L)	0.8(1)	1.2(2)	1.5 <sup>(3)</sup>	0.7(1)	1(2)	1.3 <sup>(3)</sup>	0.6(1)	0.9(2)	1.1(3)	0.5(1)	0.75 <sup>(2)</sup>	1(3)
2	50	8	15	21	4	7	10	2	4	6	1	2	4
	100	13	24	34	7	11	17	4	7	10	2	4	6
	<b>15</b> 0	17	33	46	9	15	23	5	9	13	3	5	8
	200	21	40	57	11	19	29	6	12	16	4	7	10
2.5	50	8	16	22	4	7	11	2	4	6	1	3	4
	100	14	26	37	7	12	18	4	7	10	2	4	7
	150	18	35	50	9	16	25	5	10	14	3	6	9
	200	23	43	61	12	20	31	7	12	17	4	7	11
3	50	9	17	23	4	8	12	3	5	6	1	3	4
	100	15	27	39	7	13	20	4	8	11	2	5	7
	150	20	37	52	10	17	26	6	11	14	3	6	10
	200	24	46	65	12	21	2	7	13	18	4	8	12
4	50	10	18	26	5	, 9	13	3	5	7	2	3	5
	100	16	30	43	8	14	21	5	9	12	3	5	8
	150	21	40	57	11	19	29	6	12	16	4	7	10
	200	26	50	71	13	23	35	8	14	20	4	8	13

- Notes: 1. Ozone: TOC ratio anticipated to achieve 1 log Giardia inactivation.
  - 2. Ozone: TOC ratio anticipated to achieve 2 log Giardia inactivation.
  - 3. Ozone: TOC ratio anticipated to achieve 1 log Cryptosporidium inactivation.

#### APPENDIX B

#### **CUWA MEMBER TREATMENT DATA**

Data was provided by the CUWA members, including those resulting from the operation of their treatment facilities as well as bench and pilot studies. There are variations in these data which are unique to each treatment system. For example, some systems supplied data representing ozonation of only raw water, while others supplied data with both pre- and post-ozonation. The expert panel recognizes that there are unique aspects of process operation which can affect the ultimate formation of DBPs. For this study, however, the expert panel defined "unifying criteria" in Chapter 3 for enhanced coagulation and ozone which allow a comparison of these processes and a systematic method by which to evaluate the impact of water quality constraints on DBP formation. This appendix contains the data supplied by the CUWA members.

### bromate

·	1	<del></del>	1	<u> </u>	<del></del>		·
Carter Carte VVD				<del> </del>	<del> </del>		
Contra Costa WD		ļ	ļ	<del> </del>	ļ		ļ
Randall-Bold WTP				ļ	<del> </del>	<del> </del>	
					<del> </del>		
Sample	Bromate	Chloride	Bromide				
Date	(measured)		(estimated)				
	(µg/L)	(mg/L)	(mg/L)				
2/23/93	<0.5	72	0.22	1			
4/6/93	<1.4	89	0.27				
5/21/93	10	55	0.17				
6/15/93	6	30	<0.1				
8/18/93	6	25	<0.1				
10/5/93	10.3	60	0.18				
11/17/93	30.4	142	0.43				
1/4/94	1.5	70	0.21				
2/9/94	4.6	70	0.21				
3/1/94	2.6	<b>5</b> 5	0.17				
4/5/94	7.3	77	0.23				
5/10/94	<3	57	0.17				
7/12/94	<5	112	0.34	<del> </del>			
8/9/94	<5	133	0.4				
10/4/94	51	158	0.48				
10/10/94	33	118	0.36				
11/1/94	15	150	0.45				
12/6/94	13	162	0.49				
1/10/95	5.7	94	0.28				
2/14/95	17	60	0.18				
3/14/95	7.6	35	0.11				
4/4/95	18	105	0.32		<del>-</del>		
6/13/95	<5	40	0.12				
7/11/95	21	32	0.1				
8/8/95	7.8	32	0.1				
9/19/95	<5	16	<0.1		<u> </u>		
10/3/95	<5	14	<0.1			<del></del>	
11/7/95	<5	16	<0.1				· · · · · ·
12/12/95	<5	23	<0.1				
2/6/96	<5	40	0.12				
3/5/96	<del></del>	117	0.12				
3/3/90		117	0.35				
Note:	Ozone	dose	currently	optimized	for	coagulation,	
<u></u>	not	bromate	production.	Optimized	101	Coagulation,	
	1101	Divillale	production.	ļ	<del> </del>		
Conservative	07000	donos	nro 07	25255	(raw water		
Constivative	ozone	doses:	pre-ozone	2.5-3 ppm			
Plant CT energias	from 2 5		post-ozone	1ppm	(filtered)		<del></del>
Plant CT operating	ווטווו ב-5	<u> </u>	1	<u>!</u>	1	<u> </u>	<u> </u>

-	_						96/E/9	6/8/	4/1/96	14/96	2/5/96	/8/96	12/4/95	1695	0/2/95	11/95	8/7/95	7/10/95					Date:		ATER C			1		Source water ID:	Z. Source Water.			Study ID:	Othery ID:
-																				-			Time	_	WATER QUALITY DATA: CONVENTIONAL+OZONE		_		-	aler D.	74181.	1		-	-
							=		7,8	5-1	80	5	u	2.8	u	7.7	36	57		<del>-</del>	Raw				DATA:		E	5.	1	+	<del> </del>	1	+	1	+
2	Se	F	力量を	8	Note: For	_	_		_	<u> </u>		L		L	H						Setti.	(mg/L)	100		CONVE		dicate w	Describe	_	Cent	-\	-	-	Histor	-
	# - App	Fill = Post-oz	W = Pre-02	CCWD's Randalf-Bold WTP has pre & post ozone and direct litration.	Note: Form is set up for conventional filtration and intermediate ozone.		_	L			<u> </u>		L		L		-	<u> </u>						_	NOITH		(Indicate with an 'X')	5. Describe level of study:	_	Central Valley Project Water	-	Della (Rock Slough)	4	Historical data 7/1/95-6/30/96	
	ed.	20	20.	ndall-Bold	ip for con	_	-	-		1	l T		<u> </u>	  -	_				-		Fill. Raw			_	AL+OZ	-		itudy:	4	Project V	_	South	-	7/1/95-6/	-
the circle			<u> </u>	WIPha	ventional	L	-		-		-					T			-		Seitt.		-	_	SNE	×				aler	$\dashv$		-	96/0	-
-	-	-	-	s pre & p	filtration		-			<del> </del> -	T	-		-			<u> </u> 	$\mid$			l. Ozon.	1/cm)	UV-254	-		Full-scale	Pilot-scale	Bench		(State	- <u> </u>	River	_	(Q)	1
done site				osi ozona	and interr						Ī		Ī				Ī				F#	-				Calle Re	cale	Bench-scale		Project w		ake gro		izalion S	
3				and dire	nediale o		1	69	2	ē		62	55	_52	5	3	18	3/			Ra₩									(State Project water, blend of,		(River, lake, groundwater, etc.)		(Optimization Study 8/95, etc.	
מים היסר				ct filtratio	zone.																Sei E	- 100	Alkalinity							nd ofe	]	흕		er.	
N/A and applicable (chloringling is only done after post-ozone process (after likration)				٩							į					-	-				Ozon.	Caco3	linity			L				<u>ब</u> (त.)					
							25	2	2	2	4	à	35	2	2	à	2	2			F.			L									sources and proportions:	4. If blended source water indicate	
_							10/	130	67.1	1	1 5	1	57	18	9	9	1 2	1		Raw												Soc	and prop	ded sour	
																	-			Settl.	7											Source	actions:	ce water	
																-				Ozon.	Total													Indicate	
i		Ī					8	135	1	10	18	3	55	2	200	18	1			Filt		ing/Las	Hard								1	24			
	-			İ	-	-	İ	T				İ		<del> </del> -	-	ĺ		Ì	r	Raw	 	mp/L as CaCO3)	Hardness	-		<u> </u>					1	1			
	İ	Ī	<del> </del>		Ī	İ	İ	<u>;</u>	İ	İ	Ť	Ī		-	-	İ	İ	T		Se				-		-					T	1			İ
							T				Ī	Ī		Ī	Ī	Ī	Ī	Ī		Ozon.	Calcium										1	1			Ī
		İ	ľ				İ	ĺ			T	İ		Ī		İ	ĺ		T	뀵				-	Ī						İ	Ī			1
							0.12	0 22	ê	0.31	0 12	â	8	ê	â	ê	ê	â		-	ŧ														
	_					L	L			L							L				Sein		Bromide								$\perp$				1
						_		-	0								  a			_	Ozon.	٦	de						4	_	$\downarrow$	1	-		4
1	_					_	â ^	i-	i -	0.16	Ť	├-	-	ê.	<del> </del>	r	t	-		-	Fig.				_				-	1	$\frac{1}{1}$	1		-	+
1						_	<u>.</u>	0.15	ê	â	<u>.</u>	â	0.15	<u>-</u>	12	2	A	=			Raw			_				-	-	-	+	-	_	+	+
1	_								-	L	<u> </u>					L				-+	5 E	mg NH3-MC)	Ammonia				_	+	-	-	+	1	-	1	+
-	_				-	_				L										+	4	Š	1	4			_	4		1	+	1	1	4	1
-	-		-		-	_	0.45		0.40	041	0.51	0.46	0.41	0.33	0.45	0.32	0.26	0.35		+	7	-	-			_	-	1	1	-	1	-	-	_	1
1		1			-	4	25	g	70	92	42	26	5	7	5	8	12	35			P					-		1	1	-	1	1	1	1	1
																					ر ا	3													

	1							L	0000	3	56/96	4/1/96	Seren	2	2/5/96	1/8/96	12/4/95	176/93	0.00	20.00	201102	87795	7/10/95	L					Dale		WATER						3. Source		Z. Source		1. Study		Utility ID:
																										Ozon.	145		rid.					Ī	T						_		
									1	77	63		1		2	ដ	21	21				≅	ಸ			1	!		-						T	1	Ì			_		_	
		Ī			Ī	Ī			2	3	250	280	į	3 1	ğ	140	8	8	5	3 2	1	6	8		T	ZEV	1	$\dagger$	1		_		l	l	$\dagger$	t	1	1				_	_
									Ī	1			T	Ì					Ì	Ì					l					7			r	_	-	$\dagger$	+	1				_	
													Ī	1						T	1		_			Uzon.	mg/L/		TOS			-		T			1	1					
									ě		ğ	330	2	1	ş	180	130	120	Š	2	3	=	110	_		Ĩ.								T									
L			1			-		_	8.00											,		-	8.68			Raw										T	1				1		
L	-	1	1			ļ			2		5	8	0.73		775	820	2.79	4.46	è	-		-	8.78			Settl. Ozon.	2	100								I							
L	+	-	1	_		-	-					_	0				0	0				211		_		Ozon.	S	9									1		1				
L	-	1	+	_				_		1	- 1			t		- 6	- 1		1	0.025	7	_	_			₽	_		1	1					_	-	1	1	1		1	4	
L		+	1	-				_		+	,	_	-	÷	+	-+	-+	_	-	1.5	÷	÷	4	_	_	Raw				1			_	L	_	_	1	1					
_			1	-		L	1		- 29	0		724	. 14	-		<u> </u>	7.46	7.21	7.25	=	12	71	2		_	Sent.	=	PH	-														
	_	-	1	-		L	-	-			1					1				L	L		1	_		Ozon.																	
_				1					7.18											681			6			F.															T		
									23.5	21.0	6	2	ô	1	2		5	80	22.7	23.7	25.2	1				Raw					1							ĺ					
										_					ĺ											5	Q.	Temp										Ī	Ī	T		1	1
																										Settl. Ozon.	0	ature.			Ì	Ť					İ	İ	T	T	T		
				L				100	3	210	0	1	120	12.8	120	10	3	3	220	230	250	23 9				2					T	1	1	j	j				T	1	T	t	
															_			1			_					20													Ī		Ī	İ	
-		.	_		1			-	-						_	L			1	1			L		1	200															I		
+	+	1	_		-	1			1	-	_		1	-	_		-	1	1	1		_	L		0,011								1	1	1				L				
-	1	1				1		ô	1	1	ŝ	٥	1	1	ŝ	۵	Ĝ	٥	Ť	3	÷			t				1					L										
	1	1	4			1		28	1	3	8	â	1	3	2	5	â	=		1 5	2	-																i					
	+	1	1					_	L		1		L	1				-			1		Seni	(#/100	Total																		
L	L	1	1		L			_		1		_	L	L	1				L				Ozen.	1	2																		
			1			L		-	0	6	1	•	0	-	ŀ	-	0	0	0	-		-			_	Co.																	
		L	L			L	ľ		6		1	-	u	-		-	~	J.	<b>GB</b>	9	-	,				Colforns																	
																						9		1	_												T	1		1	1	1	
															Ī	Ī						OXON.		100	2					1						İ		T	1	1	Ť	1	
					İ							Ī				Ī	1					ī	1					_	T	1	1	†				-		T	1	+	$\dagger$		
		ĺ			1		_	-	•	-	-	1		-		1	1	+	1	0	_	-	May	-	1	-	-	-	H	1	$\dagger$	$\dagger$	1		-		-	L	1	1		-	
	1				T	1			T	1		Ì	İ	1			İ	1	Ť	+			·	15,51			-	1		1	1	+	+	+	+	_	-		-	L	1	1	

						Der Pa	2000	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	2	2000	1/0/90	CENT	11/0/93	ER/Z/MI	CR/11/6	0///90	CENT					UNITED			WATER				3, 00010		7.000		i. utury	2	Utility ID:	
				Ī					Ī	1				T	T		T	T	Ozon.	1001		1														
	T	T			T		1,	-	3		,		,	T	T	Ī	١	7	7	~		10014								Ī						
			T	1		Ì	,	٥	3		4		1	1		1	-	1	1	B		March Contact of the	1				Ī									-
	T	1	1		1			1		1			1		1	1		1	1	2	(pocys															
		T	1															1		Satil Ozon	2	Crypto.														
	Ť	1						٥	-			0	-					0		=																1
H	1	1	Ť			1						1	1							R.																
П	1	1	Ì												1					Settl. Ozon.	1	Ϋ́														
П																				Ozon.	(Amil.)	Viruses														
																				F					L											
							2950	130	510	290	880	520	3	1350	510	290	880	2100		RJW			!													
	1																			Se iii	CF.	Ŧ			ĺ										Ī	
	1	1	1							Ì										Selil. Ozon.	PmC.	HPC				Ì										
							2	0	-	0	0	2	-	0	0	u	•	-		Filt.						Ī	Ī									٦
H	1	-	_			-			ĺ	İ			_	_					chlorine	e	Indic					Ī			Ī							1
	_		j	L			_	L		-	L	-				L		L	rine c	sed with	ate disini			F	L	1	-	-	-	-			-	-		_
							×	×	×	×	×	×	×	×	×	×	×	×	chloramine	used with an 'X'	ectant(s)			-												
							1.48	1 39		1 99	1.92	1.82	1.76	1.71	1.78	1.05			(mg CI2/L	dose	Chlorine															
		-	_		-		1	-		t	-	-	-		-	-	-	_	7		-			-	+	+		-			-	-	+	-		
							0.49	0.47	0.04	0.65	0.67	068	0.58	8	060	0 55			NEID-MIL)	dose	Ammonia	2	Chlorinatio													
																			chiorine		ncubub	lered	Chlorination conditions													
							1.4	6 13	20.3	200	32.5	32.5	27.1	20.3	27.1	21.7	3.97	3.07	chloramine	=	incububation time															
H	-						22.2	20.5	0.0	12.5	12.2	12.5	15.8	=	23.8	25	23.2	22	=	-	incub.			-	T	1	$\dagger$	T								
	1	-				-	Ļ	╀	+	0	┝	Ļ	-	-	841	-	9.00	Ļ	├-		모	ĺ		-	1	+	+	-		-	+		$\dagger$	-		
H	1			-			1.19		Ĺ	1.08		Γ	-	-	T	T	0.97	-	3		Residual	₹.			-	$\dagger$	1						1			
$\mathbb{H}$	4	-	-	L	L	_		L		F	<u> </u>		Ĺ	Ĺ	<u> </u>	-	<u> </u>		Ē	-	<del>-</del> -	<u> </u>		-	-	+	-		-	H	-	-	1			-
$\mathbb{H}$	-	-	_	L		_	L	-	-	1		-	_	L	_			L	-	Raw				-	-	1	-	L	H	L	-	-	<u> </u>	+	-	-
H	4	-		L		_	_		L	+	L			L	L	-			-	Selli, Ozon.	100	큪		-	-	-	1	-	L	-	-	-	1	_	H	_
H	4	-	-	_	L	L	1	1	1	0	٥	1	٨	0	اوا	^	4	-	-	9				-	-	+	L	-	-	-	-	-	-	-	Н	
Ц	1	1					ŝ	100	U	â	0.5	3	S	ŝ	S	â	<b>60.5</b>	0.9		F				L	1	1	1		L				1	1		

							6V3/96	5/6/96	411/96	3/4/96	2/5/96	1/8/96	12/4/95	11/8/95	10/2/95	9/11/95	87795	7/10/95					Date		WATER					3. Source		2. Source		1. Study	Ottotty to	
																				Raw		ľ														
																				Setti	ў <del>ц</del> )	7														-
																				Ozon.	hô/L)	HAA5														,
																				F			mection											П	T	1
																				Raw			Disinfaction By-products												1	_
																				Sett	-	Ŧ	ducts	_											T	_
															Γ		Γ			Ozon.	(Ma/C)	2										П			1	_
							۵	2.5	15.6	۵	۵	2	1	۵	Δ	5	۵	۵	T	Fig.												_	<u></u>		1	-
					Γ		İ				Ī	-			Ī	İ	ĺ		Ī	Raw		İ		r		Ī	Ī							П	1	-
		İ			T		T	Ť	T		T			T	T			-			1			r	-	-					l	-			+	-
_			-	İ		T			T	Ī	İ	İ		-		Ì	<u> </u>	İ	-	Ozon.	(pg CI-AL)	X		r	<del> -</del>				_		l	r	H	H	†	-
		-		l	-		<del> </del> -				-	İ			ĺ		İ			=	7			r			-			-	-	H			$\dagger$	-
						r	1/2/3	1/2/3	1/2/3	1/2/	1/2/3	1/2/	1/2/	1/2/	1/2/	1/2/	1/2/	1/2/3		(See above	-	Coagulant		l	TREAT						İ	Indicate	-		1	-
_	_			L	_	-	_		L	٠.								L	-	a d	<u> </u>	in in		L	MEN	L	-	<u></u>	~	<u> </u>	Ö	coagu	L	H	4	_
							27 / 0.48/0.0	40 / 0 50 /0.0	5 5/0.93/0.1	77 9/3 0/0 49	8/1.0/0.2	7/1.0/0 2	0 0/20 1/8 &	\$103.00	7/12/00	/1.0/00	35/1.0/0.1					Dose	Coage		TREATMENT CONDITIONS			Non-Jonic	Cat Poly	Aum	Coagulant	indicate coagulants studied:				
							z	z	z			1					z	2		(Y/N)	adjusted?	Acid	Coagulation Conditions		SNOIT						Chemic					
							z	z	z	z	z	z	z	z	z	z	z	z		(YAY)	adjusted?	Base	llions								Chemical formula					-
		-					7.98	68	7.24	7.12	7.12	7.05	746	721	7.25	7	721	6/4			PH		1				-		-		Units				7	_
1						<u> </u>	23 5	210	16.8	14.0	140	13.0	16.5	180	22.7	23.7	25.2	24.1		(deg. C)	_	Coag										_			+	_
			-			-	1.53/0													(mg/L)		Ozo	-	Pre/Po									<u> </u>	$\frac{1}{1}$	+	_
_					-	_	0.4 26/.13/.1	0.4 36/24/2	54 23/1	19/0	7.4 26/10	0.3 12/.04	14 10	0.3 16/0	29 .07/.0.	03 06/0	25/05 34/27/3	36/23/3	-	[] [mg/L]		Ozone		=	Stages	Post-Ozona								H	-	_
1				_	L	L	i -		l		ì	ı	1		ı	ı	i	1	ì	1	_		Ozonation Conditions	1773 St	Т	ZONS				_			-		+	_
1	_						3.40 7	3.74 6		21.39 7			12.48 7	<u> </u>	-	-	<u> </u>	1	ı	3	time	Contact 0	Conditio	Stage	Per							Ц	L		+	_
	_			-			7.18		7.36	Н	7.04	-			-	-	_	731	-	0	_	_						_					L		$\frac{1}{1}$	_
							23.5	210	16.0	13,0	12.8	12.0	15.2	21.5	23.0	250	23.9	162		(deg. C)	temp.	Ozome											:			

•	1	ľ	Ľ	•	Hole		5	ŝ	*	ŝ	Š	8	5	1	3	3	3	35	3	56.00	Š	Š	3	ž	ž	8	ş	3	ž	ş	2			Š	11/93	3	16493	VI 593	21/93	Š	ž	1	ļ	1	200	L	TER	Ĺ		L	L	ource		Source water.	Study I	Ļ	-
13				CCMO	M R MAN								-										Ì			-						1													200	1	OUAL					Source water ID:		3	ä		1
1			7	Randa	el car lor	- 	=		2	5			١.	1	,	‡	1	10											1	7	†	1	†	t	1	t	T	H			1	1	1	179	÷	+-	1	1	t	t	T	9	1	†	t	T	-
-	FL S	†	Pade a Prade	L Boid Y	118/1/02	H	Н	8	-	Ť	İ	Ť	†	t	Ť	6 8	۲	Ť	t	ğ	2	8	2	77	77	75	74	ş	72	_	8	24 8	2 2	3 8	2 2	2	8	12	Z	8	70	+	3	+	+	1	WATER QUALITY DATA: CONVENTIONAL+020NE	1	DOG.		+	Н	Π	$\dagger$	$\dagger$	-	
		+	+	I P Nas	oral Bo	┝		_		F	Ì	T	1	+	1	T	1		+	ľ	l		_	Ц						+		1	1	+	1	T T	F	-				+				}	3480	-	NA BEE	b. Describe level of study.	1	Cersira	Н	9	1	-	-
	1	+	ļ	2 2 2	ation ar	-		L	H	l	+	+	+	+	+	+	+	+	+	L	L	L	H			L		Ц			-	+	1	+	+	H	Ļ	H	H			+	1	0.20		-	OIL	1	3	3	<u>.</u>	Yalkay h	Н	3	- 8	-	_
		4	+	UD ZO	D Trees	L		L	L	ļ	1	1	+	1	+	-	1	1	-	Ļ		Ļ	L	L	L	L		Ц	Ц		-	4	4	+	+	-	ļ	Ļ		L	Ц		-			\	2	-	ļ	1	Ł	Central Valley Project While	Н	Della (Reck Struct)	Haderical Gate // Inco-pourse	-	
	8	1	+	9	A CHANG	-	+	H	┾	÷	+	÷	÷	+	+	3	+	┿	┿	-	L	_		_		L			L	Ц	_	1	1	+	1	1	-	-	Ľ			Н	÷		+	+	100		+	+	+	valer.	Н	3	- 8	-	_
	3	+	+	Total Control	Ž	-	5	ō	1	1	3 3	8 .	2	5	8	2 3	2 1	4		8	18	=	18	×	9	8	2	3	8	5	×	8	81	= 1	3 2	3 8	-	2	ž	77	123		S.			-	+	1	1	910		G	Ц		1	1	
	2	4	+	100		l	ļ	<u> </u>	1	<u> </u>	1	1	+	1	+	+	+	+	+	$\downarrow$	H	H	L	L	L	L	L	L	_		Ц	4	4	+	+	+	1	ŀ	L	<u> </u>	Ц		\$ and C	E A		-	1	-		a series	-	ata Pro	Н	River, but	-	-	_
	1	1	+	+	1	1	1	1		<u> </u>	1	+	1	+	1	1	1	+	+	1	1		L		L	L		-				1	-	+	-	+	+	T	ļ	-			029	إ		•	+	_	-	1	+	State Project water, blend of	L	Mar Brown	Constitution of the Parish		_
	3	4	1	1	+	1	8	+	÷	÷	÷	÷	+	4	- t	8	- 1	ı												٠.,	_	8			+	+	+-	÷	8	╌	-	∺	ž.	1	1	1	ļ	-	San Grander	1	1	, pier	L	1	-		
		1	1	1		ļ	2	22.0	É	1	1	3	4	<u>a </u>	a	٩	à !	2	1	2		810	3	3	à	×	ŝ	2	5	017	0 23	017	21	021	ľ		1	S A	2	027	ä		-	Ĩ			ļ	1		1	1			8		-	_
						1				1						-											L	L											L					2			1					ě	1				
			-											-			-																	-										9							İ						
١							å	0 19				2	â	ė,	4	al.	à	a e	3	Ī	Ī		Ī	Ī										1	T		T	Ī			Ī			Ä		ľ		Ī	Ī		T	Ī	Γ		T	Ī	
1		i	İ	t	i	1	la	1010								â			+	į.	7100		00	00	00		0	0012	0024				0	8	0		1		002		984		1	F	Ť	†	t	†	i	t	†	$\dagger$	T	H	Ť	T	-
1	-	4	1	1	<u> </u>	+	1-	1	1	1	1	1	7	7	7	-	1	<del>-</del>	<u>-</u> T	÷	15	T	1	Ī	1	7	12	12	~	-			~	24	ا <del>ت</del> ا	T	1	12	12	1	7	Н				ŀ	+	+	1	1	+	+	Ļ		+	+	_
1	_		1	1	ļ	1	L	1	1	1	Ì	1	-		-	1	-	1	1	1	1	-	_	-	L	L	L	L		L				1	1	1	ļ	1	ļ	L	Ļ			Sekil Ozon.	1	Amon	1	1		1	1	ļ	ļ		1	1	
1				1					1		1						1																									Ì		Ozon.	4							l				1	
1	ĺ			Ţ	Ī		å	1	10	5		9	4	2	2	al	2	۱۱ ۱۱	ž.		89/3		0 3/8	24	2	0	8	10	041			0 427	9	0	20	1			2	Q 232	2			¥			Ī				Ī						
					ĺ	Ī	×	18	1	3	3	اه	2	23	ä	=		3	518	3 8	b	8	1	162	8	ī	S	ž	112	SZ	77	x	3	a	į	5 8	3 2	18	8	8	z			A S	T	Ī	T	T			Ī	T			Ī		•
Ì	Ì	1	i	Ť	Ť	Ī	Ť	İ	İ	Ť	1	Ī	1	٦	1	1	T	Ť	Ť	Ť	Ī	1	Ī	T	T	Ī	T	Ì	İ			Ì	j	i	Ť	Ì	Ť	Ť	Ť	T	T	Ιİ			1		Ť	Ť	1	Ť	Ť	Ť	T		Ť		-
1	1	7	1	+	1	†	-		Ì	t	+	+	+	1	1	+	+	i	+	t	t	t	H			-	i	-	- 	-	H	-	1	1	1	+	†	t	╁	<u> </u>	-	1	-	Sent Ozon		-	t	+	+	+	†	$\dagger$	╁		+		-
1	1	+	1	1	+	t	1	2	+	+	-	-	님:	2	7	-	1	1	1	Ť	t	ļ	ŀ	-	<u> </u>	L	F	┝	L	-			-	+	+	+	T	÷	╁	<u> </u> 	-			3		-	+	+	+	+	+	+	H	Н	+	+	•
1	-	-	$\frac{1}{1}$	Ì	1	1	÷	÷	÷	Ť	÷	7	÷	Ť	-+	8	+	+	+	1	+	1	-	-	<u>!</u>	-	<u>l</u>	L	-	-		-	-	+	1	+	+	+	t	-	H			7	1	+	t	t	1	+	t	÷	┞	Н	+	+	
1	1	+	+	1	+	-	10	10	1	1	1	-	0	<u>의</u>	7	1	1	1	T	1	+	t	-	-	-	Ļ	-	H	<u>L</u>	Ļ			-	1	+	$^{+}$	+	÷	1	1	-			\$ 50m		ŀ	+	+	+	+	+	+	╀	11	i	1	-
t	+	1	$^{+}$	1	+	t	$^{+}$	I	Ť	<u> </u>	+	+	+	+	+	+	+	+	+	t	1	ł	-	H	-	ŀ	<u> </u>	-	L	<u> </u>			7	1	+	$\frac{1}{1}$	+	t	+	-	-	Н		⊒ 029			+	+	1	+	누	+	t		+	+	
-	+	1	+	+	t	ŀ	<u> </u>	×		1	e i	y.	+	_  	1	-		Ì.	<u>+</u>	İ	1	-	İ	1	<u> </u>	<u> </u>	<del>,</del> T		-	-		-	+	+	t	+	1	1	+	t	H	H		7		-	t	t	1	+	t	$\dagger$	<u>_</u>		+	t	-
1	1	4	+	+	1	1	1	<u>.</u>	╁	┿	+	÷	+	+	-+	3	+	+	÷	1	ļ	Ļ	<u> </u>	<u> </u>	L	H	<u> </u>	_	H				4	1	1	ļ	+	1	_	<u> </u>	L	H	4	¥	1	+	+	$\frac{1}{1}$	1	1	+	+	H	Н	+	+	
-	-	1	1	1	1	ļ	8	×	3	8	ļ	X	S S	ě	č	8	Ġ		ŀ	12	i s	ő	1	2	213	6	0		8	à	26	3	3	27	*		3	15	12	5	5	Ц		2		-	$\downarrow$	ļ	1	1	1	ļ	Ļ		1	-	
		1				L	57	8	18		i	XI.	8	ž	*	8	-	-		295	12	z	-	30	26	1	2	1 97	7	415	=	5	5		اد	200	1	16 12	ŭ	122	215		-	ž,			l			1							
	İ											1											ĺ											1	Ţ		I						i	P 020			Ī	T			T				T		
Ī	1	Ì	Ť	ľ	T	T	900	001	9	ŝ			3	8	9	8	3			8	002	002	8	003	8	8	8	9	003	004	007	8	8	8	2	100	i s	000	8	000	ê	H		7	Ì	ľ	T	Ť	1	Ť	Ť	Ť			1	1	
t	t	t	T	t	i	t		1	Г	ï	Т	Т	Т	Т	7	Ž,	Т	Т	Т	T	Τ	Г	1		Г	_	Г	_		7		7	T	3	7	7	_	~		_	-	$\dagger$	-	÷	t	+	t	†	$\dagger$	t	$\dagger$	t	Н		†	†	-
1	+	+	+	+	H	H			۲	Ť	T	+	Ť	+	+	+	Ť	+	+-	<del>†</del> -	┿	+	-	-	-	Η.	-	_	-	-	÷	+	+	7	+	╈	+	+-	Н	Н	Н	+		-		-	╀	+	+	+	+	╁	Н		+	+	
-	1	+	ļ	1	L	Ļ	8	=	24	-	ŀ	3 8	3 4	1	2	X :	Ť	1	1	I	2	2	=	•	17	3	73	73	Z	=	7	-	1	1	8		8	12	7	•	=	4		1	,	<u>.</u>	Ļ	1	1	1	1	-			1	+	_
	1	1				L					L	1		1		1		L	L	L	L											1					L						1				L	1			1				1		_
L					L		=	671	ž	ě	è		8	1	2 8		á	8	8	8	693	2	7	72	8	89	9	67	8	5	2			1	8	2	2	2.3	=	7	=		1				L	L			l			Ц	1		_
	1		L				235	210	8.8	ã	ā					3 5	0	24	246	18.3	ī	12.5	12	134	8	2	227	¥	×	8	2				:	3	ž	73.5	202	17.3	129		1	ī	Ī	ľ				1							
				L						L								L	L							j					$\int$	I		Ī		ſ					Ī	J		ļ	į					Ī				J	Ī	Ī	
	I	I	$\llbracket$										I	I	I	$\int$	I								1				Ī		J	Ī	T	Ţ	T			П			1	T	9	C	O STATE AND	ſ	Γ	Γ	Ī	T	Ī	П		1	T	Ī	
	I	I	Ĺ				25	2	200	20	2	20	15		100	200	250	2	Z	ã	142	120	a	=	9	į	2	3	ž.	7 .			:	1						j	]	I	1					Ī		I	Ī			I	I		
		ĺ						Ĭ			Ĺ	Ĺ	Ĺ		ĺ	ĺ						Ī	I					Ī		Ī		T	I	I								Ī	100		Ī					Ī	I			T	I		
_	Ĺ	Ĺ									L	Ĺ	Ĺ	L	Ĺ	Ĺ	L	Ĺ												Ī	$\int$	$\int$	Ĺ	ſ	Ĺ	Ĺ			$\int$	J	$\int$	I	-		976	Ĺ	Ĺ		L		I		$\rfloor$	$\int$	Ī	Ĺ	ز
_						-	1	1	_	Ц				Ĺ	ļ		L	L				1	1	1		ĺ	]				1				L					ĺ			07.00	1	Appear	L			L	Ĺ	L	Ц	_[		$\perp$	L	
	L	L			-		اه	٠.	۹	۵	â	a	ů,	â	ĵ	3	2	×	â	=	7	=	1	-	5		اء	٩	اد	:	-	:	5		200	200	۰	-	ā		a		F			L											
Î	ĺ		I	Ĭ	Ī	Ī	2		i K	8	2	=	8	*	=	17	8	ž	1	Ī	Ĩ	Ī		Ī	Ī	Ī	Ī	Ī	Γ	Ī	ſ	ſ	Γ	Ī	П	П	Ī	1	T	Ī	1		Ī	Γ	Γ			Г	ĺ	Γ	П	$\prod$	T	T	Γ	Γ	1

•	•	•		-	-		Ž	_	6239	8			¥	SANC C		Š	2435	á		3	*	57.85	7/10/85	57.78	3	SALA			Š	26.0			10/10/94	Q	9		21	2	5	No. of	29.94	1/4/94	2000	877			5	E651/8	\$21.03	Š	3/23/90					O.X.		WATE		Ī	Ī			3. Sourc		2. Source		. Sized		O' AMORA
				Ī	Ì	1					1															Ī	1		Ī		Ī					T							Ī	T	Ì	1	١							_						Ī	1									
			T	Ī	Ì	1				1	١	1			1			Ī	1		٦		Γ			Ī					-				1	1				Ī	Ī		Ì	Ī	Ì	Ì	j	1				0200	17-1061 AP	S.			Γ	Ī	Ì	1	1	1							_	
			Ì	Ì	1	1		Ī	-		-			ŀ	1		-	6	,	-		0	-	Ì	Ì	Ì	Ì	Ì		Ī	Ì		ľ	Ī	Ì	Ì			Ī	T	ľ	Ì	Ì	T	1	1	1		Ì		r	ž	1		ı		l	T	Ì	†	1									ľ
	-		t	t	1	1		l			1	-		ļ.	1	_						-	-	1	t	T	T		_	Ť	t		r	İ	Ì	1	_	-			r	Ì	İ	t	1	1					<u>-</u> -	+-	-	İ	Cofforms		r	t	†	t	1		_						-	
	-	-	1	†	1	1	_	-	-	t	1	-	-	t	1	-		t	1	1	_	-		l	t	t	1		_	t	İ	-	1	İ	t	1	-				t	t	1	†	1	1					İ	Sen	pw/100cml.)				-	$\dagger$	†	†	1	-		H					ŀ	-
H	-	-	+	╁	+	-			1	+	1	-	l	t	1			t	+	_	_	_	-	ł	1	1	1	-	_	t	+		-	ŀ	+	1	-	H	-	-	t		+	t	1	-			Н		L	Ozo	1	Č			H	t	+	$\dagger$	-		-	-		H	_	-	-	
	H		1	t	+	-	h		t	1	1		1	ł	1	_		t	1		Γ	l	r	t	İ	†	†		_	T	1	_	-	t	†	7	_	-	-	İ	t	1	†	†	1	1	-	-	ļ-	-	İ	7					ŀ	t	†	+	1		-	-	<u> </u>	-	r	H	-	
h	T	t	1	t	1		-	l	t	ļ.	•			1	1	-		t	1			-	İ	t	Ì	t	1	-	-	Ì	1	_	ľ	t	t	Ì	_		ľ	t	t	t	Ì	Ì	1	1		r	r	İ	Ì	+	-	•	٠.	1	t	Ì	1	1			Ĺ	T	1	İ	r			1
Ī	T	T	†	1	1				Ť	İ			Ī	Ť			İ	Ť	1		l		Ī	T	T	1	Ì		Ī	Ī	1	_	Ī	Ť	1			Ī		Ì	ĺ	Ť	1	Ì	٦	Ī		Ī	Ī	Ī	t	t	801	9			ľ	Ť	İ	1	Ī		İ	ĺ		T			İ	Ì
Ī	Ť	1	T	1	1				Ť					Ť		ľ		Ī	1		Ī		Ī	Ī	Ī	1			Ī	1			l	Ī	1		_	Ī		1	Ì	Ī	1	1				r	Ī	Ī	Ì	T	Raw Settl. Ozon.	100	Glavera		ľ	İ	1	1			Ī	İ		T		Ī	T	١
-	t	İ	1	1	1		-		1	1	-		t	t	-			,	1			-		,	1	İ				1			İ	t	1				t	†	1	İ	1	1			l	-	T		İ	t	7			COO		1	1	1	Г		1	İ		T	1	t		1
L	1	t	†	+	1	_	-	t	t	-			l	1	â	,	l	1		_			t	t	t	†			-	t	1	İ	l	İ	1	_	_	1	T	t	1	t	1	1	-		r	-	t	-	t	+	R	+	İ	Statistics of the Colonial States		†	1	1	Γ	h	İ	Ť	1	t	t	T		1
ŀ	+	+	1	1	1		L	Ì	1	1		_	ł	1	_	-	t	1	1	-	F		1	t	t			_		1	_	-	t	†	1	-		-	1	t	1	†	1	1			ŀ	Γ	t	+	1	$\dagger$	12	90		2000	-	t	1	1	-	<u> </u>	<u> </u>	+	t	t	t	t	t	1
-	t	†	+	+	1		<u> </u>	1	+	†		-	1	1		-	ł	1	1	_	ŀ	ŀ	+	+	1	1	-		1	+	1	ŀ	1	1	1		_	1	1	+	+	i	1	1	4		-	-	t	H	1	t	Sent. Ozon.		i you		ŀ	Ť	1	-	L	-	-	1	+	+	ł	1	-	
	1	1	1	1	-	_	L	1	+	+	_	L	Ī	1	-	_		1		_	H	-			+	1	-	_	!	+	-	<u> </u>	+	1	-	_		-	-	1	<u> </u>	1	+	-		L	-	<u> </u>	÷	L	1	+	13	1			f	+	1	_	_	1	T	-	+	+	1	+	1	-
_	Ī	T	1	1	4	L		I	Ì	1	_	•	1	+	4	-	T	1	4	_	L	+	ľ	+	1	+	_	_	<u> </u>	+		Ĺ	1	1	-	_		L	<u> </u>	1	+	1	+	+	_	_	-	L	l	I	+	+	_	_	Ŧ	1	-	1	4	_	H	H	-	<u> </u>	H	1	+	T	<u> </u> 	_
_	1	ł	1	-	4		L		<u> </u>	1		L	-	1		<u> </u>	-	1	4		L	-	1	+	+	1	_	_	L	1	-	L	1	1	_		L		1	1	1	1		4	_	L	_	-	-	  -	1	+	200				-	+	-	_	_	-	ļ	-	-	+	1	  -	1	
_	-	1	1	1	4		_	ļ	1	1	_	L	1	1	_	L	1	1	_			-	+	1	1	1	_	_	-	1	_			1		_	L	1	-	1	1	1	_	4	-	L	L	L	1	L	Ļ	1	A SEUT OZBA			5	-	1	1		L	1	L	<u> </u>	1	ļ	1	-	-	
L		l	j				L	1		1		L		1		L	1			_	L		Į	1	1			_		1	_	L		1			L								_	L					ì			1		1					L					ļ				
_		ļ	1	1	ĺ		L	L	1	1		L	ļ		_	L	ļ	-		_	L	_	ļ	-	-			_			_	L	ļ	-			L		ļ	1	1	1	1	1			L		L	L	L	1		_	1		ļ	1	1		L		Ļ	ļ		ļ	ļ	ļ	-	
		ļ	1	1	_			ļ	1	X.	ĝ	š	2	1	8	8	1		Š	š	8	2	Į		1	1		_		1			1	1		_	L		-	1	1	ļ	-	1	ا	_	L	ĺ	Ţ	-		1	NAM Settl. Olen.					1	-		L	L		1		ļ		1	Ļ	
_	ļ	ļ	1	1	4		L	ļ	-	1	_	L	1	1			-	1	_	_	L	L		1	1	-		_		1	4	L	-	1		_	L		ļ	ļ	1	ļ	+	4			L	_	ļ	Ļ	ļ	1	12	2	3	5	-	1	1		Ļ	_	<u> </u>	1	1	1	-	1	ļ	
L	1	1	+	1	1		-	-	-	 	4	_	ļ	1	_	_	ļ	1		_	-	-	1	+	1	-	_	_		1	4		1	1	_		L	-	-	1	1	-	-	4	_	L	L		-	  -	  -	1		۳.	Į,	1	-	1	1	_	Ļ	-	-	+	ļ	1	1	1	<u> </u>	
L	L	ļ	1	1	1		L	ļ	ľ	1	•	-	•	1	•	2	1	1	٥	•	ш	ľ	1	1	1	1	_	_	L	1	_		1	1					1		1	1	1	1	إ	L	L		ļ	L	ļ	1	7	-	1		1	1			L	L			L		1	1	1	
				-																													-									1										COMOLINA	X. 44 LYA. Pend	230044																
_	-	-	+	+	4		L	H	ł	1	-	_	Ļ	1	-	<u> </u>	-	1	-	_		-	1	1	1	+	-	_	L	1	-		1	1	-	_	L	-	1	+	1	1	1	+	-		L	<u> </u>	+	<u> </u>	1	1	NAW PE				-	+	-	1	_	-	-	+	1	t	ł	1	1	7
									ŀ	٠,	~	×	,	٠,	~	×	,	,		×	×	×	,	,	-	*	*	×	×	٠,	×	×	١,		×	×	×	×		,	1	-	×	×	×	×	×	×	×	×	×	THE PORT	×	40																
_	1	1	1	4	4	_	_	1	1	+	1	_	1	1	-	_	L	1	<u> </u>	_	L	L	ļ	1	<u> </u>	+	-	_	_	1	_	L	1	T	-	_	_	L	ŀ	1	1	1	1		_			L	Ļ	L	-	12	1	ľ			-	1	-	-	H	-		1	ļ	-	-	1	1	1
									1		5	1	8		3	2		1	-	3	8			ŀ	:	-	=	5	-	.!.	-	ᅜ	18	C)	ĸ	-		12				.  " '	4	-	3	:	-	=	-	10		100		Chaosic																
_	1	ŀ	Ť	+	+	_	L	1	ł	1	1		-	ł	1	_	1	ł	1			ī	1	1	1	t	-	_	_	1	-	-	1	1	1	-		-	-	1	Ì	1	1	+	-		-	-		1	1	2	T	2			1	+	+	4	H	-	-	+	-	H	+	1	1	-
									1			ï	265	ľ		8	8	۱	6	8	8			1			2	5	047	ľ		å	10	ľ	3	=	8	8	951		۱			3	ê	٤	83	037	30	0	2	1	1	Month		5														
	T	Ì	T	1	Ť				İ	İ	İ	Ī	İ	t			T	t	İ		-		T	T	T	Ť	1	-	r	İ	1	_	İ	Ť	1	j		1	İ	t	İ	Ť	1	1		-			l	Ť	Ť			t	3	BUT KIO	-	t	1	1	П	r	İ	İ	T	İ	T	t	t	
	L	L	1	1			_	L		1	1		L		1		L	ļ	1	į		L	L	-	1	1	1	_	L	1		_		1			_	L		L		1	1					L	L	L	L	CONDICIONA		actions.	ž	of Cond		1	1	_	Ц		L	L				L	L	1
							i					8				z	2	ŀ	إ	2	2	2	,		١		×	8	27		-	ø		l.			2		1	اِ				ا.			13	3	53			Chio	2	adjon ik	Mores	2														
									•		۱	٦	5	1		4	-	1	1	-	7	17	٦	•	1	1	1	-	-			-	-	ľ		٦	=	•	-	1	1		1	ľ	1	٦	ū	7	2		ľ	-		1																
		Γ	Ī	Ī	1				Z	2		=	12			12	15			2		2		21		Ī			=	Ę		1	7		,	×	×	15	=			-	1	Ī,		7	N.	2	8	_	_	1	1	7			ľ	T	Ì	1						Ī	Γ		Ī	Ī
		L		1	1	1		_	_	1	1	-	5	ľ	1	"	•		1		_	2	_	_	ľ	ľ	1	7	_		1	3	~	1	1	1	7	•	•	-	•		ľ				~	•	8			0					L	L	1	ļ			L	L	L	L	L	L	L	
													ž	3		=	2	8				Š	9 07						:									2	17								-	-	-	-		L		ł						1										I
4		L	L	-	1	1	-	_		1	1	ı		1	1	- 1		1	i.	- 1	- 3	j		Į			1	ł	- 1	ı	1			ſ	Į	1	- 1				1	1	1	П	1	- }	- 1	- 1	11			Į	1				L	L	1	1	4		_	L		L				-
									=	112	1	2	2	2	1	- 6	2	2	1	2	2	97	8	DX.	200	18		=	=	-		8	:5	=	1	3	ŝ	2	Ξ	8	=	1	ļ	-	-		=	티	135	077	0	THE CITY		National Property																
1	1		-	f	t	1	1	_	-	-	1	+		r	t	1	_	۲	1	1	1	_		۲		r	ł	1	-	-	1	-	-	r	t	†	1	1		-	-	-	1	t	+	1	+	1	+	-		_	P. P.	-		<u> </u>	-	+	+	+	1	-[	_		۲		Н		-	1
1	1	_	-		-	+	1	-	_	<u> </u>	L	1	-	-	1	1		۲	1	-	1	-	_	۲	L	-	1	+	-	-	1	1	-	r	1	†	1	7		-	-	-	-	1	1	+	1	1	-	- 1	4	П	П				-	-	1	+	+	+	-	-	Н	Н	Н	Н		-
									į																								į				-																¥																	
T	1	-			Ī	T	1	j				Î			Ī	1		_								Ī	Ī		1		Ī	1				Ī	1	1	1		_	Γ				T	1	1	1	1	1		0,00	Ę	됲				İ	Ť	Ť	Ì	Ī	j	j		j			Ī
-	1	1			-		1															1										1								j	ļ				1			-					3	1						1			-		_				_	

•	•	•	•	-	-	1	F		25	56.58	41.70		ć	2598	1898	7480	1	Š	10295	2611.7	57.5	1000	1000	5	Š	3,17	21495	0,000		Š	17/24	1000	5			704	Mais	Ş	Y1.54	159	1		12/8/93	107703	10/5/93	6/18/93	91335		SI:	5	54.52Z					D.A.		WAIE		Ī				J. Sourc		2. Sourc		i Study		CHEMY IO
									â	8	1	1	â	å	â	é	3	å	å	âS	as	5																															7	į																
	-	l	-		†	1	1			l	t			_		Ì				-	l	T	ł	1		_	-	t	1	-	-	-	l	1	1	-		-	-					-		-		1	1	1			7	_	HAAH	Disintectio	-	l	†	T	1	1		_			T			r
Π	-		-	$\dagger$	1	1			-	L	1	-	_				1			-	1	-			-		-	t		_	-	-		1	1					t	1	1			t	-	1	1		1	1	- 5	502		_	A BY WE			1	†	1		_				-			1
			İ						l	İ	t		-		Ì	Ì				r	İ	İ	1	1	-		T	İ	j		Ī						Ī	Ī	Ī	Ì	1			Ī	Ì	T	Ì	Ì					Cion	2	IAA	Sucts	ľ	Ì	1	1	1	٦				T	T	İ	Ī	
+	-		L	+	1	+	-	_				15	۵.	٠		,	۵	1	1		\ \ !	١,	3	1		L	1	1	-	_	-	+	1	1	-		-	-	1	+	1	_			+	<u> </u>	1	-	-		_		7 F#				-		-	1						1	1	l	1	ł
1	$\vdash$			+	1	+	-					-	~		1	1	_	_	Ī	T	T	Ť	1	1		-	ļ	+	_							_	-			1	1				t	$\dagger$		-				-	R	<del></del>	-		ŀ	t	+		-	_	-			-	$\dagger$	t	t	+
1			I	1	1	1				1				I		1		L	_	I	Ţ	ļ					I	1				Ī	1					I		1			L		I	1	1						2071	2	ō		L	I						Ī	I	1	1	Ţ	Ţ	Ţ
+	ļ	ļ	1	1	1	4					1	_	_	1	1	1		L	-	+	1	1	-		_	I	1	1			-	+	1	-	_		-	-	1				_	ŀ	+	1	1	_			L	L	d. Ozon. Ful.	Š	_		-	1	-	_		L	<u> </u>	ļ	1	+	+	ļ	1	1
+	1	+	1	+	1	-			<u> </u>	1	1	-	-	1.		-	_	-		.].	1	-	_	_	L		. .	-	=	-		1		-	_	-	-	1.	1	-		_	-		-	1	_	_	_	_	-	1	<u> </u>	٠.	5	1	1	1	2	_		L	<u> </u>	1	T	1		+	1	+
	L								1.10		3	12/3	12/3	2		273	72/3	/2/3				3	2	12/3	23	14.0		3	7273	12/3	1		313	2/3	72/3	17/3	1			2	/2/3	12/3	1213				23	/2/3	12/3	12/3	1/2/3	L	(see share	ě	Supple Street		-		7		•	_		<u>.</u>		1			1	1
											8	à	77.9	4		417	50	CAL	-	1	X S	5		8	87	ŧ	3	71	8	-			-	1	z	3	5			- [		1	8	,	4	×	37	24	ð	37	8			-					REATMENT CONDITIONS			Non-toric	Call of	7		The state of the s	day of the			
$\dagger$	t	-	+	1	1	-				+	-	2	3		-	-	ā		-	+	-	1		_			1	3	_	-	+	- -	-	-	08		-	. -	1	21	8	Г	l	-	+		_		_	-	3		1	~	0016	- Bearing	ŀ	Ī	ÖVS		_	L	1	l	-	7	1	+	t	1
+	1	1	Ť	+	1	_	_	-	+	+	4	-	L	<u>.</u>	,	-		-	18	÷	1	-	-	-	-			22	0.	00/2		2	0075	0075	9	90/2	1		2	000	_	_	1		9	9	02	012	-	014	-	-	$\vdash$			THE CHICAGON		1	-					+			1	†	t	+
	l	Ì	Ť						,	1	2	z	12	,		=	2	×	-		1	2	z	z	×		=	z	z	3				×	z	2	,	Ī,		2	2	-	-	İ	z	=	=	=	2		z	T	TAN	0,000	ģ	1	Ì	1			-		t	t	4	5	-	Ť	Ť	İ
T			1	1																																															z		TANK S	Desamon				-							1				Ī	1
			Ī					Ī	Т	7	٦		Γ	Ī	Ī	7		ī	100	T	i	1	٦	Г	Γ	Ī	ī	٦	Ī	Γ	Τ	í	٦			Ī	1	ī	ī	8				1	Т	Т		Г	7	1	ī	Т	_	ī	Т	7									Ī		Ī			1
T				1					1	3	2	ē.			-	2	28.5			1	317	23.3	24	246	183		-	125	5	1	Ţ,	3	12	2	æ	10/		1	-	=	2	1	1	ī	i	Т	٦			-	129		lees C	ierro.	.000	1														
T		Ì							Ī	T	1			Ī	Ī	٦		Γ	2	ī	1	į																									7	200	l	i	8	77	-										Ī						T	
Ì	Ì	Ì	Ì						Ť	7	7	_	Г	Т	Т	7	_	ī	0.03	۲	Т	Т	- 1		1	١	1	- 1			1	1	- 1	- 1		ı	18	1	- 1	ı	- 1	i	i.	Ė	-	٠,		080	110	8	9	701	1	914	1000								Ì			1	Ì	1	T	j
T	Ì								4		s	0	0 19	9		013	0	0 16	00/			2	ŝ	2	27	0.14		=	ğ	0.50	:	إ	037	0 27	2	013		1		2	013					1	S	0 29	8	25	2	1												Ì	Ì	Ī	İ	1	T	
			Ť				-	ľ			2	2	000	la		2	2	98	8		2	31	2	0.5	3			000	8	2		1	2	23	Š	8			3	8	8	0	0.78	1			015	018	0.2	028	029	~	Tybers.	Residual	Mozo	O de properto		Ì	_	-	Ī			İ	İ			1	Ť	
İ	Ī		Ì				-	-	١	1	×	013	001	10		2	0	009	2	1	2		037	024	8	5	3	8	8	9			-	015	002	904	1012	1	3	2	8	0 19	014		3	-	015	018	02	028	20	-			Ì	THE COMMENTS		İ		_	-				1	Ì			Ť	1
	T		Ť	Ì			_	-		1		3	21 39	8		2	1248	9.36	12.88	3		1	-	181	*	3		5	ī2 <b>8</b>	824	ž		2	22		5	-		3		1291	1337	12.8		j		-	- 8	242	ž	279	T	3	New York	Consider							Ī	Ī		İ	Ì			1	1
												3	701	Š			36	78				c c	73	6 20	5 85	12		ŝ	7	12	3		2	5	5	=				8		8.7	2		7		8	6 75	6.9	7	6	,	-	Г	Т	٦.				_										1
T	ľ				1	İ			1	1	İ	ı		1	ı	Į			ı	١	1	ſ	1	- 1		ı	1	1		ı	ı	ı	1	ļ			707	1	1	1	1		l	ł	1	İ							de C	derrop	Ozen			1				-		l	1	T	1	1	T	1
-	-	-	l	$\dagger$	1	1			-		1			-		1		_		l	t	1	1		_	-	Ì	1		-		1	1		_	-		1	+	1	-			-		1	1							-		I	1	1			_				1	Ì	$\dagger$	$\dagger$	$\dagger$	1
	L	L	L	+	+	1		_	L	L	I	-			<u> </u>	1	1	_		L	T	Ī	1	-		_	I	1				1	1	1		_	_	l	1	1	1	_		L	+	ł			-					L	L			1	1		-			-	ł	+	1	+	+	+
-	<u>L</u>	L	+	1	+	1	1		L			-		L		1	1	_	L	L	1					L		1		_	L		1	1	-		_		1	+	1	_	L	L		1	1							L		L	I		1	_	-		_		1	1	+	1	+	+
		L	-	-	1	1	+		L	L	1			_	L	1	1		L	L	+	1	1	1		L	-	1			L	-	1		-		-	-	-	-				1	1	-		1	-	-		Н	Ц	_	-	L	-		1		-				1	+	1	+	1	+
	L	_	-	L	1	+				_	-	1		_			1		_	H	-	1	-	1			-				L		l	1	1		L	L			-			_	+	1	1	-	1	_		Ц			-	L		Sugare		Pagi Ozona	1	_	L		+	1	1	1	+	+
H				L	-	1	1			L		-	-	_	L	L	1			L	-	-	1	1	-	_	_	1	1	_	L	-	1	Ŧ	-	-		L		1		1		L	1	-	+	1	1	-	1					H	-	74	1	2	-		L	L	L	1	+	+	+	+

12/18/91	1/18/0	19/21/01	10/01/6	16/81/6	8/19/91	1/8/91	7/8/91	1878/1	2/1/2	5/20/91	4/8/91	1	3/1/01	211/91	17/01	17/91	17/7/00	11/28/90	0/5/90	10/15/90	0/17/90	8/20/90	7/16/20	6/25/90	5/21/90	08/8/7	DELSAC	2/20/90	1/22/90	12/11/89	12/11/89	11/13/89	9/25/89	8/14/89	7/17/89	6/19/69	6719789	68/61/9	S115/89	4/17/89	68/E1/E	2/14/89	1/17/89			Ī		Date		WATER		If enterin			Nimous D	City of	2	Descri		3. Source		2. Source water:		Sludy	of family	
																																																1kma	1	QUALITY DATA:		g data on			Nimbus pam, American river	20110110	Sacramer	Do Do		Source water ID:		water:		ġ		
17	1.4	i	-		3	ŝ	1.7	.3		5	٥١٨	3	2.3	:	1	1.2	1.5	1.5	- A	5	-	=	3	ᆲ	1	1.2	3	=	1.3		1	-	-	5	1.4		2.3	-	-	•	2.0	-	24			Opan.				YDAT		Saason			CHI KING		Ho com	Tale Te		1						
	П	T								Ī																					T										Ī					0000	The state of	NOC.	-	A: RAW		al chang		T			200	To for Y				П				1
3	27	2	×	24	28	27	ಜ	28		8	3 8	s	2,5	: 8	1	25			22	21				27		4	g	25	5			3		3	ŀ	120	2		1	1	3 6	3 5	2 %		T	2	and the	Alkatinity		2		es in pla					p spew	thich wa				Ę		EBMUD		
																		L														1											1				1					m raw		1			Scharge	ter qual				(American) River	Ц	Alternate Source		GUMB3
23	25		2	22	24	2	31	25		3	3	á	2	3 0	1	21			20	18				27		29	2	26	1		3	2 2	2 2	3 2	4	3	120	3	3 2	2	3		3 6	:	100	l)pele	1000					OUICE N					ř	ity data				River		Source		ă
						1						Ť		T	+								-							+	İ	1		1	T		Ť		Ì	$\dagger$	1	T		1		Down	Total	Hardness			1	entering data on seasonal changes in plant raw source water quality, use upstream column.		1			-	Describe point of reference for which water quality data are being supplied, i.e. upstream and						Sludy		
â	200	ô	007	601		60		<u>-0.01</u>		60	9	001	9	0.02	3	60 01	ô	ê	6.01	0.11	001	0 02	<0.01	- 60 G	001	Ŷ0.0	5	200		2			2 6				Ì				١	3 6	3 6	à	Ì		Upsir		,		Ì	use u		Ì	Ì	1		upplied,		(State)		THING.		(Optimal		IACME
			$\dagger$			1				1	+	+	$\dagger$	+	t						-				<u>-</u>	-	1		1	1	+	Ť	+	1			t	T		T				1	1		Down.	( New)		$\dagger$	+	THE PARTY	ŀ	1	+	1		e. ups	Г	(Slate Project water, etc.)	-	(River, lake, groundwater,		(Optimization Study 8/95, etc.)		(ACWD, CCWD, EBMUD, MWD, SCVWD)
H	0 0		000	-		+	$\frac{1}{1}$			1	602		0 0	-	1	╁	H	H	-	_			_	0 03	<u>L</u> İ	C00.00			2000		-	0	1	9	200	1	$\dagger$	1	200	3 5	3	2	2 2	3	1			<u> </u>	_	<u> </u>		COLOMIN		1	+	-	_	tream a	-	ater, etc	-	undwate	_	udy 8/95		EBMU
H	=		2	-	<u> </u>	+	-	-		  -	20	7	-	+	+	1	<u> </u>	T	<u> </u>	<u> </u>			-	j ü	-	5	1	,	1 2	2	-	-15	<u> </u>	1	*18	2	1	1	- 18	312	5	†		6	1	+	Dow	CHO NHO NA	-	1	+	1	+	+	1	1		nd downstre			Ť	r. efc		elc)		J. MWO.
2	u		u J		3	2	داد	2		ناد	2	_		+	-	- u			-	2	N	2	_	<u>ا</u>	_ 	-		١.	1	1	1	2	1	1	+	<u> </u>	+	1	•		-	-	5	_	+	+	5	3 9	+	$\dagger$	$\dagger$	1	+	-	+	1	_	stream of	-	-	t	t	$\vdash$	-		SCWVD
H			Ť	T	H	Ť	t	<u> </u>		+	1	1	+	+	†	$\dagger$	t	T	Ì	r			-		Ì		T	t	Ì	1	t	†	-	-	1	İ	i	İ	Ì	1		İ	-	†	1	-	Down	(mg CI-A)	-	t	t	+	+	Ť	1	1	_	Ī	F	T	t	T	t			
2	â		ŝ	55	ŝ	à	-51	8		51	55	a	٤	5	ŝ	4				â	39	۵	à	5	5	12	١	2 2		à	ŀ				2	•	Ì,	2	3	s	5	2	8	S		Į	딍	Ī		T		Ī	Ī						Γ		Ī	Ī	Ī	Ī		
			Ť				Ī						Ì		Ť		İ								Ì	Ì	T	Ì		1	1				İ		1		Ī		Ì	1	Ì	1		Ì	str. Down.	2	-	$\dagger$	j	Ť	1	Ì	1	j			Ī	r	T	T				
0 79	1.2		=	0.6			-	12			- i	Ì				1		0 94	0.8	0.77	0 95	2.5	0.5	0.38	0 54	100		100		-		25		210	3	0 7	1		-		2 1	3	0	3	j	į	등	Ī		Ť	Ī	Ť	T	j					İ	ľ	Ť	T	T			
İ			Ť			Ť	Ť			Ì	1	Ì	1	T	+			<u> </u>		$\vdash$			-		É	Ì		t	t	†	1	Ì	Ì	1	$\dagger$	Ì	+	1	+	1	1	ì	Ť	1	Ì	-	Dow	NTU.	-	$\dagger$	1	+	1	1	1	1	-		-	F	t	$\dagger$	T			
7.6	7.6	1	7.4	7.6		7.5	0	71		7.6	0011		1:	710	+	1		<u> </u>	-	7.4	_	<u> </u>		7.5	-	-	1	+	+	+	1	7	77	-	1	- -	+	+	†	1				+	+		Upsir.	+	1	$\dagger$	-	<u> </u>	1	1	1	1			<u> </u>	H	+	$\dagger$	+			
H	ľ		7			7	F	_		-	1		<u> </u>	1	1	+	<u> </u> 		-	_			_	_	<u> </u>	1	L	i.	1	1	- 1	_L.			_!_	!	1								-			=	-	+	<u> </u>	1	1	+	+	-	_			<u> </u>	ł	╁	<u> </u>	-		
	5	1	205	22		23.5	+	20.5		21.5	- I	=	<u> </u>	-	+	1		<u> </u>	<u> </u> 	20			-	17			<u> </u>			-	1		1	<u>ا</u>	21.	ار	1	1	1	-1:	1	<u> </u>		+	1	-	딁	1	+	+	-	+	+	1	1	1			_	<u> </u>	T	$\frac{1}{1}$	H	-		-
	54	1	5	-		5		2		511	1	-	1	1	+	H	-	-	_ 	<u> </u>			<u> </u>	G	-	0	1		+	+	1	1		-10	7	1	-	1	1	1	7	1	T	+	+	1	Dow	den C	1	+	1	Ť	+	+	1	-			-	-	+	+	+			$\dashv$
70	130		1	350	œ	5	8	8	i	2 2 2	3 5	_	1	1	; =	8		8	17	5	9	_	-	œ	12	=	<u> </u>	2			3	<u>_</u>	-	3 8	4	ا	<u> </u>	<u> </u>	,	<u>.</u>	5			2 1	5	_	<u> </u>	(ded C) Colforns	+		1	1	1	+	1	1	_	L	<u>L</u>	<u> </u>	+	+	H		-	$\exists$
H	10	1	1		9	7	500	١٦		3 8	1,	+	18	5 5	1	, 3		ı	-		-		_		٥	1	T	-		15	5	5	1	1	1	5 2	9	7	7	7	916	1	1	"	Dev	V100m	167	3	-	+	+	+	1	1	+	1	_		-	$\vdash$	+	+	-	-		-
17		1		١	2	+		ب	2	_ ,	2	+	<u></u>	20	<u> </u>	4		L	7	3				Ç4	_	5	L	5		1	3 9	١	ļ,			<u> </u>	1	1	ا.	ار	<u>.</u>		<u> </u>  -		5	<u>-</u>		oliforns	-	+	+	+	+	+	+	1	_			-	H	+	+	H		4
70	원	1	5	8	ω <sub>1</sub>	1	10	٥	ü	= 8	<b>5</b>   6	1	12	1	12	8	-	<u> </u>	20	ō				٥	L	1	<u>                                     </u>	٤	1	5 8	3 2	=	7	5 6	318	5 6	5 6	7	7	7	3 6	5	1	- 1	Sir Do	100	Fecal	S. Calana	-	H	+	+	+	+	+	1	_			L	+	+	1			4
Ш		1			1	1	1	1	ŀ		1	1	I	1	L				Ш		- 1	ļ				1_	1	L	1		1	1	1	1	1	1		1	1	1	1	1	!	13	1	-1	1	1	1	ı	L	1	1			ı			Ш	L	1					

Utility ID:		1	T		ACV	VD.	<del></del>	I/ACWD	CCWD, E	DAILED A	MAD SC	VAMOV		<del>,</del>	<del>,</del>		
Duncy 15.	<del>i</del>	<del>                                     </del>	<del> </del>	1	1		}	ICACVID.	CCVVD, E	BMICD, N	1	1	-	<del> </del>	<del> </del>	<del> </del>	+
1. Study ID:	<del>/</del>	<del> </del>	<del>                                     </del>		1		i	(Optimiz	ation Stud	v 9/95 et	(C.)	<del> </del>			<del> </del>	<del> </del>	<del> </del>
	1	·			1		<del>i                                     </del>	1.575	T	1	1	<del>i</del>	<del> </del>	<del>i</del>	<del> </del>	<del> </del>	<del> </del>
2. Source w	/ater:			ī	i .		1	(River la	ke, groun	dwater, e	tc.)	<del>                                     </del>	<del>                                     </del>	<del> </del>	<del> </del>	<del> </del>	1
	T	1		7	)			1	T	1	Γ΄	1		-	<del>                                     </del>	<del>                                     </del>	1
. Source w	rater ID:			T				(State Pr	oject wate	r, blend o	of, etc.	)		1	<del>                                     </del>	<del> </del>	1
				ı					Ť			1		<del> </del>	i	·	
. Describe	level of st	udy:		Bench-	scale		in this dat	a sheet, "	Filt." refe	rs to dat	a collect	ed	1				
indicate wi	th an 'X')			Pilot-se	ale		after coap								<del> </del>	<del>                                     </del>	
				Full-sc	ale )		fitration.	1	Γ	T		1			<del> </del>	1	
								1	1			1			i	<del> </del>	
5, indicate v	with an 'X'	if data n	eported a	s "Filt"	are from	m samples	collected	after sed	imentatio	n only:							
								er sedime			ion:						
NATER QU	ALITY DA	TA: COI	VENTIC	NAL													
			ļ														
Date	Time		C	UV-		Bros	nide	Turt	idity	Tempe	rature			Disinfect	ion By-p	roducts	
		(mg		(1/0		(110			TÜ)	{deç	). C)	111	HM	HA	A5	HA	AG
		Raw	Fitt.	Raw	Filt	Raw	FIIL	Raw	FIIL	Raw	Fin.	(μց			VL)		/L)
												Raw	Fin.	Raw	FIL	Raw	FIIL
£20.00		!		<u> </u>		!				اسييا							
5/30/95		4.3	2.7			- 42 - !		16.2		65.4			ابي				
6/6/95		4.3	2.0			40.0		29.0		65.9			28.9				
6/13/95		3.5	1.8			42.0		14.1		67.3			40.2		46.5		
6/27/951		3.8	2.0			60.0 80.0		15.5		76.7			49.6		48.0		
7/4/951		4.2	23		+	00.0		17.4		73.3			45.2				<del> </del>
7/11/95		4.1	2.1	<del></del>		68.0		23.0		72.3			43.0			ļ	<del></del>
7/18/95		3.8	1.9	<del>' '</del>		50.0		19.5		73.5			45.9		<del></del> ,		
7/25/95			2.4			72.0		21.2		72.5			48.0				
8/1/95		41	2.2	<del></del>	<del></del>	65.0		13.3		78.3			48.0				
8/8/95		3.5	1.9	<del></del>	+	60.0		11.5		76.2			49.8				
8/15/951	<del>i</del>	31	2.0	<del>i</del>	<del></del>	60.0		11.4	<del></del>	77.0			58.9			<del> </del>	
8/22/95		3.2	2.2	<del>i</del>		55.0		10.6	i	75.6	<del></del> j		58.9				
8/29/951				<del>i</del>		50.0		11.5	—— <del>-</del>	71.2							
9/5/95	i	34	2.0	i		81.0	<20	12.5		70.5	<del></del>	<del>i</del>	61.1		37.0		44.0
9/12/95	i	4.1	3.3	i	-	42.0	12.0	2.3	i	68.9	i	<del>-</del> i	86.9				
9/19/95	1	4.0	3.2	1		50.0	<20	2.2		58.4	i		85.9		58.0		65.D
9/26/951	-	4.0	2.8			53.0	10.0	8.3		67.9							
10/3/95;		41	2.8			49.0	17.0	5.0		64.1			55.4		43.0		49.0
10/10/95		4.3	3.0			44.0	<40	4.4	1	62.6			72.0				
10/17/95	j	4.2				43 0		5.6		63.0		1					
10/24/95		3.9	2.8			47.0	14.0	4.3		61.9	i		ŀ				
10/31/95	İ	3.8	2.5			45 0	12.0	6.5		61.7	j	t	58.6 (		35.0		40.0
11/7/95		3.8			0.07	47.0	13.0	5.3		59.9			72.1				
11/14/95		4.3	3.1	0.18		39.0	12.0				<u>l</u>			!	46.0		52.0
11/21/95		34	3.3	0.19	0.10	42.0	16.0			!						!	
11/28/95				0.14	0.10	86.0	16.0			1			55.5		23.0		28.0
12/5/95		44	34	0.13	0.09	<del></del> !		1.6		58.5			73.1				
12/12/95		4.6	3.7	0.12	0.08	39.0	<20	2.2	!	58.0					56.0		62.0
12/26/95			2.0	0.14	0.10 0.09	38.0 97.0	<20	3.9		55.8			73.3		74 0 1		20.0
1/2/96	<del></del>	3.3	2.1	0.12	0.09	150	24.0	7.6		52.5			616		31.0		38.0
1/9/96		64	3.7	0.24		110	36.0	3.6		53.B	<del></del> -		64.6				63.0
1/16/961		64	3.5	0.27	0.10	87	31 0 24.0	4.8		51.4			75.2 I	+	54.0		63.0
1/23/96	<del>i</del>	3.0	2.4	0.18		~ <u>~</u> '	27.0	93		50.7							
1/30/96		3.5	3.2	0.20				20.0	<del></del>	51 4	<del></del>		77.8	<del>i</del>			
2/6/96	<del></del>	5.6	3.6	0.20	0.11								75.0	<del></del>			
2/13/96		5.6	3.6	0.17	80.0			<del>i</del>	<del></del>	<del>i</del>			76.1	<del>i</del>			
2/20/96		5.8	3.6	0.13		<del>i</del>		<del></del>	<del></del>				88.0			<del></del> i	
2/27/96	1	5.8	3.0	0.20		1	<del></del> i	i				<del></del>	72.8				
3/5/96		0.0	3.1	0.22	0.09		14.0		- i	·i			80.7		54.0		57.0
3/12/96		5.6	3.1	0.21	0.10	1	<20										
3/19/96		5.5	3.4	0.22	0.10		<20						61.3		49.0		52.0
3/26/96		5.3	3.1	0.21	0.09		14.D						81.3				
4/2/96				0.20	0.09							$\Box$	57.2		31.0		38.0
4/9/961		1	أحجب	0.21	0.08								94.7				
4/15/96		44	3.0	0.20	0.10		<10.0				]	آ			59.0		68.0
4/23/96		4.2		0.21	0.09		29.0						71.4				
4/30/96			2.4		0.09		34.0						76.7		41.0		52.0
5/7/96		3.7	2.6	0.20	0.09		41.0						73.3				
5/14/96		3.6	2.8	0.21			45.0						85.0		43.0		55.0
5/21/96					0.09				<u></u>	<u>  </u>			FOF				4
5/28/96		3.8	2.1	0.22			20.4	-					52.3		34.0		41.0
6/4/96		3.6	2.3	0.22			24.5	ļ					70.4		20.5		70.0
6/11/96			1.9	0.50	80.0		17.2	<b> </b>		<b>  </b>			80.1		38.0		43.0
6/25/96			1.8	0.19			10.6	ļ		<del>  </del>			53.9			<u> </u>	
7/2/96		3.2	2,0	<del>  </del>	0.08		25.2	<u> </u>	ļ				43.9				
7/9/96		3.2	Z,U				13.7	<del> </del>	1				54.8				
119/90				i			13.7	<del> </del>									
<del></del>				<del></del>				<del> </del>	<del> </del>	$\vdash - \vdash$		-					
			<del></del>					<del> </del>		i						<u> </u>	
				<del></del>				<del> </del>	<del>                                     </del>		<del> </del>				<del></del>		<del></del>
									5								

11/17/2005 11/17/2005 11/17/2005 11/17/2005 11/17/2005 12/17/2005	á		Dete	WATER		S. Descr	3 3007	2 Source	1. Study	Unitry 18
17096   17096	95	- - -	Time	ATER QUALITY DATA:		ecribe level of study:	urpe water ID:	- Water	Ö	- -
3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	5.0	Rank	$\Pi\Pi$	의 12	1 1	rtudy			$\perp$	
5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	5	Ozon,	201	E-OZONE	×					
5.6 3.7 3.5 5.6 3.7 3.5 5.6 3.7 3.5 5.6 3.7 3.5 5.6 3.7 3.5 5.6 3.7 3.7 3.7 3.7 3.7 3.7 3.7 3.7 3.7 3.7	1			THE THE PERSON NAMED AND ADDRESS OF THE PERSON NAMED AND ADDRE	Full-acale	Bench-ecale Phot-ecale	Boum B	_	Fouting	
<u>╒</u> <u>┎╴┌╶╶╶</u>	-	R N	<u>-</u>			1 1	Bay Aqued	RNet	tine Mankonng	- CWO
<u>╎┸╃╃╃╃╃╃╃╃╃╃╃╃╃╃╃╃╃╃╃╃╃╃</u>	- -	Ozon /	1254		1 2	<u> </u>	- ā	-	- 8	-
0000 0000000000000000000000000000000000		3	-	9	tration	this us	13	7	-	
8 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	25	Raw Ozon. Fit.	Alkalini	or after sedimentation and filtration		in this data sheet, "Filt," refers to data collected after coegulation, flocculation, sedimentation, and	(State Project water, beind of	(River, lake, groundwater, etc.	(Optimization Study 9/95, etc.)	CWD. CCWD
1	2	70	2 -	atation		ulation.	- Sie:	Undwate		J. BWC
100 2 100 2	ig	R		nd filtr		elan or	- 6 9	- (c)	- efc	3
		O d		rtion:	-	ntation.	_ tc )	+	-	SCAMO
<del>╎╏╏╏╏╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒</del>	╁┠	Total Ozon, Filt.	-	+	╁┼╴	2	+		+	+
<del>╽┧╏┇┩╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒</del>			ardnes	$\mathbb{H}$	-	-				-
<u>╎╏┾╅┧╃╁┾┧╃╁╃╃╄┼╀╂╃╃┦╴</u> ╎┦╇┦╢┯╇╀╃╃╣╃╗┦┞╀╅┼┼╃┼┼┦╢╏╢╗┼┼┼┞╣╃╙┆╃╃┼╇╃╇╇╃┼	-	. C.	-	$\left  \cdot \right $	$\prod$	$\Vdash$		Ш	# F	- -
<u>╎┦┦┩┩┩┩┩┩╃╃╃╃╃╃╃╃╃╃╃╃╃╃╃╃╃╃╃╃╃╃╃╃╃╃╃╃╃╃</u>	- -	Calcos) Calcium Calcium Raw Ozon, Fitt	-		$\!$				If blend	
<u>                                     </u>	$\coprod$	FI.		Ш	$\coprod$			_ 6	nd prop	
100 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		R						in Ca	4. If biended source water indicata sources and proportions:	
		Ozon.	Bramide						ndicata	
12 444		Fit						×		
100 100 100 100 100 100 100 100 100 100	i e	77	$\prod$				П			
	-	Ozen.	C.		$\dagger \dagger$	$\dag \dag$	$\parallel \parallel$	-	$\parallel \parallel$	$\parallel$
<del>╏┊╤╤╒╒╏╒╏╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒</del>	╫	1 2	9	$\mathbb{H}$	$\dashv \vdash$	╂╂	-	-	-	+
		景	#		$\prod$			-		$\prod$
86000 860000 860000 860000 860000 86000 86000 86000 86000 86000 86000 86000 86000 86000		Ray Q	= -	$  \cdot  $	#	-	-	-	-	$\perp \mid$
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	-	Ozon. FIIL	Pid IIV	H		-	-	-	-	$\dashv \downarrow$
8 9 9 9 9 8 8 9 9 9 9 9 9 9 9 9 9 9 9 9	18	<u> </u>	Ш	Ш	Ш.	Ц	Щ	Ш	Ш	Ш

Page 1 of 2

: -03105

preazon

172/05 1/1/095 1/1/095 1/2/495 1/2/495 1/3/195 2/1/05 2/2/195 2/2/195 2/2/195 3/2/05 3/2/05 3/2/05 4/2/05 4/2/05 4/2/05 4/2/05 4/2/05 5/2/05 5/2/05	7.7 7.8 8.0 8.0 7.9 7.9 8.0 7.9 8.0 7.9 8.0 7.9 8.0 7.9 8.0 8.0 7.9 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0	pH J) Dzon	7.0 67 7.0 6.9 7.1 7.2 7.2 7.1	Rew 8.6 10.8 11.3 11.6 12.3 10.2 10.0 11.2 12.		Fix.		Bromstein (pp. 1) Ozon.		Rew	TTHM (ygrL)			tion By HAAS (1991)			HAAS (pg/L) Ozen.	Fit.	Ozone dase (mg/L)	Ozone Condi Ozone (mg/L)	l ation Conc	Ozone pH ()	Ozone temp. (deg. C) 8 8
1. Study ID: 2. Source W 3. Source W 4. Describer Indicate W 4. Describer Indicate W 4. Describer Indicate W 5. Describer Indicate W 5. Describer Indicate W 5. Describer Indicate W 6. Describer Indicate W 6. Describer Indicate W 6. Transfer Indicate W	7.7   7.8   8.0   7.9   8.0   7.9   8.0   7.9   8.1   8.1   8.2   8.6   8.5   8.5   8.5   8.5   8.4   8.4	()	7.0 67 70 7.0 69 68 69 71 74 7.2	Rsw 8.6 10.8 11.3 11.6 11.6 12.3 10.2 10.0 11.2	(deg. C)			(Pg/L)		Raw	TTHM (pgr.)	Filt.		HAA5 (µg/L)			(µg/L)	Fit.	Ozone dase (mg/L)	Ozone Ozone residual (mg/L)	ation Cons Contact time	Ozone pH ()	temp. (deg. C)
2. Source w 3. Source w 4. Source w 4. Describe indicate w 5. Describe indicate w 4. Indicate 5. Indicate 5. Indicate 7. Indic	7.7   7.8   8.0   7.9   8.0   7.9   8.0   7.9   8.1   8.1   8.2   8.6   8.5   8.5   8.5   8.5   8.4   8.4	()	7.0 67 70 7.0 69 68 69 71 74 7.2	Rsw 8.6 10.8 11.3 11.6 11.6 12.3 10.2 10.0 11.2	(deg. C)			(Pg/L)		Raw	TTHM (pgr.)	Filt.		HAA5 (µg/L)			(µg/L)	Fin.	Ozone dase (mg/L)	Ozone Ozone residual (mg/L)	ation Cons Contact time	Ozone pH ()	temp. (deg. C)
1. Bouros w 1. Bouros w 2. Describe indicate w 1. Indicate w VATER QU Date Date VATER QU 1/1/05 1/1/	7.7   7.8   8.0   7.9   8.0   7.9   8.0   7.9   8.1   8.1   8.2   8.6   8.5   8.5   8.5   8.5   8.4   8.4	()	7.0 67 70 7.0 69 68 69 71 74 7.2	Rsw 8.6 10.8 11.3 11.6 11.6 12.3 10.2 10.0 11.2	(deg. C)			(Pg/L)		Raw	TTHM (pgr.)	Filt.		HAA5 (µg/L)			(µg/L)	Fin.	Ozone dase (mg/L)	Ozone Ozone residual (mg/L)	ation Cons Contact time	Ozone pH ()	temp. (deg. C)
1. Bouros w 1. Bouros w 2. Describe indicate w 1. Indicate w VATER QU Date Date VATER QU 1/1/05 1/1/	7.7   7.8   8.0   7.9   8.0   7.9   8.0   7.9   8.1   8.1   8.2   8.6   8.5   8.5   8.5   8.5   8.4   8.4	()	7.0 67 70 7.0 69 68 69 71 74 7.2	Rsw 8.6 10.8 11.3 11.6 11.6 12.3 10.2 10.0 11.2	(deg. C)			(Pg/L)		Raw	TTHM (pgr.)	Filt.		HAA5 (µg/L)			(µg/L)	Fitt.	Ozone dase (mg/L)	Ozone Ozone residual (mg/L)	ation Cons Contact time	Ozone pH ()	temp. (deg. C)
5. Describe: Indicate will indicate will be an indicate will be applied with will indicate will be an	7.7   7.8   8.0   7.9   8.0   7.9   8.0   7.9   8.1   8.1   8.2   8.6   8.5   8.5   8.5   8.5   8.4   8.4	()	7.0 67 70 7.0 69 68 69 71 74 7.2	Rsw 8.6 10.8 11.3 11.6 11.6 12.3 10.2 10.0 11.2	(deg. C)			(Pg/L)		Raw	TTHM (pgr.)	Filt.		HAA5 (µg/L)			(µg/L)	Fit.	Ozone dase (mg/L)	Ozone Ozone residual (mg/L)	ation Cons Contact time	Ozone pH ()	temp. (deg. C)
5. Describe: Indicate will indicate will be an indicate will be applied with will indicate will be an	7.7   7.8   8.0   7.9   8.0   7.9   8.0   7.9   8.1   8.1   8.2   8.6   8.5   8.5   8.5   8.5   8.4   8.4	()	7.0 67 70 7.0 69 68 69 71 74 7.2	Rsw 8.6 10.8 11.3 11.6 11.6 12.3 10.2 10.0 11.2	(deg. C)			(Pg/L)		Raw	TTHM (pgr.)	Filt.		HAA5 (µg/L)			(µg/L)	Fit.	Ozone dase (mg/L)	Ozone Ozone residual (mg/L)	ation Cons Contact time	Ozone pH ()	temp. (deg. C)
Indicate wi  Indicate wi  Indicate wi  VATER QUI  Date  \$1,005 1,1005 1,1005 1,1005 1,1005 2,	7.7   7.8   8.0   7.9   8.0   7.9   8.0   7.9   8.1   8.1   8.2   8.6   8.5   8.5   8.5   8.5   8.4   8.4	()	7.0 67 70 7.0 69 68 69 71 74 7.2	Rsw 8.6 10.8 11.3 11.6 11.6 12.3 10.2 10.0 11.2	(deg. C)			(Pg/L)		Raw	TTHM (pgr.)	Filt.		HAA5 (µg/L)			(µg/L)	Fin.	Ozone dase (mg/L)	Ozone Ozone residual (mg/L)	ation Cons Contact time	Ozone pH ()	temp. (deg. C)
Indicate wi  Indicate wi  Indicate wi  VATER QUI  Date  \$1,005 1,1005 1,1005 1,1005 1,1005 2,	7.7   7.8   8.0   7.9   8.0   7.9   8.0   7.9   8.1   8.1   8.2   8.6   8.5   8.5   8.5   8.5   8.4   8.4	()	7.0 67 70 7.0 69 68 69 71 74 7.2	Rsw 8.6 10.8 11.3 11.6 11.6 12.3 10.2 10.0 11.2	(deg. C)			(Pg/L)		Raw	(µg/L)	7.8		HAA5 (µg/L)			(µg/L)	Fin.	Ozone dase (mg/L)	Ozone Ozone residual (mg/L)	ation Cons Contact time	Ozone pH ()	temp. (deg. C)
VATER QU  Date  1/1/05	7.7   7.8   8.0   7.9   8.0   7.9   8.0   7.9   8.1   8.1   8.2   8.6   8.5   8.5   8.5   8.5   8.4   8.4	()	7.0 67 70 7.0 69 68 69 71 74 7.2	Rsw 8.6 10.8 11.3 11.6 11.6 12.3 10.2 10.0 11.2	(deg. C)			(Pg/L)		Raw	(µg/L)	7.8		HAA5 (µg/L)			(µg/L)	Fit.	Ozone dase (mg/L)	Ozone Ozone residual (mg/L)	ation Cons Contact time	Ozone pH ()	temp. (deg. C)
VATER OU  Date  1/2/05 1/1/095 1/1/095 1/1/095 1/2/095 1/2/095 2/2/095 2/2/095 2/2/095 3/2/095 3/2/095 4/1/095 4/2/095 4/2/095 4/2/095 4/2/095 4/2/095 5/2/095	7.7   7.8   8.0   7.9   8.0   7.9   8.0   7.9   8.1   8.1   8.2   8.6   8.5   8.5   8.5   8.5   8.4   8.4	()	7.0 67 70 7.0 69 68 69 71 74 7.2	Rsw 8.6 10.8 11.3 11.6 11.6 12.3 10.2 10.0 11.2	(deg. C)			(Pg/L)		Raw	(µg/L)	7.8		HAA5 (µg/L)			(µg/L)	Fin.	Ozone dase (mg/L)	Ozone Ozone residual (mg/L)	ation Cons Contact time	Ozone pH ()	temp. (deg. C)
VATER OU  Date  1/2/05 1/1/095 1/1/095 1/1/095 1/2/095 1/2/095 2/2/095 2/2/095 2/2/095 3/2/095 3/2/095 4/1/095 4/2/095 4/2/095 4/2/095 4/2/095 4/2/095 5/2/095	7.7   7.8   8.0   7.9   8.0   7.9   8.0   7.9   8.1   8.1   8.2   8.6   8.5   8.5   8.5   8.5   8.4   8.4	()	7.0 67 70 7.0 69 68 69 71 74 7.2	Rsw 8.6 10.8 11.3 11.6 11.6 12.3 10.2 10.0 11.2	(deg. C)			(Pg/L)		Raw	(µg/L)	7.8		HAA5 (µg/L)			(µg/L)	Fin.	Ozone dase (mg/L)	Ozone Ozone residual (mg/L)	ation Cons Contact time	Ozone pH ()	temp. (deg. C)
170/95 1/10/05	7.7   7.8   8.0   7.9   8.0   7.9   8.0   7.9   8.1   8.1   8.2   8.6   8.5   8.5   8.5   8.5   8.4   8.4	()	7.0 67 70 7.0 69 68 69 71 74 7.2	Rsw 8.6 10.8 11.3 11.6 11.6 12.3 10.2 10.0 11.2	(deg. C)			(Pg/L)		Raw	(µg/L)	7.8		HAA5 (µg/L)			(µg/L)	Fin.	Ozone dase (mg/L)	Ozone Ozone residual (mg/L)	ation Cons Contact time	Ozone pH ()	temp. (deg. C)
170/95 1/10/05	7.7   7.8   8.0   7.9   8.0   7.9   8.0   7.9   8.1   8.1   8.2   8.6   8.5   8.5   8.5   8.5   8.4   8.4	()	7.0 67 70 7.0 69 68 69 71 74 7.2	Rsw 8.6 10.8 11.3 11.6 11.6 12.3 10.2 10.0 11.2	(deg. C)			(Pg/L)		Raw	(µg/L)	7.8		HAA5 (µg/L)			(µg/L)	Filt.	Ozone dase (mg/L)	Ozone Ozone residual (mg/L)	ation Cons Contact time	Ozone pH ()	temp. (deg. C)
5/2/05. 1/1/075. 1/1/075. 1/1/075. 1/1/075. 1/2/075. 1/2/075. 2/1/075. 2/1/075. 2/1/075. 3/1/075. 3/1/075. 3/1/075. 3/1/075. 4/1/075. 4/1/075. 4/1/075. 4/1/075. 4/1/075. 4/1/075. 5/2/075. 5/2/075. 5/2/075.	7.7   7.8   8.0   7.9   8.0   7.9   8.0   7.9   8.1   8.1   8.2   8.6   8.5   8.5   8.5   8.5   8.4   8.4	()	7.0 67 70 7.0 69 68 69 71 74 7.2	Rsw 8.6 10.8 11.3 11.6 11.6 12.3 10.2 10.0 11.2	(deg. C)			(Pg/L)		Raw	(µg/L)	7.8		HAA5 (µg/L)			(µg/L)	Filt.	dase (mg/L)	Ozone residual (mg/L)	Contact	Ozone pH ()	temp. (deg. C)
5/2/05. 1/1/075. 1/1/075. 1/1/075. 1/1/075. 1/2/075. 1/2/075. 2/1/075. 2/1/075. 2/1/075. 3/1/075. 3/1/075. 3/1/075. 3/1/075. 4/1/075. 4/1/075. 4/1/075. 4/1/075. 4/1/075. 4/1/075. 5/2/075. 5/2/075. 5/2/075.	7.7   7.8   8.0   7.9   8.0   7.9   8.0   7.9   8.1   8.1   8.2   8.6   8.5   8.5   8.5   8.5   8.4   8.4	()	7.0 67 70 7.0 69 68 69 71 74 7.2	Rsw 8.6 10.8 11.3 11.6 11.6 12.3 10.2 10.0 11.2	(deg. C)			(Pg/L)		Raw	(µg/L)	7.8		HAA5 (µg/L)			(µg/L)	Fitt.	dase (mg/L)	Ozone residual (mg/L)	Contact	Ozone pH ()	temp. (deg. C)
172/05 1/1/095 1/1/095 1/2/495 1/2/495 1/3/195 2/1/05 2/2/195 2/2/195 2/2/195 3/2/05 3/2/05 3/2/05 4/2/05 4/2/05 4/2/05 4/2/05 4/2/05 5/2/05 5/2/05	7.7   7.8   8.0   7.9   8.0   7.9   8.0   7.9   8.1   8.1   8.2   8.6   8.5   8.5   8.5   8.5   8.4   8.4		7.0 67 70 7.0 69 68 69 71 74 7.2	8.6 10.8 11.3 11.6 11.6 12.3 10.2 10.0	Ozpn	Fiit.	Raw	Ozon.	Fin,	Raw	(µg/L)	7.8	Raw		Fin.	Raw	(µg/L) Ozen.	Fin.	dase (mg/L)	(mg/L)	time	) pH () 8.1	(deg. C)
1/10/05 1/17/05 1/2/05 1/3/05 1/3/05 2/14/05 2/14/05 2/2/05 2/2/05 2/2/05 3/2/05 3/2/05 4/4/05 4/15/05 4/15/05 5/2/05 5/2/05 5/2/05 5/2/05 5/2/05	7.8   8.0   7.9   8.0   7.9   8.0   7.9   8.4   8.1   8.2   8.6   8.5   8.6   8.3   8.4		57 70 7.0 59 58 5.0 71 74 7.2	10.8 11.3 11.6 11.6 12.3 10.2 10.0 11.2						Raw	Ozen.	7.8	Raw	Ozon.	Fin.	Raw	Ozon.	Fift			(min)	8.1	8.8
1/10/05 1/17/05 1/2/05 1/3/05 1/3/05 2/14/05 2/14/05 2/2/05 2/2/05 2/2/05 3/2/05 3/2/05 4/4/05 4/15/05 4/15/05 5/2/05 5/2/05 5/2/05 5/2/05 5/2/05	7.8   8.0   7.9   8.0   7.9   8.0   7.9   8.4   8.1   8.2   8.6   8.5   8.6   8.3   8.4		57 70 7.0 59 58 5.0 71 74 7.2	10.8 11.3 11.6 11.6 12.3 10.2 10.0 11.2													1 1			0.40	<del> </del>		
1/10/05 1/17/05 1/2/05 1/3/05 1/3/05 2/14/05 2/14/05 2/2/05 2/2/05 2/2/05 3/2/05 3/2/05 4/4/05 4/15/05 4/15/05 5/2/05 5/2/05 5/2/05 5/2/05 5/2/05	7.8   8.0   7.9   8.0   7.9   8.0   7.9   8.4   8.1   8.2   8.6   8.5   8.6   8.3   8.4		57 70 7.0 59 58 5.0 71 74 7.2	10.8 11.3 11.6 11.6 12.3 10.2 10.0 11.2									1										
1/17/95 1/24/95 1/24/95 1/3/195 2/1/95 2/14/95 2/24/95 3/7/95 3/14/95 3/24/95 4/14/95 4/14/95 4/14/95 4/14/95 4/14/95 5/2/95 5/2/95	80 80 79 79 80 79 84 81 61 82 86 85 86 83		7 0 7.0 6 9 6 8 6.0 7 1 7 4 7.2	11.3 11.6 11.6 12.3 10.2 10.0 11.2										<del></del>	- 8		<del>  </del>	5	2.2	0 64			10.6
1/24/95 1/31/95 1/31/95 2/14/95 2/21/95 2/21/95 3/7/95 3/4/95 3/21/95 4/4/95 4/15/95 4/15/95 5/2/95 5/2/95	8.0 7.9 7.9 8.0 7.9 8.4 8.1 8.1 8.2 8.0 8.5 8.6 8.6 8.3		7.0 69 68 6.5 71 74 7.2 71	11.6 11.6 12.3 10.2 10.0 11.2								4.2			- 6		-		1.7	0.44	<del> </del>	8.2	113
1/31/95 2/7/95 2/14/95 2/21/95 2/21/95 2/21/95 3/7/95 3/14/95 3/21/95 3/21/95 4/11/95 4/11/95 4/11/95 5/2/95 5/2/95	7 9 7 9 8 0 7 9 8 4 8 1 8 1 8 1 8 2 8 0 8 5 1 8 6 8 3 5 4 1		5 8 5.5 7 1 7 4 7.2 7 1	11.6 12.3 10.2 10.0 11.2								48						4	1.8	0 40		8.5	11.6
2/14/95 2/21/95 2/21/95 2/28/95 3/7/95 3/14/95 3/21/95 4/21/95 4/11/95 4/11/95 4/15/95 5/2/95 5/2/95	80   79   54   81   81   81   82   80   8.5   8.6   8.3   8.4   5		7 1 7 4 7.2 7 1	10.2 10.0 11.2								4.4						5	20	0.37		8.6	11.5
2/21/95 2/28/95 3/7/95 3/7/95 3/21/95 3/21/95 4/4/95 4/11/95 4/11/95 4/25/95 5/2/95 5/2/95	7 9   8 4   8 1   6 1   8 2   8 0   8 5   8 6   8 3   8 4   f		71 74 7.2 71	10.0			, ,					4.6						5	3.5	0.91		8.3	12.3
2/28/95   3/7/95   3/7/95   3/7/95   3/2/95   3/2/95   3/2/95   4/2/95   4/1/95   4/1/95   4/1/95   4/25/95   5/2/95   5/2/95   5/9/95   5/9/95	84 81 81 82 80 85 86 83 84		7.2	11.2							<del>  </del>	5.1	<del> </del>		- 5			- 6	3.2	0.63		8.2	10 0
3/7/95 3/14/95 3/21/95 3/28/95 4/4/95 4/11/95 4/11/95 4/18/95 4/25/95 5/2/95 5/9/95	81 81 82 80 85 86 83 84		7.2				-					5.1			6		$\overline{}$	7	3.8	0.66	<del></del>	8.2	11.2
3/21/95 3/28/95 4/4/95 4/11/95 4/18/95 4/18/95 5/2/95 5/9/95	8.2 8.0 8.5 8.6 8.3																	18	3 8	0,66		7.6	120
3/28/95 4/4/95 4/11/95 4/18/95 4/25/95 5/2/95 5/9/95	8 0 8 5 8 6 8 3 8 4		7 .	115								3.5			3			-6	3.7	0.74		7.1	11.5
4/4/05   4/11/95   4/18/95   4/25/95   5/2/95   5/9/05	8.5   8.6   8.3   8.4			12.0	<u> </u>				60			4.8						4	3 7	0.69		73	120
4/11/95 4/18/95 4/25/95 5/2/95 5/9/95	8.6 8.3 8.4 I		70	11.2					100			3.8			-4			3	3.8	28.0		74	11 2
4/18/95 4/25/95 5/2/95 5/9/95	83	<del></del>	7.1	15 3					120			82 8 i			- 6			3	3.0	0.73		7.5	153
4/25/95 5/2/95 5/9/95	84 1	<del></del>	70	14 1					90		-	49						3	47	0.59		7.8	14 1
5/9/95			71!	15.5					80			65		1				2	3.8	0.52		74	15.5
	82		72	15 7							1	54							3.5	0.55		7.2	15 7
24 105 8 2 1	7.6	-+	68	16 1								13.3							39	0 60		7.5	16.5
5/23/951	77 1	<del></del>	6.6	18.D								51 1		<del></del>		<del>i</del>			36	D.83		78	18.0
5/30/95	7.3	$\overline{}$	6.6	19.3								50				-			4.2	0.52		77	19.3
	6.9		62	190		1						51							3.3	0.59		74	19 0
	74	1	65	19.2								50 (							3.6	0.60		77	19.2
	7.5		6.6	19 1					60			47			3				3 8	0.69		7 6	19 1
	78	<del></del>	66	24.9	<del></del>	<del></del>			80			5.5							3.3	0.81 0.47		7.3 8.0	24.9
7/11/95	7.2		63	22.7	<del></del>	<del>i</del>				<del>i</del>		5.3			2				4.2	061		80	22.7
	74		63	23 2					10.0			41	- 1						41	0.52		7.5	23 2
	7.5		64						50 1			43			3 (				4.2	0 42		5.9	21 €
	7.6	<del>-</del> i	6.2	25 9					90			6.2		<del></del> !		!			2.0	0 30		69	25 9
	77	<del></del>	5.5	24 5		<del></del>		+	70 1			38 1			3		<del></del>		41	0 53		7.6	24.5
	77 1	<del></del>	63	24.4					100			30			77 1				2.2	0.28		75	
	76		66	22.0					10.0					1								7.6	22.0
	73 !		6.6	21 6				<5	110			3.3			10		1	14	2.2	0.94		77 1	21.5
	8.0		89 1	194	!	!		6.0	15.0			32.8							41	1.20		7.6	19 4
	7.5		7.0	19 9				21 0 I	14.0 1			13.8			4		<del></del> i	- 6	6.5 3.1	1.00		77	21 1 19 5
	69	<del></del>	69	17 8			+		50			E 1		-+	4 ;			5	27	0.82		78	17.8
10/10/95	8.9		6.9 1	16 8				<5	<5			5.8							2.€	0.76		77	16.8
	76			17 1 ;				9.0	<5			=							2.8	0.56		8.1	17 1
	74	<del></del>	89			!	+	<b>&lt;</b> 5	<5		1	-, -							3.0	0.77		7.5 7.5	16.7 16.6
	75	-+	6.9	15.6				<5 <5	<5 <5		<del>  </del>	5.2		-+	3				3.0	0.67		7.5	15.4
	77	<del></del> i	5 E	15.0			-	<5	<b>&lt;</b> 5		-	- v.e			4	-		5	30	0.78		7.7	15 0
11/21/95	7.6		5.9	15.0				<5	<5										2.9	0.81		7 8	15 0
	8.1		67	14.5				14 0	<b>&lt;</b> 5		L J	3.0	<u> </u>		4		+	5	35 !	0.65		7.8	14 6
12/12/95	77		7.2	13.5				<5 <5	₹5		-	6.2			5			- 6	2.3	0.65		7.9 7.5	14.5
	7.7		69 [	11 8	<del></del>			<6	<5					<del></del>	2			3	2.1	0.50		7.9	11 8
1/2/96	81 (		69	12.6			i	<5	60			4.6							2.1	0 48		7.7	12.6
1/9/96 !	75		86	11.2				<5	60			5.8			5			7	3.5	0 46		8.2	11.2
1/16/98	7.5		6.6	10.8		]		⋖5	<5			12.2	1						3.6	0.50		78	10.8
	7.6		5.3	10 2					5.0		<del>  </del>	32.9							3.7	0.79		8,1 8.2	10.2
	7.8	<del></del>	7.0	11.6					-+			5.6				{			31	0.54		8.5	11.6
2/13/95	7.8		7.0	118								5.2					$=$ $\dagger$		2.5	0.50		8.1	11.8
	7.9		5.9	12.3				<5 ∶								$\Box$			41			8.3	12.3
3/19/961			70	127	!	!		<6	<5		<u> </u>	67			_5			- 6	3.0			7.5 7.5	12 7
	7.7		64	13.2				<5	<b>&lt;</b> 5			54			3				3.4			74	13.2 15.3
	8.2	<del></del>	5.9	16.3					15.0		<del></del>	2.9			-				4.0	0.79		7.5	15.3
4/16/96	7.8		7.0	16.3				8.5							2			3	3.8	D 83		77	16 3
4/23/96	81		6.9	170				80				2.8							3.8	0.66			17.0
4/30/95	8.2		6.7	19.1					12.0			1.3			3			4	3.6	0.75			19 1
5/7/96	8.5		5.9	19.8		ļi	<del>}</del>	18.5				2.6 5.8	$\vdash$		2		<del>}</del>	3	3.8	0.54	<del></del>	<del> </del>	19.3
5/21/96	8.3	<del></del>	7.0	17.7	<del></del>	·		13.5	25 0 22 0			J 5	_						3.0	0.89	<del>                                     </del>		17.7
5/28/961	7.5		67	17.8				€4.5		_		3 1			2			3	2.7	0.51			17.8
6/4/96	7.6		6.4	24.0				12.57	€4.5			2.3							2.6	0.54			24 0
6/11/96	74		5.5	22.6				e4 5	<b>44</b> 5		$\vdash$	24			_1_			2	2.5	0.31			22.5
5/18/96   5/25/96	75		7.0	21 4	ļ	<del> </del>		44.5	<4.5	-	-	1.6	<u> </u>						26	0.35	<del> </del>	$\vdash$	21.4

16.1	9	1-	3 2.02	8.6833				108		78	2.70	3 40	5.1		
15.7	3	+	-+	10.783				126		105	320	3 50	53		
15.5	5	-	-	11.55				1100		88	3.10	3.70	5.8		
14.6	7	$\dashv$	7 2.18	8.9667				124		87	2.90	3.60	5.6		
15	Ġ,	39 8.6	-	13.633				116		96	3.50	8.8	5.9		
11.9		-	7 4.98	76.667				134		117		3.30	6.1		
12.4	ω			21.233				120		102	2.80	3.30	5.8		
12.5	2	-		17.117				1		110	3.00	3.50	б. 1		
11.3	-1			8.2833				134		127	3.50	4.10	5.8		
11.1	4		3 2.98	11.933				Ť		158	3.50	4.20	5.6		
10	9	$\dashv$		24.333				142	-	152	3.40	3.70	5.8		
19.9	8	$\vdash$	-	2.1167				ī		128	2.60	2 60	3.6		
19.1	B	-		2.1667				150		127	2.80	2.80	4.0		
17.3	6	-	-	4.65				120		112	2.40	3.10	3.7		
20.3			-	6.0167				118		105		2 40	3.1		
21.2	7	┢	_	11.5				132		104		2.00	3.2		
16.1	9	-	-	8,6833				108		78	2.8	3.7	υ 		
15.7	ω	8.3	<del> </del>	10.783				126		105	3.4	3.7	5.3	_	
15.5	5	├	├~	11.55				118		98	3.5	4.2	5.8		
14.6	7		1-	8.9667				124		87	3.1	4.0	5.6		
15	6	7 8.6	┝	13.633				116		96	3.6	4.3	5.9		
11.9			-	76,667				134		117		3.3	6.1		
12.4	3			21.233				120		102	2.9	3.6	5.8		
12.5	2	9 8.2	7 3.9	17,117				144		110	3.2	3.8	6.1		
11.3	_1	-	_	8.2833				134		127	3.7	4	5.8		
11.1	4	-	3 44	11.933				144		158	3.7	4.2	5.6		
10	8		-	24.333				142		152	3.4	4.0	5.8		
19.9	80	3 7.9	7 2.3	2.1167				144		128	2.5	2.6	3.6		
19.1	9	-		2,1667				150		127	2.8	2.7	4.0		
17.3	on	-	-1	4.65				120		112	2.4	2.8	3.7		
20.3	_	-	-†	6.0167				118		105		2.1	3.1		,
21.2	7	2   7.7		11.5				132		104	- 1		3.2		
		) Ted	(settled)							$\int$	<u>a</u>	(settled)			
+	-	-+			Raw Filt	Raw	=======================================	Raw							
Raw Filt	-	Ruk	E F	Raw	3	Cal.	2	3	F) +	Raw of	<u> </u>	=	Z)		
(deg. C)	<b>=</b>	1	Z	2		3003)	(mg/L as CaCO3)		s CaCO3)	(mg/L a		(mg/L)			10000
Temperatura		+			-		Harring -		Alkalinity	<u> </u>		7		1	
		+	+	T						NAL	CONVENTIONAL		DA CA	WAIR COACIT DATA:	VAL HAN
	×	-	1	Jon:	TRAIN DI	attacon W	er secumen	OF AITE					7		
	×	-	+		VIIIV:	nontation	ter sedim	samples collected after sedimentation only:	n samples (	are fron	7117	e petrode	IT CALL IL	b. Indicate with an X if data reported as "Filt" are from	b. Indicate
		-	+												
		-	-					filtration.		i e	Full-scale	×			
		Ë	n, and	entatio.	flocculation, sedimentation, and	occulatio	ulation, fic	after coagulation,		ale	Pilot-scale			th an 'X')	(indicate with an 'X')
		_	ted	a collec	rs to dat	-it. rate	a sheet, "F	in this data sheet, "Filt." refers to data collected		scale	Bench-scale		udy:	5. Describe level of study:	5. Describe
			H	-											
		_	۲	of, etc.)	r, blend o	ject wate	(State Project water, blend of,		queduct	South Bay Aqueduct	Sol			rater ID:	3. Source water ID:
			-												
		+	$\dashv$	្យ	dwater, et	(e, ground	(River, lake, groundwater, etc.)		٦	River				Pater	2. Source water:
		+	$\dashv$	-											
	-	+	+	라	∨ 9/95 et	tion Stud	(Optimization Study 9/95, etc.)	/ data)	Enh. Coagulation (from EC study data)	lation (fro	Coagu	E			1. Study ID:
+	+	+	-				1					1	1	1	, :-
		=		S	BMUD M	CWD. F	(ACWD, CCWD, EBMUD, MWD, SCVWD)		ð	ACWD			_	_	Utility ID:

Page 1 of 2

		Ţ		· · · · · · · · · · · · · · · · · · ·				.,		
			<del> </del>	<u> </u>	<del> </del>	<u> </u>	<u> </u>	<u> </u>	-	<u> </u>
										ļ
			<b>_</b>					1		
										<u></u>
								<u> </u>	<u> </u>	
			<u> </u>				ļ			
		<u> </u>			Indicate coag			<u> </u>	}	1
					Ð	_		al formula	Units	
					1	Alum	Al <sub>2</sub> (SO <sub>4</sub>	)3*14 H2O	mg/L	
					2	Ferric	FeCi,	*6 H <sub>2</sub> O	mg/L	
					3					1
					4					1
								1		
			1	1	TREATME	NT CONDIT	IONS			
			<del> </del>	<del> </del>			1	<del> </del>	<del> </del>	<del> </del>
C12		Disinfection	n By-produc		<del> </del>	Cosquis	tion Condition	\ne	<u></u>	1
Conditions	77	НМ	Jii Dy-produc	HAA5	Coaguiant	Dose	Acid	Base	Coag.	Coag.
Chlorine		7/L)	<del> </del>	(µg/L)	ID	2004	adjusted?	adjusted?	pH	temp.
dose	Raw	Filt.	Raw	Filt	(see above)		(Y/N)	(Y/N)	0	(deg. C
(mg Cl2/L)		<del> </del>			1,332,332,0		,,	,,	·······	,
2.34		9	1	6	1	25.1	<del> </del>	<del> </del>		
2.40		8	ļ —	6	1 1	11.8				
2.60		8	1	4	1	11.6				
2.35		9	<del> </del>	5	1 1	12.8				
2.20		8		6	1	12.5				
1.43		5	1	5	1	28				
1.57		5		6	1	21.3				
1.49		5		5	1	18.8				
1.32		4		3	1	40				
1.10		5		4	1	31.1				
1.47		4		4	1	29.4				
1 47		8		6	1 1	24				:
1,54		5		4	1 1	25				
1.60		7		7	1	23.1				
1.90		5		5	1	21.2				
2.00		13		4	1	21				
2.34		9.0		6.0	2	11.2				
2 40		7.6	1	6.0	2	11.1				
2.60		8.0	<u> </u>	4.0	2	8.1				
2.35		8.7	<del> </del>	5.0	2	15.9				
220 1				1 40	2	9.2		1		
2.20		7.8	<u> </u>	6.0						
1 43		4.8		5.0	2	16				
1.57		4.8 5.1		5.0	2 2	16 13.5				
1 43 1.57 1 49		4.8 5.1 5.0		5 0 6.0 5.0	2 2 2	16 13.5 10.2				
1 43 1.57 1 49 1.32		4.8 5.1 5.0 3.6		5 0 6.0 5.0 3.0	2 2 2 2 2	16 13.5 10.2 23.8				
1 43 1.57 1 49 1.32 1.10		4.8 5.1 5.0 3.6 4.8		5 0 6.0 5.0 3.0 4.0	2 2 2 2 2 2	16 13.5 10.2 23.8 13.6				
1 43 1.57 1 49 1.32 1.10		4.8 5.1 5.0 3.6 4.8 3.8		5 0 6 0 5 0 3 0 4 0 4 0	2 2 2 2 2 2 2	16 13.5 10.2 23.8 13.6 26.1				
1 43 1.57 1 49 1.32 1.10 1.47		4.8 5.1 5.0 3.6 4.8 3.8 8.3		5 0 6.0 5.0 3.0 4.0 4.0 6.0	2 2 2 2 2 2 2 2 2	16 13.5 10.2 23.8 13.6 26.1 16.7				
1 43 1.57 1 49 1.32 1.10 1.47 1.47		4.8 5.1 5.0 3.6 4.8 3.8 8.3 4.9		5 0 6.0 5.0 3.0 4.0 4.0 6.0	2 2 2 2 2 2 2 2 2 2	16 13.5 10.2 23.8 13.6 26.1 16.7 18.5				
1 43 1.57 1 49 1.32 1.10 1.47		4.8 5.1 5.0 3.6 4.8 3.8 8.3		5 0 6.0 5.0 3.0 4.0 4.0 6.0	2 2 2 2 2 2 2 2 2	16 13.5 10.2 23.8 13.6 26.1 16.7				

Utility ID:			L	CC	WD: Bo	liman WTP	1	(ACWD,	CCWD, E	BMUD, N	AWD, SC	(DWC											T
1, Study ID:	<u>!</u>			Historic	al data	 7/1/95-6/30	96	(Onlimiza	tion Study	/ 0/05 at			<del> </del>		4. H bler	J.J.			Ļ				
1. Siddy io.	<del>i</del> -	<del> </del>	<b> </b>	1 11310110	T COIG	177755 0150	1	COprimize	1000000	333, 81	J.,	<del> </del>		<del></del>	Sources				a toe	<u> </u>	<u> </u>		
2. Source w	ater:		De	elta - Mai	llard Slo	ough/Rock S	lough	(River la	ke, ground	water et	c )		<del> </del>	<del> </del>	Sources	Sou		<u> </u>	<del></del>				
				T	<u> </u>	1	1	(******		1	<u> </u>			<del> </del>	<del> </del>	300	1	<del></del>	*	<b> </b>			ļ
3. Source w	rater ID:			Centra	Valley	Project Wat	er	(State Pro	ect wate	r, blend o	(, etc.)								<u> </u>				
. Describe	level of s	tudy:		Bench-	-scale	<b> </b>	in this dat	a sheet, "	Filt." refe	rs to dat	a collect	led											
Indicate wi	th an 'X')			Pilot-se	cale		after coag	ulation, f	occulatio	n, sedim	entation	, and			<b>!</b>				<del> </del>	<u> </u>	<del>  </del>		
	·		X	Full-sc	ale		filtration.			<u> </u>		·			1				<b> </b>				
			1																				<del> </del>
6. Indicate v	with an 'X'	if data r	eported	as "Fift	" are fr	om sample													<del> </del>				<del> </del>
							or aft	er sedim	entation a	ind filtrat	lon:		X										<b></b> -
WATER Q	UALITY	DATA:	CONV	ENTIC	NAL																		<del> </del>
	<del></del>		) OC		-254	A 11.	1114			<u> </u>													
Date	Time		g/L)		:m)		linity CaCO3)		Hardi (mg/L as				nide		nonia		oride		DS		idity	pl	H
		Raw	Fift	Raw	Fift.	Raw	Filt.		tai	Calc	l	Raw	<u>/L)</u>		H3-N/L)	(mg			g/L)		ru)		)
		RAN	71111	17414	FIIL	NAM	r itt.	Raw	Filt.	Raw	Filt	Raw	Fift.	Raw	Filt.	Raw	Fift,	Raw	Fift.	Raw	Filt.	Raw	Fift
			l	<b></b>																			
Jul-95						43.9	44.4	47.B	47.9			<0.1	<0.1	<0.1	0.32	21.3	21.3	90	120		0.05	7.8	
Aug-95						42.3	42	47.1	46.6				<0.1			20.3	21.3		115	2.4	0.05	8.1	3
Sep-95					<b></b>	47.2	48.3	48.4	47.9				<0.1			16.1	16.3		110	2.4	0.05	8	
Oct-95						52.4	54.2	53.1	54.8			<0.1	<0.1	<0.1	0.25	17.7	18	90			0.05	8.2	
Nov-95					ļ	52.3	51.7	55.1	55.4				<0.1			20	20.4		120	5	0.05	8.4	8
Dec-95			ļ	li		54.7 63.2	55.5	62	61.3				<0.1			22.3	22.4		130	5.7	0.05	8	
Jan-96 Feb-96			<b> </b>			67.7	60.5 67.4	71.8 78	71.5 75.7	<del>  </del>		<0.1	<0.1	<0.1	0.28	29.6	29.8	130			0.05	8.5	
Mar-96				<del>  </del>		64.5	63.8	77.5	76.3	<b>  </b>		L	<0.1		II	33.5	32		195	5.1	0.05	7.8	8
Apr-96				<del> </del>		63.8	64.3	84.3	82			<0.1	<0.1	-0.4		34.3	34.3		195	5.5		8	
May-96				<del>  </del>		62.5	62.4	88.2	88.8			₹U. I	<0.1	<0.1	0.18	36.9	37.5	160		5	0.05	8	8
Jun-96						54.6	55.8	71.5	73.8				<0.1		<del></del>	44.8 35.6	45.7 36.5		210	5.4	0.05	8.2	6
0000													10.1			33.6	30.5		170	6.4	0.05	8.1	8

Γ																Ray	6	em	1	T						T						T			1		
$\vdash$		21 B	20.5	17.8	15.1	14	12.1	14.3	18.1	20.8	23.7	25.2	24.8			FIE	(deg. C)	emperature		1	-					_	+	1		-			-	+	+		_
																Raw			t	†								1					1	1	1		_
																FIR	(FgA.)	Crottlata													T						
	ŀ	7	37	33	700	31	26	21	29	42	03	6	44	Raw	(¥1	-		T	1							1					T			1	1		_
		0	0	0	0	0	0	0	0	0	0	0	0	Raw Filt.	DomL)	otal	င်									1									1		
		1	တ	ۍ.	ā	16	5	w	27	5	14	ω		_	1	•	oms								Ì	1	1				Ì		1		1		_
r														FIR	(#/100mL)	Fecal								T			1					$\dagger$	+				-
-			0	0	0	<5.3	0	0		-		-	0		┝	-	6	3		1				-	-		1	-		-	-	+	+	1	+		_
$\vdash$			0	_			-	0	<u>                                     </u>		-	_	0	-	FIE	(F/100L)	Glardia	1000141		1				-	+	1	+	-		-	-	+	+	-	+		
-		_	0	0	0		0	0					0		<del></del>	-	┿	1.	Parame						-		1					1	+				
-			<u>_</u>	-		_	-	0	_		_	-	0	-	THE THE	ysts/1001	Crypto.	THE P	-			_	-		1	+	1		_		-	+		1	+	_	
$\vdash$		-		_	_	-	-		-	_		_	-	-	Ray	-	4	1	-	+		-		-	-	+	+				-	$\frac{1}{1}$	+		+		_
F							-		-	-	-	-	-		Raw Filt.	Pm.	Viruses		-					-	$\dagger$	+		-			+	+	+	1	+		
		3	1500	880	63700	ã	2100	13700	3600	80	410	1750	98		Raw Fire	(CFL	Ŧ			1					T	T							1		1		
	i	5	0	0	0	0	0	0	0	0	0	0	0		FIX	l/mL)	HPC																				
														chlorine	used with an 'X'	Indicate																					
H	+	1	-		_	-								chic	with an	disinfec			-	1				-	+	+	1	-			-	-	+	+	+	-	
														chioramine	X,	tant(s)																					
														3	850p	Chlorine																					
	+	$\downarrow$			1	1		-	1		1		-1	_	-				-	1				-		T	+	+	_		-	-		1	+	1	
														(mg NH3-N/L)	dose	Ammonia	Raw																				
														chlorine.		- 1	¥													-							
														chloramine	€	incububation time																				1	

		<del></del>																	
		<del></del>																	
		<del> </del>																	
		<b></b>																	
		ļ																	-
												<del>  </del>			<b> </b>	<u> </u>			
		<u> </u>											<del></del>						
												<del>  </del>							
												<del> </del>							ļ
											ļi								
									[							<b> </b> -			
															<b> </b>				<u> </u>
		1					· · · · · · · · · · · · · · · · · · ·	<u> </u>					1		l				
		Chlorinatio	n conditions												nfection				
		T					tered					11			LA5	HA		TO	
incub.	pH	Residual		infectant(s)	Chlorine	Ammonia		tion time	Incub.	pН	Residual	(19			1/L)		/L)	(ha (	
temp.			used Wi		dose	dose		h)	temp.			Raw	FIIL.	Raw	FIR.	Raw	FIIL.	Raw	FII
(deg. C)	()	(mg Cl2/L)	chlorine	chloramine	(mg Cl2/L)	(mg NH3-N/L)	chlorine	chloramine	(deg. C)	0	(mg Cl2/L)			·					L
			X	X	1.7	0.37	0.24	<b> </b>	24.8	7.2	1.2	<0.5	14.1				7.1		ļ
					1.6			1				1	7.8		1	1	11.9		١
			X	X		0.36	0.23	Į	25.2	7.1		}							
		-	X	X	1.5	0.3	0.26		23.7	7.3	1.06		8.1				3.9		<u>L</u> _
			X	X	1.5 1.6	0.3 0.3	0.26 0.3		23.7 20.8	7.3 7.4	1.06 1.07	<0.5	8.1 9.8				5.4		
			X X X	X X X	1.5 1.6 1.6	0.3 0.3 0.33	0.26 0.3 0.26		23.7 20.8 18.1	7.3 7.4 7.4	1.06 1.07 1.07	<0.5	8.1 9.8 14.7				5.4 5.1		
			X X X	X X X	1.5 1.6 1.6 1.7	0.3 0.3 0.33 0.33	0.26 0.3 0.26 0.54		23.7 20.8 18.1 14.3	7.3 7.4 7.4 7.3	1.06 1.07 1.07 1.07		8.1 9.8 14.7 12.6				5.4 5.1 6.7		
			X X X X	X X X X	1.5 1.6 1.6 1.7 1.8	0.3 0.3 0.33 0.33 0.33	0.26 0.3 0.26 0.54 0.58		23.7 20.8 18.1 14.3 12.1	7.3 7.4 7.4 7.3 7.2	1.06 1.07 1.07 1.07 1.1	<0.5	8.1 9.8 14.7 12.6				5.4 5.1 6.7 8.6		
			X X X X X	X X X X X	1.5 1.6 1.6 1.7 1.8	0.3 0.3 0.33 0.33 0.33 0.33	0.26 0.3 0.26 0.54 0.58		23.7 20.8 18.1 14.3 12.1	7.3 7.4 7.4 7.3 7.2 7.2	1.06 1.07 1.07 1.07 1.1 1.1		8.1 9.8 14.7 12.6 16				5.4 5.1 6.7 8.6 7.5		
			X X X X X X	X X X X X	1.5 1.6 1.6 1.7 1.8 1.9	0.3 0.3 0.33 0.33 0.33 0.31	0.26 0.3 0.26 0.54 0.58 0.58		23.7 20.8 18.1 14.3 12.1 14	7.3 7.4 7.4 7.3 7.2 7.2 7.1	1.06 1.07 1.07 1.07 1.1 1.1 1.1	<0.5	8.1 9.8 14.7 12.6 16 17 24.6				5.4 5.1 6.7 8.6 7.5 6.3		
			X X X X X X	X X X X X X	1.5 1.6 1.6 1.7 1.8 1.9 2	0.3 0.3 0.33 0.33 0.33 0.31 0.33 0.33	0.26 0.3 0.26 0.54 0.58 0.58 0.52 0.41		23.7 20.8 18.1 14.3 12.1 14 15.1 17.8	7.3 7.4 7.4 7.3 7.2 7.2 7.1 7.1	1.06 1.07 1.07 1.07 1.1 1.1 1.1 1.12		8.1 9.8 14.7 12.6 16 17 24.6 24.3				5.4 5.1 6.7 8.6 7.5 6.3 9.8		
			X X X X X X X	X X X X X X X	1.5 1.6 1.6 1.7 1.8 1.9 2 1.9	0.3 0.3 0.33 0.33 0.33 0.31 0.33 0.33 0.	0.26 0.3 0.26 0.54 0.58 0.58 0.52 0.41		23.7 20.8 18.1 14.3 12.1 14 15.1 17.8 20.5	7.3 7.4 7.4 7.3 7.2 7.2 7.1 7.1 7.1	1.06 1.07 1.07 1.07 1.1 1.1 1.1 1.12 1.11 1.17	<0.5	8.1 9.8 14.7 12.6 16 17 24.6 24.3 20.3				5.4 5.1 6.7 8.6 7.5 6.3 9.8 12.6		
			X X X X X X	X X X X X X	1.5 1.6 1.6 1.7 1.8 1.9 2	0.3 0.3 0.33 0.33 0.33 0.31 0.33 0.33	0.26 0.3 0.26 0.54 0.58 0.58 0.52 0.41		23.7 20.8 18.1 14.3 12.1 14 15.1 17.8	7.3 7.4 7.4 7.3 7.2 7.2 7.1 7.1	1.06 1.07 1.07 1.07 1.1 1.1 1.1 1.12	<0.5	8.1 9.8 14.7 12.6 16 17 24.6 24.3				5.4 5.1 6.7 8.6 7.5 6.3 9.8		
			X X X X X X X X	X X X X X X X X	1.5 1.6 1.6 1.7 1.8 1.9 2 1.9 1.8	0.3 0.3 0.33 0.33 0.33 0.31 0.33 0.33 0.	0.26 0.3 0.26 0.54 0.58 0.58 0.52 0.41 0.31		23.7 20.8 18.1 14.3 12.1 14 15.1 17.8 20.5 21.8	7.3 7.4 7.4 7.3 7.2 7.2 7.1 7.1 7.2 7.2	1.06 1.07 1.07 1.07 1.1 1.1 1.12 1.11 1.17 0.95	<0.5	8.1 9.8 14.7 12.6 16 17 24.6 24.3 20.3 19.3				5.4 5.1 6.7 8.6 7.5 6.3 9.8 12.6		
			X X X X X X X X X X X X X X X X X X X	X X X X X X X X X X X X X X X X X X X	1.5 1.6 1.6 1.7 1.8 1.9 2 1.9 1.8 1.8	0.3 0.3 0.33 0.33 0.33 0.31 0.33 0.33 0.	0.26 0.3 0.26 0.54 0.58 0.58 0.52 0.41 0.31 0.24	act time (see Fit	23.7 20.8 18.1 14.3 12.1 14 15.1 17.8 20.5 21.8	7.3 7.4 7.4 7.3 7.2 7.2 7.1 7.1 7.2 7.2	1.06 1.07 1.07 1.07 1.1 1.1 1.12 1.11 1.17 0.95	<0.5	8.1 9.8 14.7 12.6 16 17 24.6 24.3 20.3 19.3				5.4 5.1 6.7 8.6 7.5 6.3 9.8 12.6		

	-	-	-	_	_	-	_		_		_	_		(see above)	<del>=</del>	Coagulant		TREATME	*	3	2	1	ID.	ndicate coa				
	35.7	36.7	42.9	49.9	42.2	47.4	35.6	31.1	31.6	31.8	33.7	31.2				Dose	Coagu	TREATMENT CONDITIONS				Alum	Coagulant	indicate coagulants studied:				
	γ	~	~	4	Y	Y	4	۲	~	Y	4	4		(XX)	adjusted?	Acid	Coagulation Conditions	TIONS				AI2(S	Chemica	led:				
	z	z	z	Z	Z	z	z	z	z	z	z	z	1	CYN	adjusted?	Base	ions					A12(SO4)3	Chemical formula					_
													5	=	모	Coag.						η <b>ζ</b> αι	Units					
													)	den C	demo	Coag.												

100	DIARII	DIARII	DIARII	JARII -	DIARIC	JARIO	JAR III	DIARIO	DJAR I	JARIO	JAR (0	JARIG	JAR ID	MARIN9	JARUY )	JAR09	JARUS -	JAR09	JAR09	JARO9	JARU9	JARIN 1	JARUN	AROK	AROX	AROS	JAROX	AROX	JAROS 1	JAROS	JARON	ARUN	AROT	AROT I	ARO?	רוואא	3,78077	JARO"	ARG:	ARUT I	AROT	JARIK I	ARIM	AROX	JANK I	ARIK	ARIX	JARIK.	ARG	JARIK	ARIX	JAROI	JAR01	AROI	JAROI	ARU				- - -	T WOALL		cate with	-	te with an	cnbe lave	rca water iD		TOR WATER	Jay ID:	5	
2	ž	2 2	8 8	2	90	8	3 2	£	8 8	3	ž	2	2 2	S	ş	ş	8 8	8	*	8 2	3	2	8 2	8 15	10ki	1001	100	8	ğ	icx)	ixi	8	2	(x)	190	8	100	100	(Q. )	8	(S)	ia,	(3)		100	IQ:	D 18	100	100	io	<u> </u>	¥ .	100	8 15	3	ğ [ğ			% CRW %	Water	L CA		an 'X' If gata	-		of study:	Ð		+	+		-
	2	2	2		1 2	12	,,,	2		2	2.	- 1-		-	2	12			2:	2		-		1 2	-	2.	2.4		-	- 2.	2,	-	2 2	2.	2.1	ME		2.1	-	2		-	E 1	; ;	: 1:	2	- -  -  :  :	1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	1 23	2	2 2	-	2	2 12	2	220		2	% SPW	-	CONVENTIONAL	Contract	reported as	+	$\frac{1}{1}$				+	-	-	-
	1 5	67	2.67	3 5	¥ .	¥ 1	=	S# 2		2	2		-   - -   -	125	55	2		2	~  -  -	2 2	223	2	12 1	;   =	5	-	2	~   ·		-	- -	~ [		19	5	5   5	3	- T	-1	3 4	1		-		-	3		-	-	2		3 2	H		╁┤		1-1	7	(mg/L)	힍-	-		, H.	-	T 2	À B	-	-	-	Ja7 7	-	-
100	22	21 : 0	8	3 5	23	7	3 9	0	2.01 0.055	5	E C	2		27		3,6	2 2	2	1_1	-J.	123	46 1 13	51 10	\$   \$ d	19	87	12	=   5	×		-	-	-   -	63 (	68 0	2 6 2 6	8	2	8	=   S	=	3	9	8 5	3	# ·	S) 5	1 2	93	5	20 7	5	L_I.	_!_	2.27 0	_1_	1_1	7			ŕ	1	are from	- 1	Pilot-scale	20-430	S	-	-	-813-79/	-	_
1	.053	053	83	95	335	5.5	T	17	-1-	1-	1	7	3 5	185	055	55	Ž 5	18	0.055	2   3	185	155	055	100	18.6	1 170	30		3	100	- 190	ž   3	-   -	1.750	3		*	176	8	3	3	ž	\$	1 9	1 410	0)9	3	13	110	1 610	- 0	1	П	1-	025	0.025	-	13	(1/cm)	Ş -	+	+	samples	+	$\left  \cdot \right $	-	W. CRW	-	Surrace	range of %SP	-	_
1,12,4	0 026	0.025	0037	200	0.028	0.036	S S S	0.030	2,027	P.(0.0	0.031	1900	900						0.032	0.03	200	950.0	CLIM6	0.019	OEIVB	0.020	0.021	0.024	0.025	0.026	150.0	1500	0.019	0 021	0.027	0.023	u 023	9.025	0.025	0.032	0 n.y	0.001	1000	0.00	0.001	E CE	0 30	9(X)	1100	110	6400 6400	10.034	860.0	0.035	0.036	0.039		ř		2			s collec				¥			Į₹	ξĺ	
110	128	122	123	ī	ıχ	ij	12%	125	E E	125	125	E	12.23	119	911	179	5	=	119	3	1119	1)4	119	12	13.	ij	13	1 2	Ē	122	123	13 15	3 2	3	ä	i i	23	132	F	F	Ħ	132	2	3 2	133	132	8 8	1 2	132	ij,	B E	3	123	3 23	ē	EE		784	(mg/L as CaCO1)	Alkalir		or afte	collected after sedimentation only:	THURSTION, I	after coagu	in this data				*CRW		
Ī																																																										111.	(103	Ž		T Sedime	dimenta		Jation, fi	Sheet.	(Slate Project		River, to	Optimiza		
1	0.49	0.49	0.49	0.49	0.51	0.61	200	11.04	2 2	0.64	0.64	ŝ	2	0.71	071	0.71	0.71	2,7	0.71	0.71	0.71	0.71	0.71	0.40	1.461	0.47	0.40	0.40	0.40	040	33.0	040	000	0.42	042	5 G	1	040	ŝ	0.5	043	065	30.0	GA C	0.65	0.65	065	103	0.05	0 4.5	0.6%	074	074	0.7%	0.74	2 2			(טדא)			ntation at	יאסח פחלץ:		occulatio	FIR. rata	OJECI WEIBI		(River, lake, groundwater, etc.)	(Optimization Study	2	_
11.10	; ;;	046	0 0 0 0	1	1,30	9	20.02	0.63	0.75	2	2	96	2 0						20	3		20	0.40	5 G	848	0.50	0.35	2	1.64	2	5,	8	6.65	0,60	0.50	5 S	â	r r	ដ្ឋ	26	ž	-	à	3 8	0,00	2	20 20		431	1.5.	0.0	3	G 93	0.68	3	2 2		ř		7		ig filtrat			1, sedim	a co dat	Water, Diend of.		Water, et	9/95, etc.	1	
	3.33	2.33	ğ E	5	1 27.8	ž.	1,12	13	E		8 25 1	E		7.97	7.97	797	797	797	7.97	7.97	7.97	79.	7.97	3 =	=	% I 8	× 1×	*		×	8.12	30 TE		n N	8.34	# F	2	7	2			, 65°	8,29	2 2	Ey.	R.29	22.	238	7. J.	K.29	19 8	103	3.03	59	\$ 00	203	-	Raw	0	뭐_		ign:			after coagulation, floctulation, sedimentation, and	a collected	i ≇ic.)	-		- 2		
- -			- - - -	<del> </del> -	-		-	-		-	-	-	- -	-	_	-	+	-	-		- - - -		 ->	+	-	1	-	-  -	- -	-	-		- -	_	3	1	-	-	-	- - - -	-	-	-	1	-	1	-	-	-	-	- - - -	-	-	-	-	+		(see above)	Coagulant	- 202	מדמדע		×	1		Doses incl			$\dagger$	indicate c		
1 2	ž Š	36	8 8	5 =	110	100	£ 2	70	\$ 8	5 5	ŭ	ä	3 0	120	110	100	8	8	S	25	5 5	10	10	ء او	, s	<b>32</b>	7	3 3	s ±	8	20	= -	0 0	ž.	1 20	2 3	S S	- 40	3	20	; -	10	3(60	£ 8	3	3	ž į	3	20	16	2	8	50	# H	20	5 0				COMP	1000		50 mm setting time	$\dagger$		JOB USUBNY 3 (	2	2 Polymer	D Coagulant	D Conquiant	-	-
1			- -	+	-		- -		1				-				- -																- [-			_																		-			Dianker	(Y/N)	Acid	Hatton Cond	SACIL		ing time	+		Sometimes 2)			Viv.		+	
																																																									Nankar.	AGJUSTEG?	Dose Acid Base	tions						2) mg/L polymer			SO.,, "IA H,O	- Tomula		
6.93	721	74	7 2	7 40	4.3	6.75	6.88	7.04	31.5	21.5	7.28	749	7.74	ŝ	041	05.0	35.0	6.79	6.25	6.89	7 2	7.48	7.66	7.97	38	7.17	7.26	3	1.52	761	777	785	798	7.06	7.10	រី ម៉	7.3	7.46	.36	7.71	-	6.57	6.67	27.0	6.91	7.00		73	767	7,88		6.2	52.5	7.30	ì.	3 8 8	П	= 3	Coag		1			1				ηQ/	ag/L	Unit		

Study ID	Wa		TC			/-254	Alkai		Turb	idity	l pi				lation Cond	ition5	
	% CRW	% SPW	(mç			/cm)	(mg/L as		(N	บเ	()		Coagulant	Dose	Acid	Base	Cos
			Raw	Fin.	Raw	Filt.	Raw	Filt.	Raw	Filt.	Raw	Filt.	ID		adjusted?	adjusted?	pH
				-			<del></del>				ļ	-	(see above)		(Y/N)	(Y/N)	()
MWDJARII	! !X! !		2.67	1,66	1 0.053 (	0.026	1 128	<u> </u>	( () ()	200	1	:	1	- 70	biank≃N	blank=N	<del></del>
MWDJARII	90		2.67	1.67	0.053	0.022	128	<del> </del>	0.49	1.10	8.33	1		90	<u> </u>	ļ	6.62
MWDJARIZ	90		2.95	3.(x)	0.042	0.041	1 120	<del> </del>	0.67	0,30	1.23	<u>:                                    </u>	<del>- ; -  </del>	0			1 2.20
MWDJAR12	9(1		2.95	2.76	0.042	0.032	120	1	0 67	0.28	1.23	<del></del>	1	10	T	<del> </del>	7.80
MWDJAR12	90		2.95	2 63	0.042	0.032	120		0.67	0.22	8.23	;	1	20			7.66
MWDJAR12	( 90		2.95	2.50	0.042	0.031	120		0.67	0,21	8.23		1	30			7.44
MWDJAR12	90		2.95	2.35	0.042	0.029	120		0.67	0.23	1.23	<u> </u>	1	40			7,26
MWDJAR12	90		2.95	2.33	0.042	0.029	120		0.67	0.23	8.23		1 1	50			7.23
MWDJAR12	9(1		2.95	2.12	0.042	0.032	120		0.67	0.24	E.23			60	<u> </u>	<u> </u>	7.16
MWDJAR12	9(1		2.95	1.95	0.042	0.029	120	<u> </u>	0.67	0.20	1.23	ļ	1 1	70	<u> </u>		7 08
MWDJAR12 MWDJAR12	90		2.95	1.90	0.042	0.029	120		0.67	0.25	8.23		1 1	90		<del>}</del>	7.01
MWDJAR12	90		2.95	1.86	0.042	0.028	1 120	-	0.67	0.29	¥23	-	1-1	100	<del> </del>		6.22
MWDJAR12	90		2.95	1.82	0.042	0.027	120	·	0.67	0.27	8.23	1	1	110	·		6.79
MWDIARI2	90		2.95	1.74	0.042 (	0.028	120		0.67	0.47	1.23	<del>                                     </del>	1	120			6.76
MWDJAR12	90		2.95	1.70	0.042	0.028	120		0.67	0.56	1.23		1	130		l	6.67
MWDJAR12	(X)		2.95	171	0.042	0.026	1 120	·	0.67	0.52	\$.23	i	1	140			6.61
MWDJAR12	<b>7X</b> )		2.95	1.62	0.042	0.026	120		0.67	0.45	8.23	i i	1	150			6.47
MWDJAR12	90		2.95	1.61	0.042	0.027	120		0,67	U 49	1.23		1	160			6 40
MWDJAR12	90		2.95	1.54	0.042	0.027	120		0.67	0.55	1.23		11	170	<u> </u>		6.37
MWDJAR12	961		2.95	1.62	0.042	0.028	120		0.67	1,30	R.23	<u>  </u>	1	180	ļ	<del> </del>	6.23
MWDJAR12	90 )	<del> </del>	2.95	1.69	0.042	0.026	120	<u> </u>	0.67	1.30	\$.23	<del></del>	1	190			6.18
MWDJAR12 MWDJAR13	90		2.95	1 2.26	0.042	0.035	120		0.67	3,%1	8.23 8.30	<del>                                     </del>	1	2(X)	<del></del>	<del> </del>	8.28
MWDJARI!	90		2.25	2.08	0.034	0.023	126		0.77	0.48	R_36	<del></del>	<del></del>	10	<del></del>		7 90
MWDIARIS	94:			1.86	17.034		1 126	<del> </del>		0.40	\$.30	<del></del>				·	7-
MWDJARI!	7(1)			1 2 (k)	0.034	0.019	1 126	<del></del>	0.77	0.38	X 3()		1 1				7.50
MWDIARIT	) <b>9</b> ()		2.25	1.92	0.034	0.018	1 126		97	11 46	8 30		1	40			7.41
MWDJARIN	, y()			1.86	0.034	0.018	126		e <del>7.</del>	0.45	x 30		1	5()			7.33
MWDJAR13	, iXi j			1.80	0.034	0.018	126		0.77	n <u>s</u> t	8 30		1 1	A)			7.20
MWD/ARI3	90 1		2.25	176	0.034	0.015	126		****	0.57	8,36		1	70			7 14
MWDJAR13	ye) !			1.66	0.034	0.013	126	ļi	0.77	0.5%	R.30		1 1	90)	:		7.0
MWDJAR13	90		2.25	1.52	0.034	0.012	1 126		0.77	0.55	8.30			100			6.98
MWDJAR13	(X)		2.25	1.51	0.034	0.012	126		0.77	0,78	X.30	<del></del>	<del></del>	110			6.25
MWDJAR14	90		2.31	2.48	0.033		1 127		0.58	0.54	X.211		1	0			8.22
MWDJAR14	1 90		2.31	1 2.45	0.033	0,025	127	<del></del>	1).5%	0.55	\$.20.		1 1	10			7 95
MWDJAR14	90		2.31	2.38	0.033	0.023	1 127	,	0,58	044	1,20		1	20			7.71
MWDJAR14	• 961		2.31	2.21	0.033 1	0.021	1 127	,	0.58	() 48	\$.20		1 1	30			7.52
MWDJAR14	90		2.31	2.09	0.033	(1,020)	127	!	0.58	11.67	\$.20		1	40			7.40
MWDJAR14	9()			1 198	0.033	0.018	127		0.58	0.39	8.20	1 )	1 1	50	1		7.31
MWDJAR14	(אי	1	2.31	177	0.033 (	0.017	127		0.5%	83.0	\$.20	<u>'                                     </u>	1 '	181			7.27
MWDJAR14	90			174	0.033	0.015	127	ļ	U 5%	0.77	1,20		1 1	70			7.13
MWDJAR14	ger ;		2.31	1.67	0 033 1	0.017	127	<u> </u>	0.5k	0.X2	R.20		1 1	MIT		·	7.06
MWDJARI4	90			1.55	0.033	0.015	127	<u> </u>		1) 7()	8.20 8.20			100			6.93
MWDJAR14	1 90		2.31	1.52	0.033	0.014	127		0.58	1 (X)	8.20	<del></del>	<del></del>	110			6.77
MWDJAR14	90		2.31	1 144	0.033	0.015	1 127		0.58	1,131	1.20			120			6.60
MWDJAR14	90	1	2.31	1 46	0.031	0.016	127		0.52	1,00	1.20		1 1	130			6.53
MWDJAR14	90			148	0.033 +		1 127		0.58		K.2t)		1 1	14()			· · · · ·
MWDJAR14	r 90 i		2.3)	1 42	4 44		127		0.58		8.20		1 1	150			
MWDIAR14	1 90 1		2.31	131	0.033		1 127	1	0.5%		8.20	. }		160			1
MWDJAR15	; 190	!		2.51	0.036	17,144.1	127		0.47	0.35	8.29	, ,	1	0			1.30
MWDJARIS	90 1			2.37	0.036	0,034	1 127		0.47	0.54	8.29		1 1	10			794
MWDJARIS	90			2,24	0.036	0.031	127		0.4"	0.39	\$.29		1 1	30			7.74
MWDJARIS	90	- '	3.17	2.06	0.036	0.028	1 127		0.47	0.27	8.29			40			7.52
MWDJARIS	90		3.17	1.86	0.036	0.026	1 127	<del> </del>	0.47	0.59	8.29 3.29	<del>  </del>		50			7.39
MWDJARIS	90			1.76	0.036	0.025	127	<del></del>	0.47	0.58	1.29		<del>;</del>	(%)		i	7.23
MWDJAR15	'77)			1.72	0.036	0,024	1 127		0.4"	0.65	8.29	: '	1	70			7.15
WWDJARIS	90		3.17	I fx-	0.036	0.024	1 127		0.47	0.77	8.29	-	1 1	<b>X</b> ()			7.0x
MWDJARIS	- 941		3.17	1.54	0.036	0 024	1 127		0.47	0.63	8.29		1 1	90			7.03
MWDJAR15	( X )		3.17	1.58	0.036	0.022	127		0.47	0.78	8.29		1 1	100			6.91
MWDJAR16			2.43	2.52	0.041	0.042	1 117		0.42	0.32	X.25		1	0			\$.28
MWDJARIG	9()			2.50		0.031	117	<b></b>	0.42	0.35	X.25	1		10			8.01
WDIARIG	90 1			2.32	0.041	0.026	117		0.42	0.23	¥ 25		1	20			7.80
WDJAR16	; 90 j	-		2.19	0.041	0.025	117		0.42	0.24	\$.25 \$.25	<del></del>		3i) 4U			7.5
WDJAR16	1 90		2.43	2.06	0.041	0.024	117	<del> </del>	0.42	0.30	1.25		- ; ;	5()			7.4
WDJAR16	90		2.43	1 99	0.041	0,022	117		0.42	0.30	1.25		1	GO			7.3
WDJAR16	90		2 43	1.92		0.021	117		0.42	0.35	8.25		1	70			7.2
WDJAR16	90		2.43	187		0.021	117		0.42	0.33	8.25		1	<b>X</b> 0			7.1
WDJAR16	9(1		2.43	1.82		0.021	117		0.42	0.36	8,25		- 1	90			7.0
AWDJAR16	90			1.85	0.041	0.021	117		0.42	0.36	8,25	<u> </u>		100			7.0
MWDJAR16	90		2.43	1.75	0.041	0.020	117	<u> </u>	0.42	0.39	1.25		1	120			6.8
WDJAR16	90	<del></del>	2.43	1.73	0.041	0.019	117	<b> </b>	0.42	0.46	8.25			120			6.7
WDJARI6	90		2.43	1.65	0.041	0.018	117		0.42 G.42	0.55	\$.25			140			6.6
WDIARIO	90		2.43	1.68	0.041	0.017	1 117		0.42	0.62	8.25		1	150			6.5
AWDIARI6	90		2.43	1.60	0 (14)	0.016	117		0.42	0.80	8.25		1	160			6.5
(WDJAR16	90	1	2.43	1.49	0,041	0.015	117		0.42	0.91	8.25		1	170			6.6
ALKALDANI	90			1.61	0.041	0.014	1 117		0.42	1.10	1.25	1	1	130			6.4
WDJAR16			2.43	1 64	0.041	0.013	117	-	0.42	1.10	1.25		1	190			6.3
WDJAR16	901		2.43	1.55	0.041	0.014	117		0.42	1.40	8.25		1	20x)			6.2
MWDJAR16	90		2.43	1.52	0.041	0.013	117		0.42	0.93	X.25		1	210			6.1
MWDJAR16	1 90 1			1.58	0.041	0.013	117		0.42	1.10	X.25		1 1	220			61
AWDJAR17	30	<u> </u>	2.55	2.55	0.061		114		1.20	1.20	¥ U9			0			1 D
WDJAR17	1 80		2.55	261		() ()4%	114		1,20	0 49	8.89	!		10			7.6
WDJARI7			2.55	2.55	19061	0.042	114		1.20	0.41	¥.09		1	20 Vo			744
WDJAR17	30	<del> </del>	2.55		0.061	0.041	1 114	<del></del>	1.20	0.34	\$.09 \$.09			40			7.1
THE WATER I	2 340 I	<u> </u>	2.55		11 (36)		114		1,20	0.61	2 04	<del></del>	- ;	50			20

Page 2 of 10

Study ID	w,	ter	TO	ic i	บัง	-254	Alka	initv	Turb	idity	p)	-		Coann	lation Cond	tions	
Study ID	% CRW		(mg			'cm)	(mg/L as		(N7		0		Coagulant	Dose	Acid	Base	Coa
		1		Fift.	Raw	Filt.	Raw	Fift	Raw	Filt.	Raw		ID		adjusted?	adjusted?	pł
													(see above)		(Y/N)	(AVA)	()
		<u> </u>					<u> </u>	!							blank≖N	blank=N	
MWDJARIT .	80		2.55	2.02	0.061	- U.I.V.		<del> </del>	1.20	0.44	8.09			60			6.9
MWDJAR17	W .	<del> </del>	2.55	1.84	180.0	0.0M2	114	<u> </u>	1,20	1,10	\$ 119		1	7u 80			6.64
MWDJARI7	80 80		2.55	1.84	160.0	0.032	114		1.20	0.95	\$ (19 \$ (19			90			6.5
MWDJARI7	<b>2</b> (1)		2.55	1.64	0.061	0.033	114	<del>}</del>	1_20	1 40	8.09	-	1-1	100	<del></del>		6.2
MWDJAR17	80	<del> </del>	2.55	1.67	0.061	0.033	114	<del> </del>	1,20	1.20	2.09		<del>- ; - </del>	110			6.1
MWDJAR17	80	-	2.55	1.62	0.061	0.013	114	<del> </del>	1.20	1,30	8.09	-	1	120			6.14
MWDJAR18	80	<del> </del>	2 45	2.59	0.054	0.061	121	<u> </u>	0.78	0.68	8.22		1	U			8.2
MWDIARIS	80		1.45	2.66	0.054	0.045	121	-	0.78	0.66	8.22		1	10			7.1
MWDIARIX	80	1	2.45	2,54	0.054	0.039	121		0.72	0.60	8.22		1	20			7.6
MWDJARIE	<b>X</b> ()	T.	2.45	2.32	0.034	0.035	121		0.78	0.65	8.22		1	<b>3</b> 0			7.4
MWDJARIX	<b>3</b> ()		2.45	2.35	0.054 (	0 (14)	121		0.78	0.54	2.22		1	40			7.3
MWDIARIS	<b>3</b> ()		2.45	2.22	0.054	0 032	121		0.7%	0.67	8.22		1	50			7.2
MWDIARIX	(1,8		2 45	1.95	0.054	0.034	121		0.73	11.82	8,22		1	60		<u></u> _	6.9
MWDJARIX	<b>A</b> ()		2 45	1.97	0.054	0.012	121	!	0.7%	0.76	8.22		1 1	70			7.0
MWDJARIE	<b>\$</b> ()	<del> </del>	2 45	1.77	0.054	0.033	121	!	0.78	0.78	8.22			30		<u> </u>	6.9
MWDJARIE	7(1)		2.45	1.12	0.054	0.034	121	<del> </del>	0.78	0.75	8.22	-	1 1	90			6.8
MWDJARIA	80	<del> </del>	2.45	1.76	0.054	0.035	1 121	!	0.78	0.73	8.22	L	<del></del>				6.1
MWDJARIX	<b>3</b> (1)	<del> </del>	2.45 2.70	1.75	0.054 1	0.037	1 122		0.57	0.55	8.22			110	ļ	<del></del>	8.4
MWDJAR19	80 80	<del></del>	2 70	2.65	0.049	0.031	122	ļ	0.57	0.69	8.38		1	10		<del> </del>	7.8
MWDJARI9	%()	<del> </del>	2.70	2.44	0.049 (	0.027	122	<del> </del>	0.57	U.60	2.38	<del></del>		20			7.6
MWDJAR19	80	<del> </del>	2.70	2.22	0.049	0 ()25	1 122	i	0.57	0.56	8.38		1	30	1		7.3
MWDJARIO I	80	1	2.70	2 IM	0.049	9 023	1 122		D.57	0.59	2.38		1	46)			7.3
MWDJARIO .	\$0		2 70	2.02	0 049	0.021	1 122		0.57	0.78	8.3K		1	5()			7.1
MWDIARI9	80	1	2.70	197	0.049	0.021	122		0.5	0.75	8.38		1	60			6.84
MWDIARIY I	<b>X</b> ()		2.70	1.85	13,049	0.012			0.57	0.81	8.38		1	70			6.7
MWDJAR19	\$41		2.70	1 7%	0.049	8101			0.57	0.97	8.38		1	<b>\$</b> ()			6.7
MWDJARIO	RO		2.70	, ).\$X	0.049	01015	1 122		0.37	0 29	8.38		1	9()			6.6
MWDJAR19	(13)		2.70	177	0.049	0.015	122		0.57	(1,84	8.38		1	100			6.50
MWDJARI"	(41)	<u> </u>	2.70	* 1 ##	0,049	0.016		!	0.57	1.50	X.38	-	1 1	110		·	6.5
MWDJAR2	t (K)	<u> </u>	2.53	2 (8)	0.042	11145	133		0.85		8.38		<u> </u>				
MWDJAR2	1(X)	<u> </u>	2.53	2,89	0.042	0.036	133		9.85	0.7)	8.38		<u></u>	10	<u> </u>		\$.0
MWDIAR2		<del>!</del>	2.17	2.68	0.042	0.030		1		0.53			1	30			7.7
MWDJARZ		<del>!</del>	2.53	2.51	0.042	0.027	133		0.85	0.64	8.38		1 1				7.3
MWDJAR2	31k)	<del></del>		2.30	0.042	0.029	133	<del> </del>	0.15	0.57	x.3x		<del></del>	50			7.2
MWDIAR2	100	<del> </del>	2.53	2.03	0.042	0.017				0.7%	1 R 3K		<del> </del>	(4)			6.9
MWDIAR	1(X)	<del></del>	2.53	1.99	0.042	0.028	133	<del></del>	0.85	(10	8.38		1 1	70			6.8
MWDJAR2	I(X)	<del></del>	2.53	1.90	0.042	0.018		<del></del>		1.20	X.38	_	1				6.8
MWDJAR2	1(%)	<del></del>	2.53	1,90	0.042	0 626		·		130	8.38		1 1				6 2
MWDIAR20	96)	<del></del>	179	2.87	0.057	0.055	1114	<del></del>	0.54	0,3x	1.21		1	0			. A.1
MWDJARJU	80	<del></del>	2.79	2.46	0.053	0.040				0.37	8.21		1	10			7.4
MWDJAR20	30	<del> </del>	2.70	2.60	0.051	0.044	114	1	0.54	0.25	8.2;						7,5
WMDIVK50	341)	T	2.79	2.19	0.053	0.038	114	!	0.54	0.24	8.21	,	1	30			7.43
MWDJAR20	#U		2.79	2.28	0.053	0.035	. 114		0.54	0.24	x.21		1 1	40	<u></u>		7.3
MWDJAR20	84)		1 2.79	2.20	0.051	11 016	1 114		11,54	0.20	\$.21		<u> </u>	50			7.2
MWDIAR20	\$()		2.70	2.13	0.053	0.036	1 114	<u> </u>	0.54	0.20	8.21		1				7.1
MWDJAR20	All	<del>!</del>	2.75	2.03	0.053 1	0.032	1 114		0.54	0.23	8.21	-	<del></del>	70 <b>3</b> 0			7.10
MWDIAR20	80	<u> </u>	2.79	1.97	0.053	0.033	114		0.54	0.26 U.27	8.21		<del>  </del>	9()			1 69
MWDJAR20	80	<del></del>	2.79	1.83	0.053	0.032		<del></del> -	0.54	0.27	8.21	-	1 1	1(X)			6.5
MWDJAR20	\$41	<del>}</del>	2.79	1.79	0.053	0.631	114		0.54	0.63	8.21		1	110		<del></del>	6.8
MWDJAR20	80	<del> </del>	2.79	174	0.057	0.031		1	0.34	0.39	8.21		1	120			6.7
WWDJAR20	80	<del>                                     </del>	2.79	1.70	0.053	0.02	1 114	i	,	0.43	8.21		1	130			6.6
MIVDJAR20	\$(1)	1	2.74	1.62	0.053 +	0.032	114			0.53	8.21		1 1	140			6.4
MW DIARIO	8.0	Ι	2.79	1,61	0.053.1	0,030	t 114		(1.54	(1.5R	8,21		<del></del>	150			6.5
MWDJAR20	80		2.79	161	0.053	0.030	114		0.54	0.53	8,21		1	160			6.4
MWDJAR20	Rij	1	2 79	1.63	0.053	0.048	]   4	1		1) (4)	8.21		1	171			6.3
MWD)AR20	8()	1	2.79	147	0.053	0.63	! 114		0.54	1.26	K,21		1 1	180			6.1
MWDJAR20	<b>X()</b>	!	2 79	1 55	0.053	0.032	114		0.54	1.40	8,21	<u> </u>	<u> </u>	190	<del></del>		6.1
MWDJARO	34)	<del></del>	2.79	1.52	0.053	0.02"	. 114			1.50	1 8.21		<del> </del>	2(k)			8.2
MWDJAR21	. St.	Ļ	2.41	2.42	0.036	0.038	121	<del>!</del>	0.83	0.73	8.22 8.22	<u></u>		10			7.9
MWDIARZI	80	<del> </del>	2.43	2.42	0.036	0.028	121	<del> </del>	0 #3	0.52	8.22			20			7.6
MWDIAR21	80	<del> </del>	2.43	2.09	0.036	0.023	1 121	<del> </del>	0.83	0.32	1.22		1	30			7.4
MWDJAR1	\$4)	<del></del>	2 43	2.04	0.036	0.021	121	t	0.13	0.46	1.22	·	1	40			7.3
MWDIARZI	\$()	<del> </del>	2.43	1.97	0.036	0.019	121	<del></del>	0.83	0.57	8.22		1	50			7.2
WDJARZI	80	<del>                                     </del>	2.43	1.80	0.036	0.017	121	T	0.23	0.51	8.22	i	1	60)			7.
WWDJAR21	34)	<del>                                     </del>	2 43	1.77	0.036	0.017	1 121		0.23	0.57	8.22		1	70			7.
WWDJAR21	\$63	1	2.43	1.73	0.036	0.015	1 121	L	0.83	0.67	1.22		1	<b>3</b> ()			7.1
WDJAR21	30	L	2 43	1.72	0.036	0.014	121	1	0.83	0.71	1.22		1	90			7.0
WDJAR2!	\$41		2.43	1.70	0.036	0 014	121	L	0,83	0 72	1.22		1	1(X)			6 5
WDJAR21	80		2.43	1.69	0.036	0.013	121		0.83	0.98	8.22		1	110			6.9
WDJAR22	140	1	2.41	2.53	0.038	0.038	121		0.7%	0.71	2.15	<u> </u>	1	ti			1.2
MWDJAR22	841		2.41	2.31	0.038	0.029	121		0.78	0.50	8.15	!		10	<u> </u>		7.5
WDJAR22	\$0	<del> </del>	2.41	2.23	0.031	0.027	121	<u> </u>	0.78	0.68	3.15	<u> </u>	1 1	20	<del> </del>		7.7
WDJAR22	\$(1)	<del> </del>	241	2,04	0.038	0.021	121	<u> </u>	0.78	0.55	8.15	<del>}</del>	1 1	30	<del></del>		7.5
WDJAR22	20	<b></b>	2.41	1.96	0.03%	0.019	121	ļ	0.78	0.50	X.15	-		40	<del> </del>		74
WDIAR22	86)	<del>\</del>	2.41	1.94	870.0	adik	1 121	<del> </del>	0.78	(1.3X	8.15		<del></del>	50 60	<del> </del>		7.3
MWDJAR22	80	<del> </del>	2.41	1.81	0.038	0.018	121	ļ	0.78	0,73	8.15	<del>!</del>		70	<del> </del>		6.9
MWDJAR22	20	<del> </del>	2.41	1.74	0.038	0.017	121	<del> </del>	0.78	0 85	1 8.15 E.15	<del>!</del> -	1	Xu	<del> </del>	<del> </del>	6.8
MWDJAR22	( NO	<del> </del>	2.41		0.038	0.016	121	<del> </del>	0.78	0.76	8.15	<del></del>		90	<del> </del>		6.
MWDJAR22	* *0	<del> </del>	2.41	1.64	0.038	0.016	121	<del></del>	0.72	0.76	¥.15	<del></del>	<del>                                     </del>	100	<del> </del>	<del></del>	6.7
MWDIAR22	1 341	<del> </del>	141	1.58	0.038	0,015	121	<del> </del>	0.78	0.81	X.15	<del> </del>	<del>                                     </del>	110	<del>}</del>	<del>}</del>	6.7
MWDJAR22	10	<del> </del>	2.41	1.56		0.015		<del> </del>	0.78	0.95	1 8.15	;	<del></del> -	120	·	<del></del>	b.5
MWDJAR22	3(1)	<del></del>	2.41	1.42	870 n	0.015	1 121		0.78	0.95	X.15	-	<del>                                     </del>	130	<del> </del>	<del>                                     </del>	6.5
MWDJAR22	\$41	<del></del>		2.56			<del></del>	<del> </del>	0.43	0.45	8.32	<del></del>	<del>                                     </del>	0	<del> </del>	<del> </del>	1 8.3
MWDJAR23	1 20	<del> </del>	2.51	2.56	0.050	0.055	121	<del>[</del>	0.43	0.58	1.32	<del> </del>	<del>                                     </del>	10	<del></del>	<del></del>	73
MWDJAR23	) W()	<del> </del>			0.050	0.035	1 121	<del>;</del>	0.43	11.34	8.32		1	20	1	<del>                                     </del>	7.6
MWDIARES	: 80																

Study ID	Wa			oc		V-254	Aikai	inity	Turb	idity	рН			Coagu	ation Cond	Rions	
	% CRW	% SPW	(mg	g/L)	(	l/cm)	(mg/L as	CaCO3)	(N1		()		ulant	Dose	Acid	Base	Coa
			Raw	Fitt	Raw	Filt.	Raw	Filt.	Raw	Fin.	Raw				adjusted?	adjusted?	₽ŀ
				<u> </u>	<del> </del>	<u> </u>						(Sec a	DOVE)		(Y/N)	(Y/N)	()
			<del></del>	1 1 1 1 1			<u> </u>	!			1		لمسم		blank≖N	Diank=N	
MWDJAR2)	; <b>%</b> ()		2.51	2.(x)	0.050	0.028	121	<u> </u>	0.43	0.36	£.32		!	40		<del> </del>	7.3
MWDJAR23	1 80		2.51	1.92	0.050	0.024	121		0.43	() 40	8.32			50			7.21
MWDJAR23 MWDJAR23	OE (	<u> </u>	2.51	1.79	0.050	0.023	121		0.43	0.42	1.32 3.32			70		<del>}</del>	72
MWDJAR23	, A()		1 2.51	1.62	0.050	0.022	121	<del> </del>	0.43	0.45	\$.32 I	<del></del>				<del> </del>	70
MWDJAR23	80		2.51	1.56	0.050	0.019	1 121	<del> </del>	0.43	0.55	1.32	<del></del>		- VKI		<del>:</del>	7 00
MWDJAR23	3()		2.51	1.56	0.050	0.022	121	<del> </del>	0,43	17.5%	8.32	<del>i</del>		1(X)		<del> </del>	6 9
MWDJAR24	30		2.57	2 45	111145	0.046	1113	<del>;                                     </del>	0.63	0.59	1.11	- 1		υ			3.20
MWDJAR24	30		2.57	2.49	0.045	0.035	113		0.65	11.32	8.11		,	10		1	7.9
MWDJAR24	30		2.57	2.32	0.045	0.031	113		0.65	0.29	2.11	1	1	20			7 30
MWDJAR24	\$40		2.57	2.09	0.045	0.027	113		0.65	0.28	1.11	1 1	1	30			7.6
MWDJAR34	8(1)		2.57	2.05	0.045	0.027	113		0.65	0.28	8.11	1		4()			7.50
MWDJAR24	30		2.57	1.90	1 13.045	0.026	1 113		0.65	0.27	3.)) 1	1 1		50			7.3
WDJARJ4	<b>\$</b> ()		2.57	1 90	0.045	0.025	113		0.65	0.27	8.11		1	64)			7.19
WDJARJ4	( (40)		2.57	2.03	0.045	0.023	1 113		0.65	0.27	8.11			70			7.11
WDJARJ4	30	ļ	2,57	1 1 92	0.045	0.021	113		0.65	0.28	1.11			80)		<u> </u>	7.0
WDJAR24	<b>( 5</b> ()		2.57	1.80	0.045	0.021	113		0.65	0.40	8.11	!!		90		<del> </del>	6.9
MWDIAR24	30	<u> </u>	2.37	1.69	0.045	0.02)	113		0.65	0.44	1.11			100		<u> </u>	6.94
AWDJAR24	80		2.57	1.61	0.045	0.020	113		0.65	0.45	8 11			110		<u> </u>	6.84
CWDJAR24	\$0		2.57	1.61	0.045	0.020	113	-	0.65	(1.54	8.11			120			6.71
WDIARI4	1 R41	<u> </u>	2.57	166	0.045	0.019	113	ļ	0.65	0.62	8.11			130		<del> </del> -	6.6
AWDJAR24	30		2.57	1.55	0 045	0.019	113	<del> </del>	0.65	1.20	X.11	<del></del>		150		<del></del>	6.5
WDJAR24	80	<del> </del>	2.57	1.57	0.045	0018	113	<del> </del>	0.65	1,20	8,11	<del></del>		160 (		<del> </del>	6.4
AWDIAR24	8(1	<del> </del>	2.57	144	0.045	0.017	1 113	<del>                                     </del>	0.65	11.89	\$1L (	<del></del>		170			6.3
(WDJAR24	30	<u> </u>	2.57	146	0.045	0.017	112	<u> </u>	0.65	1.53	\$ 11			Die i		<del></del>	1 63
(WDJAR24	i XU	<del> </del>	2.57	1.30	0.045	0.016	1 113	<del> </del>	0.65			<del></del>		190		<del></del>	6.2
OWDIAR24	80	<del></del>	2.57	1 1.35	0.045	0.015	113	•	0.65	0.77	111 1	-		2txi		1	0.1
WDJAR24	NU NU	<u> </u>	2.57	1 1 412	1 0 045	0.015	1 113	1		0.75	3.11	<del></del>	,	2)0		1	6.0
CWDIAR24	80	1	( 2.57	1.29	0.045	0.015	113	<del> </del>	0.65	0.95	811 1	<del></del> -	<u> </u>	220			5.9
AWDJAR25	70	<del></del>	2.67	2.67	tros	-	1 109	1	0.84	0.75	7.84	· i ·		t)			7.9
FWDJAR25	70	i	2.67	2.59	0 065	0.054	109		0.84	0.65	7,84	<u> </u>		10			76
AWDJARZS	7(1)		2.67	1 249	0.005	U-049	109	,	U.84	0.65	7 74			20 (			7.4
(WDJAR15	70	1	2.67	2.20	0.065	0.039	1119	7	0.84	0.43	7.84 i	,	1	36			7.1
AWDJAR25	70		1 2.67	1 2.10	0.045	0.037	109	1	0.84	0.50	7.84		1	40			6.9
(WDJAR25	70	i .	2 67	1.97	1 0.065	0.037	109		17.84	D 76	7 84	7 1		50		<u> </u>	6.\$
TWDJAR25	70	i -	2.67	1.92	0.065	0.035	109		1),84	0.77	784	[1		60 (			6.7
WDJAR25	70	1	2.67	1.12	0.065	0.028	109		0.84	0.90	7.84			7()			6.5
WDJAR2:	r 70		2.67	1.82	0.065	0.026	109		0.84	0.85	7.84			<b>8</b> ()		<u> </u>	6.5
AWDIAR25	70		2.67	1,66	0.065	0.026	1 109		0.84	0.87	7.24		-	90		<u> </u>	64
WDJAR25	70		2.67	1.68	0 (26.5	0.024	109	!	0.84	0.95	7 74			100		!	6.2
WDJAR26	70	<u> </u>	2.50	2.56	0.055	0.058	1115	1	0.68	0.82	8.22			0		<u> </u>	1.2
WDJAR26	70		2.50	2.53	0.055	1) ()46	1 115	ļ	0.68	0.76	1.22 /			10		<u> </u>	7.7
WWDJAR26	7()		2.50	2.39	0.055	0.041	115	<del> </del>	0.68	0.71	1 2.22 i	<del></del>		30		<del> </del>	7.5
MWDIARIN	70	<del> </del>	2.50	2.29	0.055	0.038	1115	<del>}</del>	0.68	0.75	8.22			40			7.2
WWDJAR20		<del> </del>	2,50	2.02	0.055	0.035	1 115	L	0.68	0.73	1.22			50		<del> </del>	7.1
WDJAR26	i 70	<u> </u>	1 2.50	1.96	0.055	0.033	1115		86.0	0.67	1.22	<del></del>		(61)		<del></del>	1 69
MWDJAR26 MWDJAR26	1 70		2.50	1.75	1 0 055	0.034	1 115	<del></del> -	0.68	0,70	8.22	<del>-                                    </del>		70		<del>i</del>	7.0
MWDIARZO	70	<del> </del>	1 2.50	1 1.75	0.055	0.036	115	<del>                                     </del>	0.68	0.70	8.22			#1		·	6.8
MWDJAR26	70	<del>i</del> -	2.50	1.71	1 0 055	0.031	1 115	<del></del>	0.68	041	8,22 (			1911		1	67
WDJAR26	711		2.50	1.62	0.055	0.034	1 115	<del> </del>	0.68	0.57	8.22			1(X) I		1	67
WDJAR26	71)	<del> </del>	2.50	1.72	0 055	0.031	115	<del></del>		0.72	1,22			114		1	6.5
WDJAR26	70	<del></del>	2.50	1.63	0.055	0.032	1 115	<del> </del>		1.20	8.22	1		120		1	6.4
WDJAR26	70	<del>                                     </del>	2.50	1.56	0.055	0.033	1 115	<del></del>	0.68	1 411	8,22	1	1	130		1	63
WDJAR26	70	<del></del>	. 2.50	1 1.5?	0.055	0.035	115	1	0.68	1,70	K.22			(40		i	6.3
WDIAR27	1 70		3.14	2.94	1) 064	0.061	115		0.69	0.62	8.32	i 1		0			1.2
WDJAR27	70		3.14	2.38	0 (X)4	0.027	1 115		0 69	0.45	8.32			₹D .			7.2
AWDJAR27	. 70		3 14	2.62	0.004	0.030	1;5		U.64)	0.43	1.32			20		<u> </u>	7.3
AWDJAR27	70		3.14	2 48	01144		1 115		0.69	0.41	8.32			30 (		<u> </u>	7.1
AWDJAR27	( 7t)		3.14	2 44	0 (%4	0.027	115		0 69	0.52	1.32			40		ļ	70
AWDJAR27	70		3.14	2.14	0.064	0.024	115	<u> </u>	0.69	13.55	1.32			50		<del> </del>	6.9
AWDJAR27	1 70	<del> </del>	3.14	3.27	0.064	0.029	115	ļ	0.69	11.61	1.32			(4)		<u> </u>	6.7
(WDJAR27	70	<u> </u>	3.14	2.81	DIXA	0.020	115	<del>[</del>	0.69	0.71	5,32			70		<del> </del>	6.6
AMDIARCS	70	<del></del>		1.93	0.064	0.020	115	<del> </del>	0.69	0.62	8.32			90		<del></del>	6.5
TWDJAR27	70	<del> </del>	3.14	1.83	0.064	0.029	1 115	<del> </del>	0.69	0.84	8.32 8.32			1(X)		<del>                                     </del>	6.4
IWDJAR27 IWDJAR27	70	<del> </del>	3.14	1.96	0.064	11,112.7	115	<del> </del>	0.69	L.(X)	8.32	<del></del> -		110		1	6.3
IWDJAR27	70	<del></del>	3.14	1.72	0.004	0.025	115	<del>                                     </del>	0.69	1.70	1.32			120		1	6.1
WDJAR27	70	<del>                                     </del>	3.14	1 1.92	13.1354	0,019	115		11,69	2.10	1.32			120		1	61
(WDJAR27	70	<del>                                     </del>	3,14	1.76	0.064	0.017	115	1	0.69	1.70	8.32		<del>-  </del>	140		L	6.0
WDJAR27	70	<del>i</del>	3.14	1.75	1 0.064	0.016	1 115	<del></del>	0.69	3.10	8.32			150			5.7
TWDJAR28	70	<del> </del>		2.82	0.05%	0.057	<del></del>	1	0.47	0.37	<b>3</b> .12			0			8.1
WDIAR28	70		2.74	2.63	0.058	0,047	111		0.47	0.22	8 12 1		1	10			7.5
WDJAR28	70	i	2.74	2.45	1 0.05%	D.DA2	111	1	D 47	0.20	8.12			20			7.1
WDJARZE	70		2.74	2.39	0.058	0.039	111		0,47	0 17	£.12			30			7.5
WDJAR28	70		2.74	2.27	0.058	0.033	1111		0.47	0.16	2.12		1	4()			7.4
WDJAR21	70		2.74	2.17	0.058	0.039	111		U.47	0.21	1,12		1	50			7.3
WDJAR28	70		2.74	2.04	0.05%	0.032	111		0.47	0.22	8.12		1	60		ļ	7.2
(WDJAR21	70		2.74	2.02	0.058	0.030	1 111		0.47	0.22	3.12			70		<b></b>	7.0
(WDJAR28	70	T	2.74	1.96	0.05%	0,027	111		0.47	0.24	8.12		1	\$41			71
WDJAR2K	70	(	2.74	1.22	0.058	0.027	111		0.47	0.21	8.12		1	90			6.1
WDJAR2E	70		2.74	1.82	0.058	0.028	111		0.47	0.28	8.12		1	100			6.1
WDIAR28	70		2.74	1,82	0.05%	0,030	1111		0.47	0,27	8.12		!	110		<u></u>	6.7
AWDJAR28	70		2.74	1.71	0.058		1 111	!	0.47	0.33	8.12		1	120			6.7
AWDJAR28	70		2.74	1.63	D.05X	0.029	111		0.47	0,50	8.12		1	[30			6.6
AWDIAR2E		<u> </u>	2.74	1.70	0.038	0,070	111	<u> </u>	0.47	0.53	8.12		1	140	<u> </u>	ļ	6.5
WDJAR28	. 70		2.74	1.74	0.058	0.027	111	<u> </u>	0.47	0.45	R 12		1	150			6.4
WDJAR21	70		2.74	1.58	0.058	11.026	111	<u> </u>	0.47	11.45	1.12		!{	160		<del> </del>	6.3
			2.74	1 21	0.058		i III		0 47	0.58	8.12		1	170	<b></b>		6.3
WDJAR28	70	<del></del>	2.74	1.68	1 0 058	0.023	111		0.47	0.61	R 12		1	180	i .	l .	

MWDJAR31	MWDIARD	MWDJARJ2	MWDJAR12	WMOIARIE	MWDIARUS	MW:DJARJ2	MWDJAR32	CCRYCOMM	MWDJARJ2	MWDIART	WWDIARU2	WWDIARD	MWDJARJ2	MWDJARJ2	MWDIARTO	TOWN WA	MWDIARU2	MWDIARUS	MWDJARU2	MWDJARI	MALLANCIA	MADIAN	WW.DIARJI	MWDIARI	MWDIARU	HWDJARJI	HANDIVE I	I SEVICIAL	MWDJARJI .	MWDIARI;	MWDJAR3:	MWDIARII .	I CHYICAMP	MWDIARU!	WWDIARI	LAVIDAM	WWD.ARU	MULANT	MANUAR II	MACIAICI	MWDARGO	MWDJARW	MWDIARJO	MWDIARIO	MWDIAR30	MWDIARW	WWDIARW	MWDIARIO	WW.DIARU0	WWDIARU	MWDIARIO	WW.DIARJO	MWDIARN	MARIONES	WALDAR!	DIVIDAM	MWDIARI	MWDIARI	CAVIDAM	MWDIARS	CAVICAM	MWDJAR29	MWDJAR29	MWDJAR29	MWDJAR29	MWDJAR29	WTJARJ6	WWDIAR39	MA DIANCO	MW WALL	310000	WWDJARZ9	MWDIARZS	WWDJAR29	MWDJAR29	MWDJAR29	MWDJAR29	MW:DJAR2"					Study ID
3 8	8 8	15	20 20	101	3 3	70	3 3	3	3	8 8	3	ä	70	ਲ	3	2 2	8	ż	į,	וא	2 2	-	ð	ż	12	O,C	25	Ä	ż	70	70	'n	וא	3	70	105	3	1	2	<u> </u>	# 2	76	2	15	70	OK.	נול	ż	3	2 2	2	115	70	2 8	Q (2)	i Cr	)(X)	100		<u>(</u>	IX)	J)	מל	70	לל	3	3	3	3 2	3 2	3 2	2	3 3	Ę	6	70	3	טל				% CRW   % SPW	×
																																																																																		W SPW	-
172	17.72	149	2.49	2.49	2 2	2.49	2 5	2.49	2.49	2 3	249	2.49	2.49	2.49	246	3	1 13	2.49	2.49	2.60	2 8	100	2.60	2.60	2.65	2.65	2.60	3.60	2.60	2.60	2.60	2.80	2.60	2.60	2.60	2.85	2.50	8	6		1	24	1	12	2.4	2.44	244	1	24	1 1	1	2 #	ž	2	250	2.50	2.50	2.50	8	2.50	2,50	2.50	2.50	2.50	2.50	8	3	250	3	5	5	١	S	2.30	2.50	2.50	2.50	2.50			Raw	(mg/L)	7
2.50	2.62	Ē	77	1.39	- y	155	ž į	1.59	1.60	67	:   =	s	-	_	2	٠.		2	2.5	_	_];	:   :	5	4	1.50	1.47	1.52	1.52	1.62	1 62	1.72	131	1.87	£	2.00	2.10	2		8				127	1.79	.83	**	1.88	. <b>#</b>	.5	3,0	2.02	2.20	2.36	2.5	£ 5	1.7%	1.85	 2	200	2.30	2.55	1.37	1.39	1.41	1.47	1.47	49	8	5	3 6	,		3 2	97	2.12	223	2.44	1,4			F	Š	Ĭ
0.074	0.074	0,043	S S S	0.048	0 0	0.048	C X	0.04%	0.043	0 0	0.148	8 10.0	D DOM	0.048	0	000	0.048	0.048	8110	0.053	005	2027	0.031	0.053	0.053	0.051	0.053	0.053	0.053	0.053	0.053	UUSI	0.053	0.053	0.053	0.053 .	0.053	1500	0.051	2007	0.14	2	0.042	0042	0.147	CHO O	0 (42	0,142	0 (142	C C	042	0.042	3 K,	200	0.000	0	0.040	0.040	0000	0.040	0.040	0.040	0.040	0.040	0.040	O (K)	0.043	COR	0.00	0.0		2 2	0.040	0.040	0.040	0.040	0040	0 040			Raw	2	S
550.0	0.662	0.015	0.015	0.017	0.017	K10 0	0018	61070	0.021	0.023	0.022	0.022	0.022	0.027	0.00						0.017		0.01×	0019	0.020	0.020	0.021	0.021	0.023	0.023	0.024	0.026	0 (12)	62070	1500	0.033	97(17)	0.052	0051	11110	001/	31018	610.0	01015	10.01	1 91010	0017	610.0	6100		0.024	0.027	0.032	0042	0020	11122	0.022	0.023	0.029	0.029	0.037	10.0	0.014	0.018	910.0	0.017	2100	0.015	0.01	1017		0.019	0.020	0.020	0.023	0.026	0.030	0.040			F	(cm)	V-254
2 ž	ž	106	\$ 3	108	3 8	ī	ğ 5	8	ğ	ž ž	ğ	108	8	ğ	ğ	ŝ	Ş	īķ.	īœ	ī	-	-	-	1	Ē	114	ž	ī	114	711	114	124	114	114	ï	=	ī			100	5	116	=	116	116	116	116	-116	116	= =	116	116	10	116	2 2	Ē	¥	ž	e k	Ē	¥	115	115	115	115	E :	5	115				1	= =	=	IIS	115	115	115			Raw	(mg/L as CaCO3)	Alkaling
			_		1		1									1						-			L	L	_							_	-		-	-			-	_		Ļ	_			_	_		L			_ .	.   .	L			_							]		1	$\downarrow$			-		-	L						7	CO3)	~
3 3	70 6	2 22	0.52	a.s	2 2	320	2	22.0	20.53	2 2	ន	22.0	0.52	0.52	252	3 2	220	0.52	0.52	0.45	2	2	10.5	3	043	0.45	0.45	0.45	0.45	0.43	0.43	0.45	0.45	0.45	0.45	2	2	7			1	2	0.34	0.2	0.8	0.1	0.3	e .	0.3		2.0	0.1	0.3	2	3 5	0.63	0.42	042	0 42	0.43	0.42	0.63	0.68	0.68	23.0	200	064		2 5			0.63	20.63	26.5	0.68	0.68	0.68	1970			A S	(N	i u
2014	0.53	1.10	0.85	0.72	20.5	0.70	r i	0.49	0.39		0,30	0.33	0.30	22.0	029	200	1 02	0.37	0.44	-	-	5	0.71	1 2	077	0.63	0.67	0.50	0.52	0.48	0.42	543	0.42	0.53	0.33	Ē	11.50	2		1 30	2	-	0.75	0.95	1.10	0.54	0.72	e e	0.51	2 2	0.50	0.50	19.0	2	2 8	0.73	0.61	0.60	0.49	0.49	0.35	120	1.20	10	1,00	- 10	ē	2	3 5	3 2	1	9.//	E E	i k	0.2	0.52	15.0	0.48			F .	(NTC)	Ϋ́
x 03	1.03	X.X.	X (X)	1.0K	1,0%	100	2.58	3.3	N.Do	8 8	1.06	3.06	8.1%	8.0%	X.06	N CK	pa (X	X.UK	\$.(X:	X.25	, , , , , , , , , , , , , , , , , , ,	3.5	x 29	8,29	8.29	1.29	1.29	1.29	X.29	8.29	8.29	1.29	X.29	K.29	K.29	¥.29	8.29	1.29	9 29	* 1	A 34			3.14	X.TA	1 11.8	K.I.A.	M. Ta	X .		1.14	11.8	X 14	-	A A	7.41	K.4)	3.4	**	141	7.4	K.20	1.20	1.20	8.20	0.5	ğ	\$20	300	07.6	5	07.8	1.20	120	8.20	¥.20	100	1.20	-	-1	Raw Fitt.	=	모
	-	-	  -  -	-			-	-	-	-	-	-	-	_	-	-	1		-	-	-	-	-	1	-		-	-	_	_	_	-	-	_	1	-	-	-	-	-	1	-	-	-	-	_			-	- -	-	-	-	-	-	-	1	-	- -	-	-	-	1	1	-	-	-	-	1	1-	1	-	-	-			-	_		(See above)		Coaquia	
# 20	ē,	220	210	18		160	150	i ii	0,0	10 5	3 8	5	70	œ,	g		5 2	5	c	200	2	s s	3 8	150	ā	130	120	10	100	92	25	- *	8	ž	40	10	20	5	=	160	181	1 1		Ē	tx)	- P	- 26	6,4	8	- S	5 5	20	10	5	5 2	3 8	8	â		3 5	-	175	19(	150	140	- H	120	110	<u>8</u> 3	8 8	5 0	3 8	\$   X	5 5	8	20	5	0			T	٦	ı
							+			1		-				1					+		-								_		-			-	-		-	- -	-	-	- -	-	-	-				- -	+	_		- -		-			-	-						1	-	1	+	-		-	-	-	-	-	-	-	biank=N	(Y/N)	adjusted	Dosa Acid	nutation Con
		1					1															1						-						-			-		+						-		-			- -					1	†			+		+	-	-			-	1	1	†			†	1	+				-	- Dianx = N	(Y/Y)		Base	attons
7.38	7.59	5.86	.s. 5	6.13	A 9	6.51	6.65	6.75	5	6.83	6.97	72	714	727	7.4	7.43		7.90	8.07	6.23	2		ر ا	0.46	6.52	6.50	6.68	67.3	6.86	6.96	7.00	7,0%	7.20	7.27	7.32	7.52	7.64	7.91	1.30	637	0.00	0.4	25	6.70	6.74	6.79	6.82	6.86	7.(%)		7,5	7.53	7.81	: i	r ×	6.93	7.13	7.33	7.03	ř	3.40	6.27	6.33	0.40	6.58	6.63	67	6 50	2	3		7.06	7.39	7.4	7.51	7.69	7 92	1 \$.20		<b>a</b>	P .	Coag	

Page 5 of 10

N

MWDIARUS MWDIARUS	MWDIARU	MWDIARUS	MWDIARJA	MUDIANI	MWDJARJK	MWDIARUR	KWDIARUS	*CNVIONH	KUKALOWM	MADIVER	WWDIARUT	MWDJARJ7	MWDJARJ7	WWD/ARJ:	MWDJAR37	WWDIANO.	MWDIARU7	WWDJAR37	יו מאותשים	MAN CONTRACT	MADING:	DATOWN	MWUAKS	340000	MWUJARG	MWDIARCE	MWUJAKI	WHO WAS	MACA	WWDIAK-16	MWDIARD	31000	A BAICWA	MWDIAR36	MWDJARJ	MWDIAR VI	MWDIARS	WWDIARU	XWDJARX.	MADIARY	WINDIARIA	WWDJARJa	WWDWW	*CHYIGMM	MWDJARU	WWDJARJ6	WWD/AKJ6	WWD/ARG	WWDJARJS	MWDIARUS	WWDJARJS	MWDJARUS	MWDIARIS	MWUARIS	WWDIARGS	MADIAN	WWDIARDS	MWDIARUS	MWDIARUS	MWDJARUS	MWDIARUS	MWDIARUS	MWDIARIS	MWDIARUA	AUDIARIA MA	MWDIARU	MADIARY	MWDIARU	MADIARY	MWDIARU	WWDIARJA	MWDJARJA	WWDIARDA	MWDIARG	MWDIARU	MWDIARUA	MWUARUM	WWDIAR33	WWDJAR33	MWDJARJ	MWUNAU	MWDIARG	330000	MWUMAC	1000				
8 8	- [	1	1	1		- 1	1	1	- 1	1	1	ı	66)	60	ŝ	2	8	8	8	5	5	2	9	\$ 8	2 8	8	8	3	3	8	ž	2 9	2	3	ž	8	8	3	ŝ	8	S.	(3)	ŝ	(S)	ŝ	69	ક	ŝ	<u>\$</u>	3	3	ĝ.	8 8	8 8	3 8	3	8 8	3	8	8	8	3	8	8	8	83	8	8	3	2	33	8	2	8	8	8	2	8	8	8	2	8	9	8					% CRW
																																														_									-																	_																	* SPW
249	2	1 12	2.40	2.49 1.51 0049	2.49	2.49	149	2.49	2.49	1 1	256	2.56	2,56	2.56	2.56	2.56	2.56	2.56	3	8	2 2.50	1 20	,	و ا	,	ر پار	, ,		1	ŀ	3	ا ا	77		Ę	is	12	1	3.22	ננ	3.22	3.22	3.22	7	322	3.23	31:	3,22	3,44	ŭ.	1	1	2	i	í	1	1	1	i	1	1	*	ì	2.51	2.51	2,51	2.51	5	2	2.5	2.51	2,5			2	2	2	2.72	12		3 2	1 :	1	1 1	3			Raw	(m)
=   = =	يَ ن	1.39	ij	3 5	1.62	3.	Ē	1 42	1	2	1	1.39	1.37	1.38	ž	5	2	25.	63	3	- 3	1	3		1	1	1 6	1		1	-		7	3	-	75	9	202	2117	2.17	134		2.38	1.52	2.69	2.80	2.98	1.20	1	1.05	ž	. F	=	2	9	3 13		3	2.49	18	2.92	3.23	12	1.47	-	Ē	1.69	1.70	2	99	1.91	13			8	12		1.67	3	8		3 5		2	:			F	-
0.000	CHIAN I	9	0.049	0 0 0 0	0.049	U.O.C.	0.049	0.049	SMED	0 049	0.039	0.039	0.039	0.039	610.0	0.010	0.039	0039	0.015	0019	0.00	d.o.y	0.030	1	0.000	0.00	0.039			1			O IX	2	E CX	000	EX2:	0.00	D (344)	0 (24.1	13 (K-1	GWH.	(),(ku) i	FKIR	200	0.0%	D.IKL	D CKM	1,817	180.0	180.6	1,802.0	00*1	3	2 08 0 081	17.17.	0.000	1	0.00	a.axı	2.92   n.ux1	1 180.0	18070	U.IMB	S DAR	810.0	0.648	0.044	9	0048	3900	0.048	1,000	1	0 048	0.048	5	0074	0.074 0.0	100	0.10	3		2007	7,510	_	Ц	Ra¥ ·	3
0.019	0.021	0.014	0.014	0.017	81019	0,020	0.020	0.023	0.027	0.049	0.014	810.0	810.0	0.015	710.0	0.018	0.01.5	0.016	0.015	0.017	0.016	270	1000	11.00	2000	0.040	0.0.3	1000	1000	1	0.020	2000	0 025	0.027	0.026	0.026	0.000	0.030	0.033	0.04	0.035	0.017	0.038	0 53455 5	1341	0.047	0.051	1 2900	0.028	170.0	0.027	0.028	0.028	0.026	0.028	1000	100	103	0,136	Wen	0.044	1 150.0	0.077	0.036	0.035	0.023	0.023	0.027	0.019	0.020	120.0	0.024	020.0	0.023	0.031	0.035	9	0.037	0.035	0.034	000	1	0 1	2 0			Ц	Filt.	Ц
= = =	3 3	S E	ī,	5 5	5	110	iā	011	180	100	10.9	109	109	109	109	103	109	109	901	109	000	107	19	100	Life 1	0	9			1	9	3	ğ	0,	107	97	5	107	107	107	(G)	107 1	107	707	107	107	147	107	2	Ξ	Ξ	Ξ	=	= =	= =			=	Ξ	٥	Ξ	Ξ	Ξ	198	109	109	104	150	Ş	Ş	169	109	153	i i	3	100	Ş	Ř	Ž	ī		1	ž į	Ē	ž			Raw Fill	(mg/L as Ca
$\prod$		_		_			_			1	_	-	_				-		-	1	-	-	-	-	-	-	1	-		_		-	-	_					_				_	_		_	_	-			_	_	1	-	- -	-	_ _	-	L	-	_	_	_	L		L		L	-		_	-	L		L	L	-	L		-	-	1	1	$\downarrow$	1	1		- 1	
2 2 2	e i	r	î.	2 2	ů.	2	2	0.84	e X	3	<u>.</u>	0.88	0.88	C.XI	0 88	0.83	0.88	2		O.XX	2 2	,	3	4 2	2 2.33		2	2 2						c S	3	2	2	043	5	3	0.43	(A)	043	543	0.0	3	0.47	043	0.74	÷ 3	1,10	0.74	0 74 .	2	2 2	2 2		074	0.74	0.74	0.74	074	0.74	9	0.77	0.77	0.77	0.77	0.77	0.77	0.77	0.77	0.77	0 7/	0.77	0.77	6.7	3	1.70	7.70	2	3	2	5	•			Raw	(N)
1.20	0.95	3 3	e R	2 S	0.62	19.0	2	0.33	0.34		120	1.00	1,00	0.87	0 95	0.97	£.36	8	ŝ	26	0.50	ç ç		100	5	3 2			1	1		1	3	2	N. C	0 %	2	7,0	ů,	a.27	0.25	0.26	0.32	13.18	027	u.Ju	÷27	040	1.50	3	-	0	0.64	2	3 3	2 2	3 8	6	047	11.56	9.50	0.51	39.0	3	1.40	0.88	0.78	0.73	0.00	1	0.57	2.73	2		0.70	0.70	100	2.00	0 97	3		2		6.5				ī.	5
X.13	1.13	5 5	2 13	5 5	1.5	* 1.3		8.13	8.13		1.5	1.15	\$.15	8.15	\$.15	1.15	11.1	£.15	5	15		1			× 1.5	1.17	100	4 3	•				<b>X</b> 10	=	8,10°	* 10	# TG	<b>1</b> .10	=	1.70	E.10	8.10 ·	E.10 1	E 10	X.10	30.30	1 B13	1.10	X 36 ·	1 95.4	. X.	8.36	8.30	1 10	11. A. J.		7 6	\$.36	8.36	8.36	8.36	2.36	3.36	1.27	127	1.27	127	7.27	127		74.8	1.27	-		127	1.27	1.	3	9	1.03		a.U.		# 03 03		+	1	Raw Filt	0
		- - -	-	- - -	1-	<u>-</u>	. -	-	-	1	+	-	-	-	-1		-	_	-	-	-	1	1	-	- -	†	-	- -	1	1		1	1	-	-	-	-	-	-	-	-	-	-	1			-	7	-	1	-		-	1	- -	•	- -	-		-	-	-	-	-	-	-	-	-	-	-	-	-	-	+	-	-	. -	-	-	†- -  -	1	†	-	1	†		(see above)	6	Coagulant
150	130	120	100	2 1	E	8	8 8	3	20	0	,	ē	150	140	130	120	110	103	8	5	20 5	8 8	5		8	-   - 	=	=	ě	120	130	3	150	140	140	120	- 5	Juk	3	35	3	ž	50	40	ut	20	10	a t	1 150	141	130	1 120	130	100	8 8		2 3	1		in the	20	10	0	ī	120	110	100	ž	ě	è	£	ž.			10	ē		100	8	3	3 3	3 8	8 8	se	5			П	8
		1		- -	1				-					-		-		-	-						-		1		1	1					-		-			-	-	-	-	-								-			- -	-   -		-	-	-	-		-												-							1	1			N=XDEIG	(Y/N)	adjusted?	se Acid
																																				-				-																						1-										-														Dianx=V	(7/N)	adjusted?	Base
6.39	0 4	6.53	6.71	39 6	6.57	6.9%		7.29	1,4	7,7		i i	636	6.39	6.56	6.76	6.3	6.88	6.98	7.01			770	740	7,57		100			2 5	2	64	6.49	6.58	2 00	677	2	0.86	6.95	7.0%	725	740	7.19	7.31	743	7.53	73	8.13	5.93	CX1.6	6 (X.	4.17	6 33	2	0.01	640	6.78	7.10	12.	1	7.57	7.8	27	6.4	6.43	0.68	6.76	0.3	2	0.4	7.09	7.18	ì		137	1		-	6.26	2	611			3 3		1		맞	Coag.

Page 6 of 10

MWDJAR44	WWDJAR44	MWDJAR44	MWDJARA	MWDJAR41	MWUAKA	WWDJAR43	HWDIAR43	MWDJARAJ	MWUIARA	MWDIARAS	MWDJAR43	MWDJARAS	MWDIARA	MWDIARAS	TWENT CHAN	TAU DIA	THE PARTY OF THE P	MACOARA	MACOAKA.	MWUJARAZ	MWDJAR42	MWDJAR42	MWDJAR42	MWDJAR42	MWDJAR42	MWDIAR42	WWDIARAI	MWDJAR42	LINALIGNAM	WWD/AR4:	MWDIAR4	MANICAN	ARATCHE A	MW'DIARA!	MWDIARA	MW.DJAN41	KWDIAR4)	MWDIARA	XWDJAR40	W.D.ARAD	THE CONTRACT	NWDIARA:	1000	THE CONTRACT	MI DIAR	MWUJAKAO	MWDJAR40	MWDJAR41	MWDIARAG	MWDJAR4:	MWDJARau	MWDIAR40	WWDIAR4I)	MWDJAR40	MWDJAR40	MWDIARAH	MWDJARA	MWDJAR4	MWDIAR4	MWDJARA	MWDJAR4	WWDIARA	MWDJARA	MWDJARA	MWDJAR4	MWDIARA	MWUAKA	310000	THE CONTRACT	NACTOR AND AND AND AND AND AND AND AND AND AND	WWUJAKU	MACIONA	340000	MWOJARO	MWDIARO	MWULAKIY	NA CONTRACTOR	MWUJARJA	MUNICA	TOWN TOWN	MWDIAR 19	MWINNE	MWUARIN	MWDIARIN .					21.007
ž A	£	50	\$0	8 5	έĮξ	8	55	8	i X	35	8	8	s	8	2	£   3	5 3	s =	3 8	×	80	¥	8	50	50	50	ž	50	9.	8	*	5	3	£	3	50	S	5	60	2	8	3 9	5 8	5	=	Ē	8	3	S	65)	£	3	60)	8	8	8 3	(81)	68	100	(3)	100	1001	<b>8</b>	ŝ	8	8 8	3 8	8	5 2	3 8	2	2	3 2		8	9	\$ 8	8	8	S	8 9	8 3	3 8	\$ 8		-	+	-	200
-	- 3		-		-	-	-	<u>_</u>	-	موا		,	3		-1;	٠ ا ١	4,	,,	,				12	2	2.	- 2		4	,,	,,	.,	264	2,		_	-	2	12	,	, ,	1			١.						,,		2.		12	-	,	, ,	,,,	,,		,,	-	2	2	2			,		,	,				,		-	,,,			2	,,		-		+	+:	+	W SPW
= =	11 2.70	11 2.20	3.1	20		, ,	18 2.0	18 2.0		2.10	.18 2.21	22	1	22	271	-}-		-}-	- -	1.81	╀	-	2.37 1.79	-	2	-	-	-		_	2 -	2   2	2	2	2	2	2.69	2	57	57	3	3 3		ין ני ין ני	3 3	3			1.0	57	57 1 70	57   1,80	57 1 214	57 2.11	57	57 24	3 55	- 5	1.9	55 1.95	55   2.14	55 1 20	55 - 2.20	\$ 2.3	55 24	55 2.5	100	, ,			-	-	+	1.00	+	+	1	+	+	-	_ ,	+	- -	264 269	- -	+	-†	Raw Filt.	1 114441
1 800%	0.0%	0.00	0.00,6	u ox	0.081	130.0	1 0.081	180.0	000	0.081	180.0	140.0	120.0	0.0%	O OX			1,000	0.001	0.00	9.001	1001	0.061	0.061	0.061	19001	10001	0.001	5 0.079	0.074	0.079	0.079	0.079	200	0.074	7 0070	0.070	0.079	77.2		D CALL	O.				0100	0	0.042	0 K	004.7	0.042	0 142	0 542	- K	2000	0 0	1 0 (4)	0.143	0,043	1 01047	0.043	10001	0.043	0.043	0.023	Q.C.			0.00	2000	0.054	4	J.	11000		1000	0000	1000	0.040	000	0.039	0.049	0.059	4 CH 11 6		$\dagger$	+	Raw	4
0.041	1 1	1 1	ΙÌ	- 1	0.026	1	1	- 1	1	0.036	\$10.0	950.0	0.036	0.039	OCA	0 0	0000	0200	2,11,12	V.028	0.028	11.U.ZA	0.028	0.025	0.027	0.031	0.034	20.0	13,612,0	001	2	040	ŝ.	0 PE		850.0	O OXAS		9100	0017	0 017	000	0.000	0.00	1000	27.00	0.021	1200	0.023	0 024	0.026	0.028	0.00	0,032	5000	0 042	8.027	0.025	0.027	0 026	0.030	0.027	0.029	0.029	0.031	202	0.040	1	0.00			0.023		1	0.02.5		2010	2020	0,0,0	000	0.03	200	0030	0.05				File	(444)
<u> </u>	103	103	103	<u> </u>	ŝ	3	166	ē	3	ş	ŝ	ā	š	ē	5	Ž		į	5 5	10,	ē	ē	ē	113	103	FQ3	101	=	£	£	٤	2	Ē	É	É	ž	i	£	٤			5					Ē	9	Ē	2	ã	E I	101	101	Ξ		ē	2	2	Ē	123	123	123	Ē	2	Ē	3   5		5		2	104		9	3	109	5	2 5	19	3	5	3	00	3 3	116			Raw	
$\prod$																				-	L													_					_{			-	-			-					-	_																																				Fift	וננייי
- J	Н	-	Н		0 47	-	Н	4	╀	H	-	2	5	3		3	1 :		2 5	0.5	0.73	9	0.75	0.75	0.75	0.75	37.0	0.75	0 85		2	2 2		2	2	2	*	2		= 1		<u>.</u>				1.5	2	100	3 10	3 =	3.10	3.30	1 (01.1)	. i	=	ē   =	9.85	5.K.S	0.85	0.85	0.85	U.R.5	2		2						- -	-		9	2			2					0.48	2 4		-	Zán.	Raw Filt	121
	0.27	123	0.51	8	200		1.20	0.7%	3 6	0.67	0.61	25	릸	a C	3		1	2 2	9	ž	, ye	ě	0.85	0.85	0.51	0.6%	11.57	2	0.9%	<u>.</u>	0.00	2	3	5	0.50	0.05	1		3	2	2	3				3	2	3	27.	25	0.20	124	17.27	2	ş (		385	- Si	031	35.0	13	120	5	2	200	2	100		3 2	3 2	1.00	2		0.68	S	2	Ę	2	9				1 2	: 3	-	$\downarrow$	+	+	
198	755	7.99	7.94	S	20.0	3	1.32	8		8.32	X.32	£	1.53	13	S.	13		1	-	-	* 17		1.17	8.17	1.17	X.17	1.17	K.17 :	X.13	20		*			×II		2	×	30.8	× .	*05	* 05		0.017	200		*.03	1.05	8.03	0.0	805	1 517.1	1 50'8	X.O.S.	ā	20.5		1.21	723	1.23	X 2.1	(7)	5	*	E	125				1.60	1.76	-	20	3.26	1.26	146	0.40	7.26	1.26		* 20	* 76	120	1.26		1	Xav Till	7	
- -	_	_	1	_				-	-	_	_		_	-	-	1			-		-		-	_	-	٠	1	_		-	-	_		-	_	-	-	_	-	-	-	-	4	1	-	. -	. _				-	_	۵	-	4	-	ا.		-	_	4		_	-	_	-4	4	4		4				-	-		-		. -		-	-	-			(See above)	(See above)	5	,
ş	20	70	٥	. S	£ 3	120	110	ã	8 8	8	8	8	40	ĕ	20	i i	٥	1100	100	3	2	2	R	ŧ	ĕ	20	ιg	a	ŝ	E	3	£	š	8	30	3	IG.	0	1901	2	200	160	ŝ	i e	126	200	100	8	ž	2	Ē	Ř	48)	'n	뜅	5	: 18	Ē	×	15	710	g	35	3	5	ij,	5 6	> 3	Š	S	Ş	1	3	5 8	ž	3	2	9 8	3 3	5 1		5 6	3 3	5 0	ı	1	1	1_	_i
																																																												-																					1				DISOR	(N/A)	William .	adjusted?	
																														-											-																																									1			Nexuello	NAVER NAVER	None nine	adjusted?	
7.36	7.50	7.76	1.14	\$ 93	5.99	2	6.33	6.49	2	6.3	6.71	7.13	7,22	7.36	7,5	725			2	0.51	6.00	9.53		7.03	7.12	7.33	7.49	1.15	6.19	1	6.61	6.73	6	g	7.05	725	747	99	5		311	61		c .	, , , ,	6.7	9.7	0.89	8	7.92	713	7.26	7331	7.54	7.68	7.85	6.75	2 2	6.91	6.97	705	121	7,	7.57	7	7.60	7 108		2		000			0.0	6.2	245		7.12	7.29	į	71/2	ìè	1	1		١.	3	1	١,

Page 7 of 10

N. P. N. P	Study ID	Wa	iter	TC	oc .	LIV	/-254	Aikai	inity	Turn	idity	pH	<del></del>	Coacu	lation Cond	itions	
Martine	Judy ID			(mç	1/L)					(N1	U)		Coagulant				Coag.
Company   Comp				Raw	Filt.	Raw	Fift.	Raw	Filt.	Raw	Filt.				adjusted?		
Marging			<u> </u>									ļ	(See above)				()
Second   19	MWDIARA	50	1		2.32	: UUKr	0.035	1 103	<del> </del>	1 1 1/1	1 11 21	7 90 (	<del> </del>	4/1	DIBINXAN	) Dianx=N	714
Marchand   Part   Marchand   Ma			-						<del>                                     </del>				1				
Marchand   S	MWDJAR44	50						103					1				
Marting   Mart									Ī								
Marchane   19			ļ <u>.</u>						L								
Membrane   19									<u> </u>								
Marchane   19									<del> </del>								
Martine   18			<del></del>														
WYSTAME   St.   2,00   1,00   104   105   105   107	MWDJAR44	50	i							1.30	0.52	7.99					6.44
MYSTART   St.   26   22   10   10   10   10   10   10   10													<del></del>				
EMPORANCE   20			ļ			0.0%6			ļ				-1				
MYDDARES   19			ļ						<u> </u>				<del>  </del>				
MYDIAMS   S.   26   26   15   100			-			1			<del> </del>								
WYDLANES   S.   246   134				2.46	2.07		0.036	105					1			1	
MYGMARS   S.   246   126   169   169   169   161   162   161   1		50								0.87	0.33	2.14					
MYDIANE   Se			!														
MANDARS   30			ļ													ļ	
MYDIANES   S						-			<del> </del>								
MYDIANES   S   1.26   1.90   1.002   1.003   1.002   1.003   1.002   1.003   1.004   1.005   1.004   1.005   1.004   1.005   1.006									1								
Mystolands   Sc	MWDJAR45		i					1 105	<u> </u>								
MYDIAME   19			1														
MYDIANE   SI						<u> </u>										ļi	
MYDIANE   6			<u> </u>						<del> </del>								
MYDLAKE   10			<u>:</u>						<del> </del>				<del></del>			<del>  -                                   </del>	
MANDARS   No			<u> </u>						<del></del>								
WYDIASE   S			·		1.36		0.014	105				X.14		176			
MYDIAMA   S	MWDJAR45											13.14	<del></del>				
WYDIASE   S0			l .						1								
WODIANG   30			1						<del> </del>							<del> </del>	
MYDIARD   90			<del>                                     </del>						<del> </del>								
Memorian   Memorian			<del></del>						1								
MWDJAKR   Sc					2 (X)	() ()4()	9410						1 1 1	50			
MYDIARR   3-	MWDJAR46	50								0.73	90.0						
MWDJAR6   St									,								
MyDiARe   Se   2,46   159   0.000   0.004   0.05   0.07   0.09   131   1   1   0.00   0.005   0.006			<u> </u>						!							<u> </u>	
MWDJARE   9									<del></del>							i	
MWDJAR6   S			<del> </del>						i				1 1	[11)		1	
MWDJAR6	MWDJAR46	50	1	2.40	1.26	0 040 j	6 023	1415		0.71	1.100	\$.11	1	120			6.50
WWDJARG   9																	
NAME   19			<u> </u>						<u> </u>								
WWDJARG   59			-						ļ								
MWDJARG   99			i						<del>                                     </del>							<del> </del>	
NWDIJART   50				2 79	2.70	0.063					0.50		1 1	10			7.85
NWDLARE   S0		5()			$\overline{}$								<del></del>				
MWDDARF   S0					-				1				ئىــــــــــــــــــــــــــــــــــــ				
MWDIARE   50			!						<u> </u>								
MWDIARAF   90			<del>!</del>						<del></del>								
MWDIARAF   50			<del> </del>														
MYDIARK   30			<del></del>						-				1 1				
MWDJARRT   50	MWDJAR4"									0.42	0.54		<u> </u>				
MWDDARR   S0   2.79   1.53   0.063   0.021   102   0.42   0.04   1.23   1   1.20   0.46																	
MWDJARR   S0			!						<del> </del>								
MYDIARAT   S0			i													<del></del>	
MWDIARA   S0			<del> </del>						<del> </del>							i	
MWDIARA   50			I						i _				1 1	150			6.20
MWDIARR\$   100   3.31   3.21   0.126   0.103   73   2.40   0.83   7.91   1   100   1.20   1	MWDIAR4"	50						102		0.42		8.23					
MWDIAR48																	
MWDIAR8																<del> </del>	
MWDIARR   100   3.31   2.36   0.126   0.061   73   2.40   0.52   7.91   1   40   0   0.83   MWDIARR   100   3.31   2.22   0.126   0.054   73   2.40   0.55   7.91   1   50   0   6.79   MWDIARR   100   3.31   1.87   0.126   0.049   73   2.40   0.56   7.91   1   50   0   0.64   MWDIARR   100   3.31   1.87   0.126   0.049   73   2.40   0.50   7.91   1   70   0   0.51   MWDIARR   100   3.31   1.78   0.126   0.049   73   2.40   0.50   7.91   1   70   0   0.51   MWDIARR   100   3.31   1.78   0.126   0.049   73   2.40   0.05   7.91   1   70   0   0.51   MWDIARR   100   3.31   1.78   0.126   0.049   73   2.40   0.05   7.91   1   10   0   0   0.52   MWDIARR   100   3.31   1.78   0.126   0.049   73   2.40   1.10   7.91   1   90   0   0.52   MWDIARR   50   2.55   2.55   0.057   0.057   0.94   0.34   0.36   7.93   1   0   0   0   7.95   MWDIARR   50   2.55   2.25   0.057   0.051   0.94   0.34   0.36   7.93   1   0   0   0   7.36   MWDIARR   50   2.55   2.20   0.057   0.045   94   0.34   0.17   7.93   1   30   0   7.51   MWDIARR   50   2.55   2.14   0.057   0.041   94   0.34   0.17   7.93   1   30   0   7.54   MWDIARR   50   2.55   1.86   0.057   0.057   0.045   94   0.34   0.17   7.93   1   30   0   7.54   MWDIARR   50   2.55   1.86   0.057   0.057   0.045   94   0.34   0.17   7.93   1   30   0   7.54   MWDIARR   50   2.55   1.86   0.057   0.057   0.045   94   0.34   0.19   7.93   1   30   0   7.54   MWDIARR   50   2.55   1.86   0.057   0.057   0.057   0.045   94   0.34   0.19   7.93   1   30   0   7.24   MWDIARR   50   2.55   1.86   0.057   0.0		<del></del>							-								
MWDIAR48   1100   3.31   2.22   0.126   0.054   73   2.40   0.056   7.91   1   50   6.79																	
MWDIARR   100   3.31   1.89   0.126   0.049   75   2.40   0.95   7.91   1   70   6.15   MWDIARR   100   3.31   1.83   0.126   0.050   73   2.40   0.83   7.91   1   80   6.79   MWDIARR   100   3.31   1.78   0.126   0.050   73   2.40   1.00   7.91   1   80   6.79   MWDIARR   50   2.55   2.55   0.057   0.057   94   0.34   0.36   7.93   1   0   0   7.35   MWDIARR   50   2.55   2.25   0.057   0.051   94   0.34   0.36   7.93   1   0   0   7.35   MWDIARR   50   2.55   2.20   0.057   0.051   94   0.34   0.17   7.93   1   10   0   7.36   MWDIARR   50   2.55   2.20   0.057   0.045   94   0.34   0.17   7.93   1   20   7.71   MWDIARR   50   2.55   2.25   2.25   0.057   0.045   94   0.34   0.17   7.93   1   20   7.71   MWDIARR   50   2.55   2.14   0.057   0.041   94   0.34   0.19   7.93   1   30   7.59   MWDIARR   50   2.55   1.36   0.057   0.052   94   0.34   0.19   7.93   1   30   7.59   MWDIARR   50   2.55   1.36   0.057   0.052   94   0.34   0.19   7.93   1   30   7.59   MWDIARR   50   2.55   1.36   0.057   0.052   94   0.34   0.19   7.93   1   50   7.35   MWDIARR   50   2.55   1.36   0.057   0.032   94   0.34   0.20   7.93   1   50   7.35   MWDIARR   50   2.55   1.46   0.057   0.028   94   0.34   0.20   7.93   1   50   7.25   MWDIARR   50   2.55   1.67   0.057   0.028   94   0.34   0.20   7.93   1   50   7.25   MWDIARR   50   2.55   1.67   0.057   0.028   94   0.34   0.20   7.93   1   50   7.25   MWDIARR   50   2.55   1.67   0.057   0.028   94   0.34   0.20   7.93   1   50   7.25   MWDIARR   50   2.55   1.67   0.057   0.028   94   0.34   0.20   7.93   1   50   7.25   MWDIARR   50   2.55   1.67   0.057   0.028   94   0.34   0.20   7.93   1   50   7.25   MWDIARR   50   2.55   1.67   0.057   0.028   94   0.34   0.20   7.93   1   50   7.25   MWDIARR   50   2.55   1.67   0.057   0.024   94   0.34   0.20   7.93   1   100   7.25   MWDIARR   50   2.55   1.56   0.057   0.021   94   0.34   0.22   7.93   1   100   7.25   MWDIARR   50   2.55   1.56   0.057   0.021   94   0.34   0.22   7.93   1   100   7.25   MWDIARR   50   2.55														50			6.79
MYDIARA   100   3.31   1.83   0.126   0.050   73   2.40   0.83   7.91   1   80   6.09																	
MWDJAR48   100   3.31   1.78   0.126   0.149   73   2.40   1.10   7.91   1   90   5.32   MWDJAR48   50   2.55   2.55   0.057   0.057   94   0.34   0.36   7.93   1   0   0   7.95   MWDJAR48   50   2.55   2.20   0.057   0.051   94   0.34   0.36   7.93   1   0   0   7.36   MWDJAR48   50   2.55   2.20   0.057   0.051   94   0.34   0.17   7.91   1   10   7.36   MWDJAR48   50   2.55   2.20   0.057   0.051   94   0.34   0.17   7.93   1   20   7.71   MWDJAR48   50   2.25   2.14   0.057   0.041   94   0.34   0.17   7.93   1   30   7.59   MWDJAR48   50   2.25   1.70   0.057   0.057   0.051   94   0.34   0.19   7.93   1   30   7.59   MWDJAR48   50   2.25   1.70   0.057   0.057   0.053   94   0.34   0.20   7.93   1   40   7.48   MWDJAR48   50   2.25   1.80   0.057   0.057   0.052   94   0.34   0.20   7.93   1   50   7.39   MWDJAR48   50   2.25   1.67   0.057   0.022   94   0.34   0.20   7.93   1   50   7.29   MWDJAR48   50   2.25   1.67   0.057   0.022   94   0.34   0.20   7.93   1   50   7.29   MWDJAR48   50   2.25   1.67   0.057   0.022   94   0.34   0.20   7.93   1   50   7.29   MWDJAR48   50   2.25   1.67   0.057   0.024   94   0.34   0.20   7.93   1   50   7.29   MWDJAR48   50   2.25   1.67   0.057   0.024   94   0.34   0.20   7.93   1   50   7.29   MWDJAR48   50   2.25   1.67   0.057   0.024   94   0.34   0.20   7.93   1   100   7.22   MWDJAR48   50   2.25   1.67   0.057   0.024   94   0.34   0.20   7.93   1   100   7.23   MWDJAR48   50   2.25   1.55   0.057   0.024   94   0.34   0.24   7.93   1   100   7.23   MWDJAR48   50   2.25   1.55   0.057   0.021   94   0.34   0.34   0.42   7.93   1   100   7.02   6.80   MWDJAR48   50   2.25   1.55   0.057   0.021   94   0.34   0.42   7.93   1   110   0.55   MWDJAR48   50   2.25   1.57   0.057   0.021   94   0.34   0.42   7.93   1   110   0.55   MWDJAR48   50   2.25   1.49   0.057   0.021   94   0.34   0.42   7.93   1   110   0.55   MWDJAR48   50   2.55   1.49   0.057   0.021   94   0.34   0.42   7.93   1   110   0.55   MWDJAR48   50   2.55   1.49   0.057   0.021   94   0.34																	
MWDIARAS 50 2.55 2.55 0.057 0.057 94 0.34 0.34 0.36 793 1 0 0 7.95 MWDIARAS 50 2.55 2.32 0.057 0.051 94 0.34 0.34 0.17 7.91 1 10 7.36 MWDIARAS 50 2.55 2.32 0.057 0.051 94 0.34 0.17 7.91 1 10 0 7.36 MWDIARAS 50 2.55 2.14 0.057 0.057 0.051 94 0.34 0.17 7.91 1 30 7.71 MWDIARAS 50 2.55 1.67 0.057 0.032 94 0.34 0.34 0.20 7.91 1 30 7.91 MWDIARAS 50 2.55 1.74 0.057 0.032 94 0.34 0.20 7.91 1 50 7.91 1 7.91 MWDIARAS 50 2.55 1.74 0.057 0.032 94 0.34 0.20 7.91 1 50 7.91 MWDIARAS 50 2.55 1.67 0.057 0.032 94 0.34 0.20 7.91 1 50 7.91 MWDIARAS 50 2.55 1.67 0.057 0.032 94 0.34 0.20 7.91 1 50 7.91 MWDIARAS 50 2.55 1.67 0.057 0.032 94 0.34 0.20 7.91 1 50 7.91 MWDIARAS 50 2.55 1.67 0.057 0.032 94 0.34 0.20 7.91 1 50 7.91 MWDIARAS 50 2.55 1.67 0.057 0.032 94 0.34 0.20 7.91 1 50 7.91 MWDIARAS 50 2.55 1.67 0.057 0.032 94 0.34 0.20 7.91 1 70 70 70 7.27 MWDIARAS 50 2.55 1.67 0.057 0.032 94 0.34 0.34 0.19 7.93 1 70 70 70 7.27 MWDIARAS 50 2.55 1.67 0.057 0.032 94 0.34 0.20 7.93 1 70 70 70 70 70 7.27 MWDIARAS 50 2.55 1.67 0.057 0.032 94 0.34 0.20 7.93 1 70 70 70 70 70 70 70 70 70 70 70 70 70									<del>                                     </del>								
MWDIAR4\$ 50		50	1(A)						<del> </del>								
MWDIARR 50 2.55 2.20 0057 0.045 94 0.34 0.17 7.93 1 20 7.71 MWDIARR 50 2.55 1.14 0.057 0.041 94 0.34 0.09 7.93 1 30 7.55 MWDIARR 50 2.55 1.86 0.057 0.007 0.			<del>                                     </del>						<del>                                     </del>								
MWDIAR48   50   2.55   2.14   0.057   0.041   94   0.34   0.09   7.93   1   30   7.59   30   7.59   30   30   7.59   30   30   30   30   30   30   30   3			L											20			7.71
MWDIAR48 50 2.55 1.74 0.057 0.022 94 0.34 0.20 7.91 1 50 7.39  MWDIAR48 50 2.55 1.64 0.057 0.028 94 0.34 0.20 7.91 1 50 7.39  MWDIAR48 50 2.55 1.64 0.057 0.028 94 0.34 0.20 7.93 1 60 7.30 7.31  MWDIAR48 50 2.55 1.64 0.057 0.058 94 0.34 0.20 7.93 1 70 90 7.35  MWDIAR48 50 2.55 1.64 0.057 0.052 94 0.34 0.22 7.93 1 90 7.35  MWDIAR48 50 2.55 1.64 0.057 0.022 94 0.34 0.32 7.93 1 1 90 7.35  MWDIAR48 50 2.55 1.65 0.057 0.022 94 0.34 0.34 0.32 7.93 1 1 100 7.02  MWDIAR48 50 2.55 1.55 0.057 0.022 94 0.34 0.34 0.35 7.91 1 100 7.02  MWDIAR48 50 2.55 1.55 0.057 0.022 94 0.34 0.34 0.35 7.91 1 100 6.95  MWDIAR48 50 2.55 1.55 0.057 0.022 94 0.34 0.34 0.35 7.91 1 100 6.95  MWDIAR48 50 2.55 1.55 0.057 0.022 94 0.34 0.34 0.35 7.91 1 100 6.95  MWDIAR48 50 2.55 1.55 0.057 0.022 94 0.34 0.35 7.91 1 120 6.95  MWDIAR48 50 2.55 1.56 0.057 0.022 94 0.34 0.35 7.91 1 120 6.95		50			<del>,</del>					0.34							
MWDJAR48 50 2.55 1.64 0.057 0.028 94 0.34 0.19 7.93 1 60 7.34 MWDJAR48 50 2.55 1.64 0.057 0.028 94 0.34 0.19 7.93 1 70 70 7.35 MWDJAR48 50 2.55 1.64 0.057 0.028 94 0.34 0.19 7.93 1 70 70 7.35 MWDJAR48 50 7.35 1.61 0.057 0.028 94 0.34 0.20 7.93 1 70 70 7.35 MWDJAR48 50 7.35 1.61 0.057 0.022 94 0.34 0.20 7.93 1 70 70 7.35 MWDJAR48 50 7.35 1.55 0.057 0.022 94 0.34 0.34 0.20 7.93 1 100 7.35 MWDJAR48 50 7.35 1.55 0.057 0.023 94 0.34 0.34 0.40 7.93 1 100 7.02 7.02 MWDJAR48 50 7.35 1.55 0.057 0.023 94 0.34 0.34 0.40 7.93 1 100 7.02 7.02 MWDJAR48 50 7.35 1.55 0.057 0.023 94 0.34 0.34 0.34 0.40 7.93 1 100 7.02 7.02 7.02 7.02 7.02 7.02 7.02 7.																	
MWDIARAK 50 2.55 1.64 0.057 0.02K 94 0.34 0.19 793 1 70 7.27 MWDIARAK 50 2.55 1.67 0.057 0.026 94 0.34 0.20 793 1 80 7.25 MWDIARAK 50 2.55 1.67 0.057 0.024 94 0.34 0.20 793 1 80 7.25 MWDIARAK 50 2.55 1.67 0.057 0.024 94 0.34 0.22 793 1 1 80 7.25 MWDIARAK 50 2.55 1.67 0.057 0.024 94 0.34 0.22 793 1 1 90 7.21 MWDIARAK 50 2.55 1.69 0.057 0.024 94 0.34 0.34 0.22 793 1 1 100 7.02 MWDIARAK 50 2.55 1.55 0.057 0.023 94 0.34 0.34 0.27 1 1 110 1 6.95 MWDIARAK 50 2.55 1.55 0.057 0.022 94 0.34 0.34 0.38 791 1 110 1 6.95 MWDIARAK 50 2.55 1.55 0.057 0.022 94 0.34 0.40 7.99 1 1 120 6 80 MWDIARAK 50 2.55 1.56 0.057 0.022 94 0.34 0.42 799 1 1 120 6 80 MWDIARAK 50 2.55 1.56 0.057 0.021 94 0.34 0.34 0.42 799 1 1 120 6 80 MWDIARAK 50 2.55 1.56 0.057 0.021 94 0.34 0.34 0.42 799 1 1 120 6 80 MWDIARAK 50 2.55 1.49 0.057 0.021 94 0.34 0.34 0.42 799 1 1 140 6 0.55								<del></del>					1			<del> </del>	
MWDIARAR 50 2.55 1.67 0.057 0.024 94 0.34 0.20 7.93 1 80 7.15 MWDIARAR 50 2.55 1.61 0.057 0.024 94 0.34 0.22 7.93 1 90 90 7.15 MWDIARAR 50 2.55 1.61 0.057 0.024 94 0.34 0.22 7.93 1 90 90 90 90 90 90 90 90 90 90 90 90 90			<u></u>						ļ								
MWDJAR48 30 2.55 1.61 0.057 0.024 34 0.34 0.22 7.93 1 90 7.13 MWDJAR48 30 2.55 1.69 0.057 0.021 94 0.34 0.34 0.40 7.90 1 100 7.02 MWDJAR48 30 2.55 1.56 0.057 0.021 94 0.34 0.34 0.40 7.90 1 100 6.95 MWDJAR48 30 2.55 1.56 0.057 0.022 34 0.34 0.34 0.38 7.90 1 1 110 6.95 MWDJAR48 30 2.55 1.56 0.057 0.022 34 0.34 0.34 0.38 7.90 1 1 110 6.95 MWDJAR48 30 2.55 1.56 0.057 0.021 34 0.34 0.34 0.38 7.90 1 1 120 6.80 MWDJAR48 30 2.55 1.56 0.057 0.021 34 0.34 0.34 0.34 0.35 7.90 1 1 120 6.80 MWDJAR48 30 2.55 1.56 0.057 0.021 34 0.34 0.34 0.34 0.35 7.90 1 1 140 6.65 6.65 MWDJAR48 30 2.55 1.44 0.050 34 0.050 34 0.04 7.90 1 1 140 6.55 MWDJAR48 30 2.55 1.47 0.057 0.020 34 0.40 0.34 0.44 7.90 1 1 140 6.55									<del> </del>								
MWDJARAR   30   2.55   149   0.057   0.023   94   0.34   0.40   7.93   1   100   7.02   MWDJARAR   30   2.55   1.55   0.057   0.021   94   0.34   0.34   0.38   7.93   1   110   6.93   MWDJARAR   50   2.55   1.55   0.057   0.022   94   0.34   0.42   7.93   1   120   6.80   MWDJARAR   50   2.55   1.56   0.057   0.022   94   0.34   0.42   7.93   1   120   6.80   MWDJARAR   50   2.55   1.56   0.057   0.020   94   0.34   0.42   7.93   1   150   6.63   MWDJARAR   50   2.55   1.49   0.057   0.020   94   0.34   0.42   7.93   1   140   0.55   0.55   0.55   0.56   0.55   0.56   0.55   0.56   0.55   0.56   0.55   0.56   0.55   0.56   0.55   0.56   0.55   0.56   0.55   0.56   0.55   0.56   0.55   0.56   0.55   0.56   0.55   0.56   0.55   0.56   0.55   0.56   0.56   0.55   0.56   0			<del> </del>						<del> </del>								
MWDIAR48   \$0   2.55   1.55   0.057   0.023   94   0.34   0.38   7.93   1   110   6.95   MWDIAR48   \$0   2.55   1.58   0.057   0.022   94   0.34   0.42   7.93   1   120   6.81   6.63   MWDIAR48   \$0   2.55   1.56   0.057   0.021   94   0.34   0.44   7.93   1   130   6.63   MWDIAR48   \$0   2.55   1.49   0.057   0.020   94   0.34   0.44   7.93   1   140   6.53   MWDIAR48   \$0   2.55   1.47   0.057   0.020   0.44   0.34   0.34   0.44   7.93   1   140   6.53   0.55   0			1										1				7.02
MWDJARAK   50   2.55   1.58   0.057   0.022   94   0.34   0.42   7.93   1   120   6.80   MWDJARAK   50   2.55   1.56   0.057   0.021   94   0.34   0.42   7.93   1   130   6.63   MWDJARAK   50   2.55   1.49   0.050   94   0.34   0.44   7.93   1   140   6.55   MWDJARAK   50   2.55   1.47   0.057   0.020   0.44   0.34   0.70   7.91   1   150   6.44		50									W.T.0						
MWDJARAX 50 2.55 1.49 0.057 0.020 94 0.34 0.44 7.93 1 140 0.55 MWDJARAX 50 2.55 1.47 0.057 0.020 04 0.34 0.70 7.91 1 150 6.44	MWDJAR4X		<u> </u>						ļ								
MWDJARAS 50 2.55 1.47 (1057 0.02)1 64 0.34 0.79 7.91 1 150 6.44			<del> </del>						<del>}</del>						<del></del>	<u> </u>	
			I						-						<del></del>		
	MA.DIVK4x	50	<del></del>	2.55	141	0.057	0.024	94				791					

Page 8 of 10

Study ID		iter	70			-254	Alkai		Turb		p)-				lation Cond		
	% CRW	% SPW	Raw	Filt.	Raw	/cm) Filt,	(mg/L 23		[NT		1)	F:0	Coagulant	Dose	Acid	Base	Coag.
			-N#W		NAW .	riii.	Raw	Filt.	R#W	Filt.	Raw	Fitt.	(see above)		adjusted? (Y/N)	adjusted?	pН
		<del> </del>		-				-					(SEE BUCVE)		blank=N	(Y/N) blank=N	0
MWDJAR49		1 100	2.33	2,36	0.077	0.074	1 73	i		0.85	8.07		1	D			8.07
MWDJAR49		100	2,33	2.20	0.077	0.064	73			0,57	1.07		1	10			7 65
MWDJAR49		100	2.33	2.19	0.077	0.050	73	1		0.75	1 07		1	20		1	741
MWDJAR49		100	2.33	2.03	0.077	0.046	73			0.56	\$.07		1	30			7.24
MWDJAR49		100	2.33	1.84	0,077	0.043	73			0.72	8.07		1	40			7.15
MWDJAR49		100	2.33	1.75	0,077	0.040	73			0.75	\$.07		1	50		<u> </u>	7 05
MWDJAR49	ļ	100	2.33	1.72	0.077	0.040	73			0.53	X.07		1	60			7.0x1
MWD/AR49		100	2.33	1.78	0.077	0.037	73			0.47	\$.07		1	70			6.87
MWDJAR49	L	100	2.33	1.41	0.077	0.035	73	<del> </del>		0.47	8.07		1	90			6.73
MWDJAR49		100	2.33	1.54	0,077	0.030	73			0.56	\$.07	_	1	100			6.58
MWDJAR49		100	2,33	1.31	0.077 (	0.028	73	Ī		0,60	8.07		1	110			6.45
MWDJAR49		1(X)	2.33	1.30	0,077 (	0.011	73	<del></del> -		0.45	x 07		1	120			6.38
MWDJAR49		100	2.33	1,25	0.077	0.029	73			0,60	8.07		1	130			6.23
MWDJAR49		) (X)	2.33	1.20	0,077	0.028	73			0.65	8.07		1	140			6.14
MEWDIARS	1(X)		2.37	2.40	0.048	B.IM\$	131		0.76	(1.5)	8.23		1	0			1.23
MWDJARS	100		2.37	2.27	0.048	0.043	131	<u> </u>	0.76	0.57	8.23			10			7.88
MWDIARS	100	<del> </del>	2.37	2.19	0.048	0.038	131	ļ	0.76	0.47	1.23		1 1	20		<del> </del>	7.77
MWDJARS MWDJARS	100		2.37	2.07	0.048	0.036	131		0.76	0.59	2.23 2.23			40			7.52
MWDIARS	100	<del> </del>	2.37	1.90	0.048	0.029	131	<del></del>	0.76	0.46	\$.23			50		<del> </del>	7.44
MWDJARS	100	<del>                                     </del>	2.37	1.94	0.048	0.028	131	<del>                                     </del>	0.76	0.78	8.23	-	1	60	<del></del> -		7.36
MWDJARS	100		2.37	1,34	0.048	0.026	131		0.76	0.77	8,23		1	70			7.25
MWDIARS I	100		2.37	1.77	0.048	0.025	131		0.76	0.\$2	8.23		1	80			7.16
MWDJARS	) (N)		2.37	1.75	0.048	0.024	131		0.76	0.85	8.23		1 1	90			7.05
MWDIARS	TUX	ļ	2.37	1.68	0 (14%	0.015	131	<u> </u>	0.76	0.86	8.23			IIX		<u> </u>	7 06
MWDJAR4	100	1.00	1.37	1.65	0.048	0.015	131	<del> </del>	6.76	1.30	8.23	<del> </del>	1	110	<del></del>	<del> </del>	6.97
MWDIARSO (		100	3.90	1.69	0.110	0.072	77	<del> </del>	1.7	0.79	8.(k) 8.(X)			10		<del></del>	8 00 7 44
MWDJAR30		100	3.90	3.17	0.110	0.072	77	<del>                                     </del>	1.7	0.39	8 (R)		<del></del>	20		<del>  </del>	7.15
MWDJAR50		100	3.90	2.81	0.116	0.037	77	i	1.7	0.38	N.(N)		1	30			6.99
MWDIARSH I		100	3.90	2.3X	0,110 (	0.032	77	<del></del>	1.7	0.31	8 (X)	-	<del></del>	40			6.92
MWDJAR50		100	3.90	2.25	0110	0.029	77		1.7	9.66	3 (X)		1	5()			6.29
MWDJAR50		100	3 %)	2.16	0.110	0.024	77	1	17	0,60	X (X)		1	60			6.66
MWDIAR50 1		100	1,90	2.(K)	0.110	0.020	77		1.7	().5X	2.(X)		1 1	70			6.45
MWDJAR50		100	3.90	1.99	0,110 )	6 020	77	<u> </u>	1.7	0.65	% (X)		1 (				6.31
MWDJAR30		( (K)	3 90	2 (X)	0 [10 ]	0.021	. 77		17	0.67	% (X)		1 !	90		<u> </u>	6.14
MWDJAR50		100	3.90	2.03	0.110	0.018	77		1.7	1.10	8.(X) (X) X		1 1	100			5.93
MWDJARSI MWDJARSI		100	3.90	3.17	0.097	0.103	21		0.85	2,30	7,80		<del>- i - i</del>	0		<del> </del>	7.16
MWDIARSI		100	3.09	2.94	0.097	0.077	81		0.85	0.33	7 \$0		<del></del>	10			7.58
MWDJARS1		100	1.09	3.28	0.097	0.072	81	<u> </u>	0.85	0.36	7.811			20		<del></del>	7.38
MWDJARSI		100	3.119	2.97	0.097	0.066	RI.		0.85	().40	7 80		1 1	30			7.14
MWDJAR51		100	1 (19	2.42	0.097 1	0.054	31		0.85	0.29	7 80		1	40			7.06
MWDJAR51		100	3 09	2.23	0,097	0.049	3.1		0.85	0.45	7.80		1	50			7.00
MWDJARS1		100	3.09	2.55	0.097	0.051	81		0.85	0.30	7.80		1 ;	60			6.97
MWDJAR51 :		100	3.09	2 32	0 (197	0.044	81		0.85	0.36	7 (1)			70 1			677
MWDJARSI		I ION	3,09	4,5	0.097	() (141)	*1		0.85	0.31	7 %()			80			6.60
MWDJARS1 MWDJARS1		100	3.09	2,33	0.097	0.039	81	<u> </u>	0 85	0.38	7.80		1	90			6.43
MWDJARSI		1 100	3.09	1.94	0.097	0,040	81	<del>}</del>	0.85	0.62	7.80		<del></del>	110			6.35
MWDJARS		1(X)	3 04	1.74	0.097 1	0.038	18		0.85	035			1 1	120		· ·	6.23
MWDJARSI		100	3.09	191	0.097 (	0.035	*1	1	0.85	0.30			1	130		1	6.25
MWDJAR52		100	2.78	2.94		O OXU			0.78	0.77	7.72		1	U			7.91
MWDIARS2		100	2.73	2.88		0 (V-)			0.72	D-407	7.72						7.70
MWDJARS2 1		100	2 78	2,40	!	0.051		!	0.78	0,36	7.72			20			7.37
MWDJAR52	ļ	100	2.7x	2.09		0 (48	<u> </u>	<del>  </del>	0.7%	0.31	7.72	!	1 1	30			7,14
MWDIAR52		100	2.78	1.95		0.0140	<u>'                                    </u>	<del> </del>	0.78	0.33	7.72	!	- 1	50			7.11
MWDIARS:		100	2.78	1.75		0.031	<del></del> _	<b> </b>	0.78	0.32	7.72			60			6.25
MWDJAR52 I	<del></del>	100	2.78	1,64		0.028	<del></del>	<del>  </del>	0.78	0.37				70		<del></del>	6.84
MWDIAR52		I(X:	2.78	1,52	-	9 026			0.78	0.64	7.72			<b>\$</b> 0			6.71
MWDJAR52		100	2.78	149		0.025	1	-	0.78	0.50	7.72		1 1	<del>9</del> ()			6.65
MWDJAR52		100	2.78	1.47		0.025			0.7%	0.54	7.72		1	1001			6.58
MWDIAR52		IOX)	2.7%	1.43		0.024			0.7%	0.50	7.72		1	110			6.45
MWDJAR52		100	2.78	1,36		0.023			0.78	0.52	7.73		- !	120			6.34
MWDJAR52	<u></u>	100	2.78	1.29		0.023		<b> </b>	0.78	0.65	7.72		1	130		<del></del>	6,07
MWDIARS2 MWDIARS3	<del> </del>	100	2.78	1.34	0000	0.024	79	<del> </del>	0.7%	1,00	7.72 7.98			0			7,98
MWDIARS3		100	2.25	2.24	0.065	0,046	79		1.10	0.82	7.98			10		<del> </del>	7,58
MWDIARS3	<del> </del>	100	2.25	1.98	0.06	0.031	79		1.10	0.40	7.98			20			7.33
MWDIAR53		100	2.25	2.06	0.065	0.021	79		1.10	0.38	7.98		1	30			7.13
MWDJARS3		100	2.25	1,59	0.065	0.017	79		1 10	0.42	7.98		1	4(1			7.07
MWDIAR53		(K)	2.25	1.75	0.065 1	0.016	74		1.10	0.46	7 9\$		1	50			6.97
MWDIAR53		100	2.25	1.45	0.065	0.013	79		1.10	0.59	7.98			60		L	6.69
MWDJAR53		100	2.25	1.38	0.065	0.009	79		1.10	0.74	7.08		- 1	7() St)			6.61
MWDJAR53		100	2.25	1.29	0.065	8181.0	79		1.10	0.69	7.98		1	90)			6.54
MWDJAR53 MWDJAR53		100	2.25	1,21	0.065	0 (XI)7 0.00%	79 79	ļ	1.10	0.69	7.98			1(X)			6.33
MWDIARS)		100	1.25	1.19	0.065	O DING	79	<del>  </del>	1.10	\$5.90	7.98		<del></del>	110			6.29
MWDIARS4	<del> </del>	100	2.92	3.21	0.087	0.091	72		0.52	0.55	7.87		<del></del>	0		<del>  </del>	7.90
MWDIARS4		100	2.92	2.91	0.08"	0.070	72		0.52	0.70	7 X7		1	10			7.64
MWDJAR54	<del> </del>	100	2.92	2.33	0.08	0.051	72		0.52	0.59	7.87		1	20			7.54
MWDIAR54		100	2.92	2.55	0.087	0.043	72	L	U.52	0.52	7 87		1	30			7.35
MWDJAR54		100	2.92	2.05	0.087	0.039	72		0.52	9.47	7.87		1	40			7.15
		100	2.92	1.91	0.087	0.037	72		6.52	0.45	7,87		1	50			7.11
MWDIAR54		100	2.92	1.63	0.087	0.030	72		0.52	0.52	7.87			- 60			6.57
MWDIAR54 MWDIAR54																	
MWDIARS4 MWDIARS4 MWDIARS4		100	2.92	1.49	0,087	0.025	72	ļ	0.52	0.49	7 27			70 80			6.85
MWDIARS4 MWDIARS4 MWDIARS4 MWDIARS4		100	2.92 2.91	1.55	0.087	0.022	72		0.52	0.45	7.87		1	#n 90			6.72
MWDIARS4 MWDIARS4 MWDIARS4		100	2.92											<b>XI</b> )			

Page 9 of 10

Study ID		ter	TO	oc .	U	V-284	Alka	linery	T	.72.2	<del></del>						
	% CRW	% SPW	(m	g/L)		t/cm)	(mg/L as			oidny	P	н			ulation Cond	itions	
			Raw	Filt	Raw	FIRE	Raw			TU)		}	Coagulant	Dose	Acid	Base	Cost
			T	T				Filt.	Raw	Fift	Raw	Filt	ID		adjusted?	adjusted?	pН
		1					<del> </del> -			<u> </u>			(See above)		(Y/N)	(Y/N)	0
MWDJAR34		100	2.92	1.30	0.087	0.014	72			1	1	<u> </u>			biank=N	blank=N	V.
MWDJAR54		100	2.92	1.27	0.017	0.013	72		0.52	0.62	7.27		1	120	T		6.12
MWDJAR54		100	2.92	1.22	0.027	0.013			0.52	83.0	7.27		1	130			6.08
MWDJAR54		100	2.92	1.25	0.027	0.014	72		0.52	0.81	7,57		1	140			5.93
MWDJAR54		100	2.92	1.23	0.047	0.021			0.52	0.98	7.87		. 1	150	1		5.69
MWDJAR55		100	2.62	2.65	0.036	0.023	72		0.52	1.30	7,87		1	160			5.51
MWDJAR55		100	2.68	2.43	0.086	0.061	62		0.72	0.55	7,82		1	0	-		7.77
MWDJARSS		100	2.68	2.24	0.016	0.051	62		0.72	0.42	7,82		1	10			7.52
MWDJAR55		100	2.68	2.00	0.086	0.031	62		0.72	0.74	7,\$2		1	20	<del>                                     </del>		7.35
MWDJAR55		100	2.68	1.76	0.086	0.036	62		0,72	0,24	7.12		1	30			7.18
MWDJARSS		100	268	1.76	0.036		62		0.72	0.29	7.82		1	40			7.12
MWDJAR55		100	2.68	1.58	0.086	0.032	62		0.72	0.30	7.82		1	50			7.20
MWDJARSS		100	2.68	1.40	0.086	0.030	62		0.72	0.28	7.12		1	60			
MWDJARSS		100	2.68	1.45	0.036	0.029	62		0,72	0.24	7.82		1	70	<del></del>		7.08
MWDJAR55		100	2.62	1.40	0.036	0.027	62		0.72	0.25	7.22		1	80			
MWDJAR55		100	2.68	1.34	0.086	0.024	62		0.72	0.31	7.82		1	90			6.84
MWDJAR55		100	2.68	1.47	0.016	0.023	62		0.72	0.25	7.82		1	100			6.50
MWDJAR55		100	2.68	131	0.086	0.024	62		0.72	0.74	7,82		1	110			
MWDJARSS		100	2.68	1.34	0.046	0.024	62		0.72	0.44	7.82		1	120			6.45
MWDJAR55		100	2.68	1.33	0.086	0.021	62		0.72	0.63	7.82		1	130			6.20
WDJAR55		100	2.68	1.30		0.022	62		0.72	0.50	7.32		1	140			5.95
WDJARSS		100	2.68	1.32	0.086	0.022	62		0.72	0.72	7.82		1	150			5.83
			****	1.54	U.U#6	0.021	62		0.72	0.72	7.12			160			5.52

Page 10 of 10

#### ∞nv-F-S

Study ID			<b> </b>	Disir	fection	By-pro	iucts		Coagui	tion Condi	tion#		
	ered			TTI	НМ	HA	AA5	Coagulant	Dose	Acid	Base	Coag.	Coag.
	mmoni	bubation t	Residual	(µg	/L)	(μ	]/L)	٥		adjusted?	adjusted?	pН	temp.
	dose	(h)	1	R≥w	Filt	Raw	Filt	(see above)		(Y/N)	(Y/N)	0	(deg. C)
	g NH3-N	chlorine	(mg Cl2/L)								1		
MWDOP4					67.4	1	29.4	ı	20	Y		7.17	
MWDOP4					62.7		< 28.9	1	20	Y		7.11	
MWDOP4					54.9		< 22.3	1	20	Y		6,34	
MWDOP4					49.9		21.0	1	20	Y		6 40	
MWDOP4			1		53.1		20.9	1	20	Y		5.52	
MWDOP4					52.2		22.4	1	20	Y		5.71	
MWDOP4					62.1		23.8	1	30	Y		7.26	
MWDOP4					63.5		<b>Q4.7</b>	ı	30	Y	1	7.05	
MWDOP4					53.0		< 21.1	l	30	Y		6.26	
MWDOP4					53.8		<20.3	1	30	Y		6.50	
MWDOP4					48.1		<17.8	1	30	Y		6.23	
MWDOP4	T				46.7		<21.5	1	30	Y		5.43	
MWDOP4					56.4		24.9	1	40	Y		6.97	
MWDOP4	1				57.1		25.3	1	40	Y	1	7.24	
MWDOP4					52.4		< 21.5	ī	40	Y		6.30	
MWDOP4					43.9		<18.7	1	40	Y		6.19	
MWDOP4					45.9		< 18.0	i	40	Y		5.65	
MWDOP4					46.1		< 18.6	1	40	Y		5.74	
MWDOP4					43.6	i	<15.8	1	40	Y		5.42	
MWDOP5					22.2		11.7	ı	10	Y		5.88	
MWDOP5					22.0		147	i	20	Y		7.58	
MWDOPS	1				18.7		11.1	ī	20	Y		6.89	
MWDOP5					166		9.5	J	20	Y		6.50	
MWDOP5					174		9.2	• 1	20	Y		5.75	
MWDOPS	7				17.5		< 10.6	1	20	Y		5.31	
MWDOP5	1				18.7		9.8	1	40	Y	ii	6.90	
MWDOP5	7				16,3		9.2	1	40	Y		5.53	

010 0 010 0																																		
100	- 200	100	000	100	_ CI 0			121		-10	1	\$1			-	130		51.9																042140
	0100>	100	0100	100	0 27		ļ —	221	ļ	91	1-1	S C				121		151	181					+0			ET			980 0			276	0415/83
0.03	-1-26-	1-200-	500	110						- 51		09	1			151		09 /	00 L			13		10	-		<b> </b>				<b> </b>	I		040040
200	003	200	900	1 0	19 O		l	121		- 51	{	51				121		. 09 t_	7 60			£!_ _		0.5		-\		1			<b>!</b>			DEVECTED
003	100	500	900	010	97 0		1	221	<del> </del>		1	. <u></u> £				121	l	C8 T	09 (			<u> </u>		0.51			ļ	ļ	<u> </u>	ļ	_	II		04/08/83
100		500	800	#10	ZS 0	·	1	121	·	- 51	4 <del> </del>	0.0				121		D9 L	091	ļļ.		1-1-		10		-1	ļ	ļ		I	<del>}</del>	l		010993
200	700	Z0 0	900	110	0+0		<del> </del>		<del></del>	71	<del> </del>					_! []_	<del>  </del>	_ 1 ed_	00 1			£ !		0.3	-	-					·			0109033
200	200	200	90 D	010	470		1	171	<del> </del>	-21-	1	30				151		E 9 5	85 L			£		12 0 12 0			l	<del> </del>		{}	1	<del></del>		D40143
100	200	100	100	100	9C Q		1	121	1		1	SET				151		265	95 L			EI		10-	1-		1	1	<b> </b>	<del> </del>	1	<del>  </del>		CRITONO
100	000	100	50.0	900	60.0		_	155		21	1	51				121	l	119	251			- 1-		110	-		<del> </del>				<del> </del>	<del> </del>  -	<del></del>	C8/4040
Z0 0	7.00	100	100	90.0	100			133		1.5	1	اغذا				121	1	C1 9	05 Z			13		ii G	-	-			-		<del></del>	1		C6/1040
90 0	0.15	\$1 D	SZ Q	OC 0	51.0			123	1	91		05				153	II	90 9				· -			<del> </del>	-	-			-	<del> </del>	<del>  </del>		08/90/0
500	100	100	60.0	55.0	PS 0		1	123		Z.1	1	00				133		C6 5								<del> </del>	t	1	-	-	1	tt		0100032
160	601	00.1	951	111	102			155		0+		43.2				133	11	05 /	05 (				7	10	1—	-	Zi	1		860.0	<del> </del>	11	278	68/50/10
200	700	200	110	#10	1/0			15.5		9 (		0.8				135		OS L	051	-				110	7		12	-		960 8	1		MZ	£8/50/r0
100	OI O	110	100	27 E	101			121		οź		130				150		39 (	99 /			33			7-		1			1	1			0403/83
700	000	90.0	610	EE 0	E8 0			171		11		51				150		39 T	99 L			53									1			20/2010
005	200	200	90 0	#00	90 C			153		S i		Sh				150		99 2	99 L			53												0403/83
700	200	0.05	Z0 0	100	200			122		- 1		SC				130	ll	99 1	99 (			53												CB/CO+O
1 200				0.03	620			155	ļ	01		SI				150	ll	88 T	99 1			13	_				<b> </b>			L		1		0403/03
50.0	0 00	16.0	0.38	9C 0	00.0	·	ļ	155		- 1	1	05		[		021	— — ·	- 10 9 -	99 /				-		-		<b></b> -	<b> </b>	ļ		<b> </b>	<b> </b>		E8/10/40
100	100	500	800	010	50			221		- 51	<del>  </del>	12				150		66 S	89 1			35	}			-}	<del>                                     </del>			ll		<del>  </del> -		DEVIDAG
100	100	0100>	100	0.05	97.0		-	- 221	<del> </del> -	- 61	<del> </del>					150		66.5	99 /			55					1	ļ			<del> </del>	<del> </del>		D+10+0
0100>	200	100	100	0100>	110			221		-55	1	\$1 \$1				150		109	89 L			22					1	<del>  </del>	-	1	<del> </del>	<del>  </del> -		65/10/10
0.03	\$0 C	80.0	120	0.31	81.0		1	153		30		55				130		111	211			<del></del> -		10	-		1		-	560 D	1-	1	782	CONTRO
£0.0	600	100	50.0	120	950			123		- 51	1	55				021		21.1	211					10	+					8000	<del> </del>	-+	786	C6/91/6'0
0100>	0100>	0100>	010 D	0100>	031			6.51		01	11	20				130	- I	til	711					13 0	1-	1	1			8500		1 1	197	DESIACO
100	500	80.0	220	170	890			151		3.5	1	530				001		197	107			31		60	1		EL			1	1		OS E	01/51/83
0100>	0100>	CO 0	Jio	828	94.0			221		61	1	551				0.01		18 /	18 1			15		K 0	7-		EL	1				1	05 C	05/17/10
0100>	0100>	0100-	900	61.0	850			811		91		54				0.01		18 /	187			16		r£ 0			EL						05 C	01/51/83
000	000	£00	90.0	81.0	490			133		30	ш	061				546		25.1	Z6 L						1									103625
0.03	100	600	603	10.0	0.0		<b>!</b> -	155		21	11	281	1			565		26 2	26 2								1							10/26/92
000	900	100	97.0	90.0	270			15.5	ļ	11		120				5 8 1		79.1	185						1_	_					<b> </b>	II	I	10.56/85
010 00	0100	200	PI 0	82.0	210		<u> </u>		ļ	31		5 (2				8 61	I !	161	16 1								ļ	ļ			·l			10/20/92
0100>	9100-	0100	100	110	89 G			13	<del> </del> -			551				5 61	lI	16 7	161				_						L	<u> </u>	ļ			103035
010 D>	100	100	200	900	69 D Z+ O		l	521	<del> </del>		·}	130		1		661		161	151									<u> </u>	ļ			II		103085
0100	0100	0100=	910.0=	100	PE 0		ļ	E Z1	}	21		51				30.0	<u>  </u>	90 L	II								<del> </del>	ļ.—	<del> </del>	ļ		1		287 IAN
40 010	0100-	100	100	200	22.0		<del> </del>	121		61-	<del> </del>	02			[	9 OZ	<del>  </del>	90 /		<b> </b>							₩		<b>∤</b> —	<del> </del>	-	1		2871A11
100	100	200	200	100	0.35		<del> </del>	221	<del> </del>	11	<del> </del> +	05			<u> </u>	602	<del> </del>	60 Z	II						-}	-	├		├	1		<del>  </del>		78/01/01
20.0	200	200	200	500	620			155		<del>                                     </del>	1	12			<b> </b>	602	I	20.7	l								<del> </del>		<del> </del>		<del> </del>	<del>  </del>		101385
100	20 0	70.0	Z0 0	600	0 33			121	<del> </del>		+	51				0 1E	t	EOB	1									1	<del> </del>	<del> </del>	·			101745
200	200	20.0	200	0.03	PZ 0			121		11	-	51				912		6 02									+	<del> </del>		-		1		10/15/85
100	0100>	100	100	200	0.20			122		01	1-	SI				310		90 9										-	<del> </del>	<del> </del>	1	1		1013/85
20.0	200	200	to a	100	D 34			15.3		21		0.0				112		8 30	187			91		10.0	1		St	1	1	SOI 0	1		225	1006/92
100	0.05	ZØ 0	0.02	200	0.20			151		10		51				112		11.9	18 £			85		0.34			S#	1	1	201.0			331	100235
100	100	100	010	81.0	27.0			15.5		11		59				23.3		80.9	8 02			91							780 B					284200
500	000	100	100	60.0	150		ļ	153		SI		57			l	EEE		81 5	20.8			91						_	6100					08/34/85
000	50.0	900	000	50 0 50 0	00.0		<del> </del>	2 2 1 C 2 1	<b> </b>	21		ac.			L	23.3		02.8	200			91	_		_				Z/00					25/17/80
003	CO 0			100	15.0			133	├	11		0.0				1 62	II	8 0 3	208	<u> </u>		91		6.0	_		10	<b>_</b>	6/00	801.0	<b> </b>		3.33	28/22/60
200	200															202	E. 1													٠	<b>├</b> ──	1		28/22/80
- 66		600	D0 0						{		<del>{</del> {		•						<b> </b>									T .						28/22/00
	100	100	500	£0.0	92.0			151		E 1		09						134				<del></del>					-		1000	011.0		1		78/17/80
		600	000	P0 0	92 q 52 0			151		E 1		01	킈	_		202		96 L	96 (			91	_		7	=	厂	_	190 0			$\Box$		75/17/60
100	000 000	E0 0	800	£0.0	92.0			151 155 155		E 1 9 1 5 1		0 g 0 L				रदर रदर		7 36 7 96 7 56	96 £				=							0110				25/12/80
100	CO 0	100 100	20 0 0 0	20 0 20 0 20 0	96 q 52 0 96 0 04 0			151 155 155 151		E 1 91 51 21		01				202 202 203		96 L 96 L 96 L	96 L			91		×0					\$20 D	0110 9010				Z5/17/80 O9\1995
0 04 20 0	CO 0	100 100 100	\$0.0 \$0.0	20 0 Ex 6	96.4 52.0 96.0			151 155 155		E 1 9 1 5 1		0 g 0 L				2 CZ CZ CZ 9 SZ		96 L 29 G 19 G 10 B	96 £			91		x o					810 D	901 D 811 G				28/12/80 26/18/180 26/1/80
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	20 0 20 0 20 0 10 >	004 000 000 000 000 000 000 000	10 0 20 0 50 0 50 0 50 0	10 > 20 0 11 0 20 0 10 0	96 q 58 0 96 0 96 0 96 0			121 221 221 121 121		11 21 21 23		00 00 00 00 120				202 202 203		96 L 96 L 96 L	96 L			91		X O					\$40 0 \$40 0	0110 9010				Z5/17/80 O9\1995
000 000 000 000 000 000	20 0 20 0 20 0 10 > 10 >	000 000 000 000 000	10 0 10 0 10 0 10 0 10 0 10 0 10 0	10 0 20 0 11 0 20 0 20 0	90 9 50 90 90 90 90 90 90 90 90 90 90 90 90 90			1 21 2 21 2 21 1 21 2 21 2 21		51 21 22 61		0 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0				22 22 22 24 24		96 L 29 9 10 8 00 8	10 t 00 t 16 L			91 51 51		X O					920 0 920 0 590 0	0110 0 108 0 118 0 114				28/12/80 08/1983 08/10/85 08/10/85
005 005 005 005 001 001	000 000 000 000 100 100 900	000 000 000 000 000 10> 10>	100 100 100 100 100 100 100 100 100 100	200 200 200 200 200 200 200	959 032 040 040 040 040 040 040 040			121 224 225 121 221 221 221 221 221 221		\$1 91 51 21 22 61 91 61		00 00 00 120 01 01				101 101 101 101 101 101		1 3 2 2 2 3 2 4 2 4	96 £			9 i 5 i		X O					8200 9200 9800 \$800	0110 9010 9110 9110 E110				25/12/60 26/1/60 26/1/60 26/1/60
100 200 200 200 200 200 200 200	20 0 20 0 20 0 10 > 10 > 10 0 90 0	100 100 100 100 100 100 100 100	100 100 100 100 100 100 100 100 100	200 200 200 200 200 200 200 200 200 200	0.32 0.32 0.34 0.40 0.10 0.10 0.10			1 21 2 21 2 21 1 21 2 21 2 21 2 21 2 21		51 21 22 61 91 61 61		120 120 120 120 110 110 110 110				22 22 22 24 24 24 26 26 26 26 26 26 27 26 27 27 28 28 28 28 28 28 28 28 28 28 28 28 28		1 32 1 33 1 33 1 33 1 33 1 30 1 30 1 30 1 30	96 L 68 L 10 8 10 8			91 S1 S1 91 FZ S2 S1		X 0 X 0 IE 0 IE 0			19		8200 9200 1900 5900 1900	010 010 010 0110 0110 0110 0110		202	\$0 £	25/12/60 26/91/60 26/01/60 26/01/60 26/03/60 26/03/60 26/03/60 26/03/60
20 0 20 0 10 > 10 0 10 0 10 0 10 0	20 0 20 0 10 > 10 > 10 0 90 0 10 >	100 100 200 200 200 10> 10> 100 100	100 100 100 100 100 100 100 100	200 200 200 200 200 200 200 200 200	0 32 0 32 0 34 0 40 0 10 0 10 0 10 0 11 0 21 0 21			1 21 2 21 1 21 2 21 1 21 2 21 2 21 2 21		\$1 91 51 21 22 61 91 61		0 1 0 1 0 0 0 1 0 0 0 1 0 0 0 1 0 0 0 1 0 0 0 1 0 0 0 1 0 0 0 1 0 0 0 0 1 0				20 20 20 20 20 20 20 20		1 346 1 376	96 L 96 L 96 L 96 L			91 51 51 91 92		X 0 X 0 IE 0			15 19		8200 9200 1900 5900 1900	0110 8010 8110 7110 5110 7110		282	90 C	08\5\125 08\1905 08\1903 08\10\25 08\10\25 08\0\0\25 08\0\0\25 08\0\0\25 08\0\0\0\25 08\0\0\0\0\0\0\0\0\0\0\0\0\0\0\0\0\0\0\
004 005 005 001 001 004 004 001 CF 38	60 20 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	001 004 004 003 003 001 (01 001 004 004 004	001 001 001 002 003 003 003 003 003	000 000 000 000 000 000 000 000 000 00	0 32 0 32 0 34 0 40 0 33 0 33 0 33 0 33 0 43 0 43			15 / 15 / 15 / 15 / 15 / 15 / 15 / 15 /		1 1 2 2 2 4 1 2 2 2 4 1 2 2 2 4 1 2 2 2 4 1 2 2 2 4 1 2 2 2 4 1 2 2 2 2		120 120 120 120 110 110 110 110				22 22 22 24 24 24 26 26 26 26 26 26 27 26 27 27 28 28 28 28 28 28 28 28 28 28 28 28 28		1 32 1 33 1 33 1 33 1 33 1 30 1 30 1 30 1 30	96 L 68 L 10 8 10 8			91 S1 S1 91 FZ S2 S1		X 0 X 0 IE 0 IE 0					8200 9200 1900 5900 1900	010 010 010 0110 0110 0110 0110		Z# C		25/12/60 26/91/60 26/01/60 26/01/60 26/03/60 26/03/60 26/03/60 26/03/60
0 005 0 005 0 005 0 001 0 001 0 001 0 001 0 001 0 001 0 001 0 001 0 001	(2) 100 (100 (100 (100 (100 (100 (100 (100	001 004 000 000 000 001 001 001 001 001	At 000 000 000 00	0.32 0.32 0.33 0.34 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35	() Sep)	6	15 (15 ) 15 (15 ) 15 (15 ) 15 (15 ) 15 (15 ) 15 (15 ) 15 (15 ) 15 (15 ) 15 (15 ) 15 (15 ) 15 (15 ) 15 (15 ) 15 (15 ) 15 (15 ) 16 (16 ) 17 (16 ) 18	-(1864)	1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2		0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0				202 202 203 204 204 202 203 203 204 204 204 204 204 204 204 204 204 204		96 L 96 L 98 L 99 L 99 L 99 L 99 L 99 L 99 L 99 L	70 8 98 7 98 7 19 7 10 8			91 51 51 91 FZ 52 51		X 0 X 0 E 0 E 0 E 0 E 0			19		820 D 820 D 820 O 190 O 590 O 590 O 190 O 190 O 190 O	0110 9010 9110 9110 9110 9110 9110			90 C	25/12/60 26/91/60 26/01/60 26/01/60 26/03/60 26/03/60 26/03/60 26/03/60	
005 005 005 401 401 601 001 001 CF 38 (LLAY)	005 005 005 005 001 001 002 001 002 001 001	(1/4m²) (1/4m²) (10 > (10 ) (10 > (1	At Act Act Act Act Act Act Act Act Act A	6m943 6m943 10.2 10.2 10.2 10.2 10.3	9.38 0 32 0 32 0 40 0 40 0 10 0 11 0 43 0 43 0 43 0 43 0 43 0 43 0 44 0 44	threat	Hel	13 ( 15 5 15 5 15 5 15 5 15 7 15 1 15 1 15 1	Saubia 91	1 2 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2		0 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	well		mot0	22 22 22 24 24 24 26 26 26 26 26 26 27 26 27 27 28 28 28 28 28 28 28 28 28 28 28 28 28		7 266 7 200 8 01 8 02 8 02 8 03 8 04 7 266 7 266 8 04 8 05 8 05 8 05 8 05 8 05 8 05 8 05 8 05	96 £ 10 8 10 8 10 8			91 51 51 91 FZ 52 51	in the second	X 0 X 0 X 0 X 0 X 0 X 0 X 0 X 0 X 0 X 0	181	Dren	MEM .		010h. 010h. 010h. 010h. 010h. 010h. 010h. 010h. 010h. 010h.	010 010 010 0110 0110 0110 0110		mosto		25/12/60 26/91/60 26/01/60 26/01/60 26/03/60 26/03/60 26/03/60 26/03/60
0 005 0 005 0 005 0 001 0 001 0 001 0 001 0 001 0 001 0 001 0 001 0 001	(2) 100 (100 (100 (100 (100 (100 (100 (100	(1/4m²) (1/4m²) (10 > (10 ) (10 > (1	At Act Act Act Act Act Act Act Act Act A	600 600 600 600 600 600 600 600	0.32 0.32 0.34 0.40 0.35 0.45 0.35 0.45 0.45 0.45 0.45 0.45 0.45 0.45 0.4	Ozene.		15 (15 ) 15 (15 ) 15 (15 ) 15 (15 ) 15 (15 ) 15 (15 ) 15 (15 ) 15 (15 ) 15 (15 ) 15 (15 ) 15 (15 ) 15 (15 ) 15 (15 ) 15 (15 ) 16 (16 ) 17 (16 ) 18		1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	ж	0 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		1	(deg C)	MAJE WAS THE TANK THE	Ma	7 200 L 200	70 8 98 7 98 7 19 7 10 8		wezo frued	91 51 51 91 FZ 52 51	Ma (6	XO XO XO XO XO XO XO XO XO XO	18 EW.	2242 98 J	WEN TO	'Ma	10010 10010 10010 1001 1001 1001 1001	0 110 0 108 0 108 0 113 0 113 0 113 0 113 0 118 0 118		(Ngm) nost0	90 C	Z8/12/80 Z6/91/80 Z6/01/80 Z6/01/80 Z6/01/80 Z6/90/80 Z6/90/80 Z6/90/80 Z6/90/80
005 005 005 401 401 601 001 001 001 CF 38 Ludy]	005 005 005 005 001 001 002 001 002 001 001	(1/4m²) (1/4m²) (10 > (10 ) (10 > (1	At Act Act Act Act Act Act Act Act Act A	600 600 600 600 600 600 600 600	9.38 0 32 0 32 0 40 0 40 0 10 0 11 0 43 0 43 0 43 0 43 0 43 0 43 0 44 0 44	Ozene.	Hel	13 ( 15 5 15 5 15 5 15 5 15 7 15 1 15 1 15 1	Saubia 91	1 2 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	ж	0 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		1	(2 gab) nostO	MAJE WAS THE TANK THE	78(3)	7 266 7 200 8 01 8 02 8 02 8 03 8 04 7 266 7 266 8 04 8 05 8 05 8 05 8 05 8 05 8 05 8 05 8 05	70 8 98 7 98 7 19 7 10 8			91 51 51 91 FZ 52 51	Ma (6	X 0 X 0 X 0 X 0 X 0 X 0 X 0 X 0 X 0 X 0	W1	Kikishih Las Caco Ozen. Ozen.	WEN TO	181.5	010h. 010h. 010h. 010h. 010h. 010h. 010h. 010h. 010h. 010h.	0 110 0 108 0 108 0 113 0 113 0 113 0 113 0 118 0 118		mosto	90 C	25/12/60 26/91/60 26/01/60 26/01/60 26/03/60 26/03/60 26/03/60 26/03/60
005 005 005 401 401 601 001 001 001 CF 38 Ludy]	005 005 005 005 001 001 002 001 002 001 001	(1/4m²) (1/4m²) (10 > (10 ) (10 > (1	At Act Act Act Act Act Act Act Act Act A	600 600 600 600 600 600 600 600	0.32 0.32 0.34 0.40 0.35 0.45 0.35 0.45 0.45 0.45 0.45 0.45 0.45 0.45 0.4	Ozene.	Hel	(204) 121 (204) 122 (204) 123 (204)	anex0 laubia at	1 6 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	THE STATE OF THE S	0 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		1	(deg C)	MAJE WAS THE TANK THE	THE STATE OF THE S	7 200 L 200	70 8 98 7 98 7 19 7 10 8		westo funkt	91 51 51 91 FZ 52 51	Ma (6	XO XO XO XO XO XO XO XO XO XO	**************************************	2242 98 J	WEN TO	1992	MS.VU (most) most) 880 0 180 0 280 0 280 0 180 0 850 0	0110 8010 9110 1110 9110 9110 9110	FINE	TOC (Agm)	MEN.	28/1/280 26/1/200 26/1/2
005 005 005 401 401 601 001 001 001 CF 38 Ludy]	005 005 005 005 001 001 002 001 002 001 001	(1/4m²) (1/4m²) (10 > (10 ) (10 > (1	At Act Act Act Act Act Act Act Act Act A	600 600 600 600 600 600 600 600	0.32 0.32 0.34 0.40 0.35 0.45 0.35 0.45 0.45 0.45 0.45 0.45 0.45 0.45 0.4	Ozene.	Hel	(204) 121 (204) 122 (204) 123 (204)	Saubia 91	1 6 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	THE STATE OF THE S	0 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		1	(deg C)	MAJE WAS THE TANK THE	781.3	7 200 L 200	70 8 98 7 98 7 19 7 10 8		westo funkt	91 51 51 91 FZ 52 51	The state of the s	0 20 0 20 0 20 0 20 0 20 0 20 0 20 0 2	- le	Alkallerity Coco es Coco	Meral West	Tel d	MS.VU (most) most) 880 0 180 0 280 0 280 0 180 0 850 0	0110 8010 9110 1110 9110 9110 9110	FINE	TOC (Agm)	MA.	Z8/12/80 Z6/91/80 Z6/01/80 Z6/01/80 Z6/01/80 Z6/90/80 Z6/90/80 Z6/90/80 Z6/90/80
005 005 005 401 401 601 001 001 001 CF 38 Ludy]	005 005 005 005 001 001 002 001 002 001 001	(1/4m²) (1/4m²) (10 > (10 ) (10 > (1	At Act Act Act Act Act Act Act Act Act A	600 600 600 600 600 600 600 600	0.32 0.32 0.34 0.40 0.35 0.45 0.35 0.45 0.45 0.45 0.45 0.45 0.45 0.45 0.4	Ozene.	Hel	(204) 121 (204) 122 (204) 123 (204)	anex0 laubia at	1 6 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	THE STATE OF THE S	0 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		1	(deg C)	MAJE WAS THE TANK THE	THE STATE OF THE S	7 200 L 200	70 8 98 7 98 7 19 7 10 8		westo funkt	91 51 51 91 FZ 52 51	The state of the s	0 X 0	izlanitali (E	or after see Altealinity Coco as L	Meig Abus		#15.VU #17.VU #10.10 #10.00 #10.00 #10.00 #10.00 #10.00 #10.00 #10.00	MEN SHOOL	PRE-	SATAG Y SOT Dem Jeen	TILIAUC west	### Garden  ### Ga
005 005 005 401 401 601 001 001 001 CF 38 Ludy]	005 005 005 005 001 001 002 001 002 001 001	(1/4m²) (1/4m²) (10 > (10 ) (10 > (1	At Act Act Act Act Act Act Act Act Act A	600 600 600 600 600 600 600 600	0.32 0.32 0.34 0.40 0.35 0.45 0.35 0.45 0.45 0.45 0.45 0.45 0.45 0.45 0.4	Ozene.	Hel	(204) 121 (204) 122 (204) 123 (204)	anex0 laubia at	1 6 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	THE STATE OF THE S	0 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		1	(deg C)	MAJE WAS THE TANK THE	TM2	7 200 L 200	70 8 98 7 98 7 19 7 10 8		westo funkt	91 51 51 91 FZ 52 51	The state of the s	0 X 0	izlanitali (E	or after see Altealinity Coco as L	Meig Abus		#15.VU #17.VU #10.10 #10.00 #10.00 #10.00 #10.00 #10.00 #10.00 #10.00	MEN SHOOL	PRE-	SATAG Y SOT Dem Jeen	TILIAUC west	28/1/280 26/1/200 26/1/2
005 005 005 401 401 601 001 001 001 CF 38 Ludy]	005 005 005 005 001 001 002 001 002 001 001	(1/4m²) (1/4m²) (10 > (10 ) (10 > (1	At Act Act Act Act Act Act Act Act Act A	600 600 600 600 600 600 600 600	0.32 0.32 0.34 0.40 0.35 0.45 0.35 0.45 0.45 0.45 0.45 0.45 0.45 0.45 0.4	Ozene.	Hel	(204) 121 (204) 122 (204) 123 (204)	anex0 laubia at	1 6 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	THE STATE OF THE S	0 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		1	(deg C)	MAJE WAS THE TANK THE	TM2	7 200 L 200	70 8 98 7 98 7 19 7 10 8		westo funkt	91 51 51 91 FZ 52 51	The state of the s	0 X 0	izlanitali (E	i after sedit to after se se after sed the all of a Doc Doc as L	ACT NOTES		2 moord s 2 moord s	OLIO OLIO OLIO OLIO OLIO OLIO OLIO MEN MEN MEN MEN MEN MEN MEN MEN MEN MEN	PAE-C	SATAG Y SOT Dem Jeen	TILIAUC west	### Garden  ### Ga
005 005 005 401 401 601 001 001 001 CF 38 Ludy]	005 005 005 005 001 001 002 001 002 001 001	(1/4m²) (1/4m²) (10 > (10 ) (10 > (1	At Act Act Act Act Act Act Act Act Act A	600 600 600 600 600 600 600 600	0.32 0.32 0.34 0.40 0.35 0.45 0.35 0.45 0.45 0.45 0.45 0.45 0.45 0.45 0.4	Ozene.	Hel	(204) 121 (204) 122 (204) 123 (204)	anex0 laubia at	1 6 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	THE STATE OF THE S	0 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		1	(deg C)	MAJE WAS THE TANK THE		7 200 L 200	70 8 98 7 98 7 19 7 10 8		westo funkt	9 1 5 1 5 1 9 1 7 2 7 3 8 1 8 1 8 1	Total Table	0 X 0	izloven france	f affer seed or affer see Alkalimity	helselles belselles veril		## ## ## ## ## ## ## ## ## ## ## ## ##	0110 0100 0100 0100 01112 0112 0112 011	PAE-C	SATAG Y	TILIAUC	PARTIES O HERCARD AND A HERCARD AND A HERCARD
005 005 005 401 401 601 001 001 001 CF 38 Ludy]	005 005 005 005 001 001 002 001 002 001 001	(1/4m²) (1/4m²) (10 > (10 ) (10 > (1	At Act Act Act Act Act Act Act Act Act A	600 600 600 600 600 600 600 600	0.32 0.32 0.34 0.40 0.35 0.45 0.35 0.45 0.45 0.45 0.45 0.45 0.45 0.45 0.4	Ozene.	Hel	(204) 121 (204) 122 (204) 123 (204)	anex0 laubia at	1 6 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	THE STATE OF THE S	0 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		1	(deg C)	MAJE WAS THE TANK THE	Ma .	7 200 L 200	70 8 98 7 98 7 19 7 10 8		westo funkt	9 1 5 1 5 1 9 1 7 2 7 3 8 1 8 1 8 1	inon, and in in in in in in in in in in in in in	0 X 0 X 0 0 2 0 0 2 0 0 2 0 2 0 2 0 2 0 2 0 2 0	itelessooi Malekeen Isloomel	inolisings  in after seeks in a sea seas seas seas seas seas seas se	notheralds potables well well		## ## ## ## ## ## ## ## ## ## ## ## ##	May May Sept of the sept of th	X se pope se .	ATAG Y	TUAUC	MATTER OFFISSE OFFI
004 005 005 001 001 001 001 CF 38 (udy)	005 005 005 005 001 001 002 001 002 001 001	(1/4m²) (1/4m²) (10 > (10 ) (10 > (1	At Act Act Act Act Act Act Act Act Act A	600 600 600 600 600 600 600 600	0.32 0.32 0.34 0.40 0.35 0.45 0.35 0.45 0.45 0.45 0.45 0.45 0.45 0.45 0.4	Ozene.	Hel	(204) 121 (204) 122 (204) 123 (204)	anex0 laubia at	1 6 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	THE STATE OF THE S	0 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		1	(deg C)	MAJE WAS THE TANK THE	7M2	7 200 L 200	70 8 98 7 98 7 19 7 10 8		westo funkt	9 1 5 1 5 1 9 1 7 2 7 3 8 1 8 1 8 1	inon, and in in in in in in in in in in in in in	0 X 0	itelessooi Malekeen Isloomel	inolisings  in after seeks in a sea seas seas seas seas seas seas se	notheralds potables well well		## ## ## ## ## ## ## ## ## ## ## ## ##	0110 0100 0100 0100 01112 0112 0112 011	X se pope se .	ATAG Y	TUAUC	PARTIES O HERCARD AND A HERCARD AND A HERCARD
004 005 005 001 001 001 001 CF 38 (udy)	005 005 005 005 001 001 002 001 002 001 001	(1/4m²) (1/4m²) (10 > (10 ) (10 > (1	At Act Act Act Act Act Act Act Act Act A	600 600 600 600 600 600 600 600	0.32 0.32 0.34 0.40 0.35 0.45 0.35 0.45 0.45 0.45 0.45 0.45 0.45 0.45 0.4	Ozene.	Hel	(204) 121 (204) 122 (204) 123 (204)	anex0 laubia at	1 6 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	THE STATE OF THE S	0 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		1	(deg C)	MAJE WAS THE TANK THE	Tales	7 200 L 200	70 8 98 7 98 7 19 7 10 8		westo funkt	9 1 5 1 5 1 9 1 7 2 7 3 8 1 8 1 8 1	Jecred Je	0 X 0 X 0 X 0 X 0 X 0 X 0 X 0 X 0 X 0 X	ile. rei	ufe sheet, included, inclu	à side et cos velle mode side polsedos velle velle 18	soptim	### ##################################	MENUTE COME	EW Steel	ATAG Y	(X ne de le INE  GROOMS  GR	
004 005 005 001 001 001 001 CF 38 (udy)	005 005 005 005 001 001 002 001 002 001 001	(1/4m²) (1/4m²) (10 > (10 ) (10 > (1	At Act Act Act Act Act Act Act Act Act A	600 600 600 600 600 600 600 600	0.32 0.32 0.34 0.40 0.35 0.45 0.35 0.45 0.45 0.45 0.45 0.45 0.45 0.45 0.4	Ozene.	Hel	(204) 121 (204) 122 (204) 123 (204)	anex0 laubia at	1 6 1 1 6 1 6 1 6 1 6 1 6 1 6 1 6 1 6 1	THE STATE OF THE S	0 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		1	(deg C)	MAJE WAS THE TANK THE	Ma .	7 200 L 200	70 8 98 7 98 7 19 7 10 8		westo funkt	9 1 5 1 5 1 9 1 7 2 7 3 8 1 8 1 8 1	Jecred Je	0 X 0 X 0 0 2 0 0 2 0 0 2 0 2 0 2 0 2 0 2 0 2 0	ile. rei	ufe sheet, included, inclu	à side et cos velle mode side polsedos velle velle 18	soptim	### ##################################	May May Series and Ser	EW Steel	ATAG Y	(X ne de le OFFISSE OFFI	
004 005 005 001 001 001 001 CF 38 (udy)	005 005 005 005 001 001 002 001 002 001 001	(1/4m²) (1/4m²) (10 > (10 ) (10 > (1	At Act Act Act Act Act Act Act Act Act A	600 600 600 600 600 600 600 600	0.32 0.32 0.34 0.40 0.35 0.45 0.35 0.45 0.45 0.45 0.45 0.45 0.45 0.45 0.4	Ozene.	Hel	(204) 121 (204) 122 (204) 123 (204)	anex0 laubia at	1 6 1 1 6 1 6 1 6 1 6 1 6 1 6 1 6 1 6 1	THE STATE OF THE S	0 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		1	(deg C)		362	Hd	Mark 10 8 10 8 10 8 10 8 10 8 10 8 10 8		westo funkt	9 1 5 1 5 1 9 1 7 2 7 3 8 1 8 1 8 1	Jecred Je	0 X 0 X 0 X 0 X 0 X 0 X 0 X 0 X 0 X 0 X	Ci waler.	Sinis Proje algoritation, i after seed in after see to a refer see to a refer see	is side in cos redicable motivation company to	soptim	#200 0   190 0   580 0   580 0   580 0   190 0	Sending State of the state of t	EW Steel	ATAG Y	ica ioni (X. no dit X. no dit TLIAUS	and control and co
005 005 005 401 401 601 001 001 001 CF 38 Ludy]	005 005 005 005 001 001 002 001 002 001 001	(1/4m²) (1/4m²) (10 > (10 ) (10 > (1	At Act Act Act Act Act Act Act Act Act A	600 600 600 600 600 600 600 600	0.32 0.32 0.34 0.40 0.35 0.45 0.35 0.45 0.45 0.45 0.45 0.45 0.45 0.45 0.4	Ozene.	Hel	(204) 121 (204) 122 (204) 123 (204)	anex0 laubia at	1 6 1 1 6 1 6 1 6 1 6 1 6 1 6 1 6 1 6 1	THE STATE OF THE S	0 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		1	(deg C)	MAJE WAS THE TANK THE		1 224 1 22 1 22 1 22 1 28	96 / 10 8 00 8 16 / 66 / 68 / 20 8 20 8 20 8		wezo frued	9 1 5 1 5 1 9 1 7 2 7 3 8 1 8 1 8 1	Jecred Je	0 X 0 X 0 X 0 X 0 X 0 X 0 X 0 X 0 X 0 X	Ci waler.	ufe sheet, included, inclu	is side in cos redicable motivation company to	soptim	### ##################################	Sending State of the state of t	EW Steel	ATAG Y	ica ioni (X. no dit X. no dit TLIAUS	UNICLES  LONG LINE  GROOMS  GR
005 005 005 401 401 601 001 001 001 CF 38 Ludy]	005 005 005 005 001 001 002 001 002 001 001	(1/4m²) (1/4m²) (10 > (10 ) (10 > (1	At Act Act Act Act Act Act Act Act Act A	600 600 600 600 600 600 600 600	0.32 0.32 0.34 0.40 0.35 0.45 0.35 0.45 0.45 0.45 0.45 0.45 0.45 0.45 0.4	Ozene.	Hel	(204) 121 (204) 122 (204) 123 (204)	anex0 laubia at	1 6 1 1 6 1 6 1 6 1 6 1 6 1 6 1 6 1 6 1	THE STATE OF THE S	0 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		1	(deg C)			1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	10 8 00 8 10 10 8 00 8 16 4 00 8 16 4 10 8 10 8 10 8 10 8 10 8 10 8 10 8 10	1325005	wezo frued	9 1 5 1 5 1 9 1 7 2 7 3 8 1 8 1 8 1	Jecred Je	O X O O X O O X O O X O O X O O X O O X O O O X O O O X O	ci water, sell interestati int	(Fibrat, Intro State Propie ate streed, interpretation, interp	b side of cos refe mode side postación (	alwy to	Pav/R	MENUAL SEPTIMENT OF THE PROPERTY OF THE PROPER	California (Califo	ATAG Y	:Of sole :Of sole (X no alth- X' no alth- TLLAUC	mercana a decrea of the course
005 005 005 401 401 601 001 001 001 CF 38 Ludy]	005 005 005 005 001 001 002 001 002 001 001	(1/4m²) (1/4m²) (10 > (10 ) (10 > (1	At Act Act Act Act Act Act Act Act Act A	600 600 600 600 600 600 600 600	0.32 0.32 0.34 0.40 0.35 0.45 0.35 0.45 0.45 0.45 0.45 0.45 0.45 0.45 0.4	Ozene.	Hel	(204) 121 (204) 122 (204) 123 (204)	anex0 laubia at	1 6 1 1 6 1 6 1 6 1 6 1 6 1 6 1 6 1 6 1	THE STATE OF THE S	0 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		1	(deg C)			1 224 1 22 1 22 1 22 1 28	10 8 00 8 10 10 8 00 8 16 4 00 8 16 4 10 8 10 8 10 8 10 8 10 8 10 8 10 8 10	1325005	wezo frued	9 1 5 1 5 1 9 1 7 2 7 3 8 1 8 1 8 1	Jecred Je	O X O O X O O X O O X O O X O O X O O X O O O X O O O X O	ci water, sell interestati int	Sinis Proje algoritation, i after seed in after see to a refer see to a refer see	b side of cos refe mode side postación (	alwy to	Pav/R	Sending State of the state of t	California (Califo	ATAG Y	:Of sole :Of sole (X no alth- X' no alth- TLLAUC	and control and co
004 005 005 001 001 001 001 CF 38 (udy)	005 005 005 005 001 001 002 001 002 001 001	(1/4m²) (1/4m²) (10 > (10 ) (10 > (1	At Act Act Act Act Act Act Act Act Act A	600 600 600 600 600 600 600 600	0.32 0.32 0.34 0.40 0.35 0.45 0.35 0.45 0.45 0.45 0.45 0.45 0.45 0.45 0.4	Ozene.	Hel	(204) 121 (204) 122 (204) 123 (204)	anex0 laubia at	1 6 1 1 6 1 6 1 6 1 6 1 6 1 6 1 6 1 6 1	THE STATE OF THE S	0 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		1	(deg C)			1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	10 8 00 8 10 10 8 00 8 16 4 00 8 16 4 10 8 10 8 10 8 10 8 10 8 10 8 10 8 10	1325005	wezo frued	9 1 5 1 5 1 9 1 7 2 7 3 8 1 8 1 8 1	(5) Makeched allow, and allow, and allow.	O X O O X O O X O O X O O X O O X O O X O O O X O O O X O	ri Skiady cd water, Elle, rei beccutati interiolati	Opinvit silts  (River, lance site shoet, signification in signification, signific	b shift of house of house of house of house shift of house shift of house o	alwy to	Pav/R	OF 100 CO	California (Califo	ATAG Y	:Of sole :Of sole (X no alth- X' no alth- TLLAUC	mercana a decrea of the course

110294	10.4	110194	MICA!	10/201	HANZA!	10/2/104	10/27/84	1075594	HENEZOI	1026/94	10/26/94	10/26/91	10/25/01	102494	08/29/94	04/194	26/1/94	20170		MC2//0	0// 10/0	CK-07/10	04/2/00	20,700	1	200	1830/10	07/06/93	16/4/20	CEVEZNO	200720	25.50	25175	06/17/93	C6/1/90	08/1/80	C641/80	871783	08/13/83	05/13/93	86138	051383	05/12/93	05/12/93	05/15/83	05/12/93	05/12/93	COMOUSE	DEVERON	050393	CENTRA	D\$40343	0473483	04799	CEMEZ 2-0	04/26/93	Cerecyo	Caractro	2000	2017/00	042753	04/26/83	04/26/90	CHZZWO	C8/27/80	C6/22/90	DW72993	CACCAGO				2200					
		ΙŤ	302(4)	1		Ī	T	Ī			Ī			310	151	352	1	T	1	9			Ī		Ī	Ī		1		38	š	3	322	32		33	Г	Γ						Γ	Γ				3 5	318	318	318				1	T		T	Ī	Ī	307	307	Г			1	Ī	Ī	T	Ī	Ī	T	1	Row	Ī	1
HH			ŋ 2 76 (d)	$\dagger$	H	+	$\dagger$	-						317	362	352	+	+	1			+	t	t	$\dagger$	1		7	378	1	-1	33	1	1	-	ž		-	t			r	T	T							Н	_		1	+	†	+	t	1	t	t	T		-		1	1	1	1	t	t	†	†	†	Ozen	1	륁
HH	+		(4) 217(4)	+	H	+	H	-	H	L		_		(4) 274	(d) 2 80 (d)	287	1	+	12	3 2 2 2		-	+	1	+	+	+	1	-	1	-	٦	1	-	1	_	H	ŀ	H		1	t		ŀ	l		L							<del> </del>	†	+	$\dagger$	†	$\dagger$	1	+	1	T	H		1	1	+	†	+	†	t	†	7	Ę		
HH	+		0 0003	$\dagger$	Н	+	H	$\vdash$						900	0 003	3	1	1	7	9 9			1	t	1		0	•	1	1	-	1	1		-		-	1	t	1	-	t	t	T	-			-	0 10	9108	0 10	0.10	1	1	1	+	1	+	†	t	t	010	9 100	-		1	1	+	1	t	t	†	†	÷	Raw	1	1
HH	+		0048	+	H	+	ŀ	$\vdash$	H	L	-	Ц			0054		+	+	1				ł	+		000	1	=	1	1	-	+	1	1	-		_	-	t	-	t	t	t	H	-		-		•			*		+	+	+	+	+	+	t	t	f		-		1	+	+	+	†	$\dagger$	†	1		CZON.	1	Ş
$\parallel \parallel \parallel$	+		0036	+	Н	$^{+}$	+	H		L	-	H			98 0042		1	+	+				$\dagger$	$\dagger$	- 1		+	4	1	1	_		-		_		r	-	t	t	t	t	t	t	H		-	-	-	H			Ц	1	1	+	+	+	$\dagger$	t	t	t	t	-			1	1	1	1	†	†	+		786		
HH	+	$\vdash$	2	+	Н	+	$\dagger$	H		-	-			77	П	₹	+	+	1	7	8	Т	+	+	1	2	2	2	=	=	£	7.	8	8	12	2	82	T	t	l	t	t	t	t	+	+	H	-	11	n	n	π	-	1	+	+	1	†	+	†	t	3	a	l			1	+	†	†	t	†	1	!	)		-
HH	$\dagger$	$\parallel$		$\parallel$	H	†	t	İ			H						1	t	+	†	t	t	$\dagger$	†	†	1	1	1	1	1	_			-		_	r	T	t	İ	t	t	T	T	T	r	r	İ			r		-		1	1	1	1	†	t	Ì	İ	T	İ			1	T	†	†	†	†	†	1	Raw Ozen.	4. s. c	À
$\parallel \parallel \parallel$	+			$\dagger$	Н	+	t	╁		-	-					1	1	+	1	$\dagger$	t	†	t	t	†	t	┪	1	1	1	_	1				_	l		t	t	t	t	r	t	T	-		-		-					1	1	1	†	+	†	t		1	T			1	†	1	1	1	†	†		7		7
HH	+	H		+	Н	+	t	F			-	-	L		L	+	1	+	1	+	t	1	$^{+}$	†	+	1	-		1	-	-	-	-	-	_	-	r	l	t	t	+	t	t	l	t	$\vdash$	H	-		-	H			+	1	1	+	+	$\dagger$	†	t	$\dagger$	t	H	-		1	†	1	1	+	†	+	_	N. See	ч	-
0 0 0	00	00	0 0	+	Н	+	+	t		-	H	H	_	0.26	0	1	+	+	1		+		2	1		-	2	2	2			2	•		05	05	100						100		93	2	9	0	0.5	2	0.5	0.5	0.5	0	2	2	•	8		+	†	5		+	-		1	+	1	1	+	+	1		CION		7
2 2 3	8 =	8 8	8 %	+	H	+	H			_	_			*	n		+	+	-   '	2 2	3 2	1	3 5	SI	3	5	*	=	٦	8	x	ž	=		22	8	_	1	1			1		1	-	ā	-	-	7	E	-	8		a	34	24	<u> </u>	8	-	-	+	-	-	-	L	Ц	$\frac{1}{1}$	1	+	+	+	+	1		¥ .		Ì
$\parallel \parallel \parallel$	$\perp$	-	$\parallel$	4	$\sqcup$	+	+	ŀ	L		L				Ц	-	1	1	1	+	1	1	+	+	+	1	-	_	4	4			-			_	-	L	+	L	1	1	1	ļ	L	-		L		<u> </u>	-	L	μ		4	-	-	4	+	1	+	1	+	1	L			4	-	1	1	+	4	4	Н	Н	_
	$\perp$	$\parallel$	22.0	Ц	Ц	1	1	L		L	L	L	L	074	3	•	4		2		-   2	Ā	1	1	1	1	4	_									L	L	-	1	1	-	-	ļ	-			L		L		L	L	Ц	4		1	1	1	1	1	1	1	L		Ц	4	1	1	1	1	1	-	_	Tare C	1 1	į,
Ш		Ш	Ш	Ц		1	1				L						1	1	-	1	1	1	1	1	-	1											L	L	1	1	-	1	1	L	-			-		L	L					1	1	_	1		1	1	1	-		Ц		1	1	-	1	4			Dzeet.	Š	Thicky
								L														1														L				L					L		L	L										]						L				4			1	1		4	Ē	-	_
8	Z	ZZ	2 9					ř	70	7	8	ž	7	23	85	ŝ	3	3	6	- 5		:				8	2	7 93	ž	27	787	ž	7	ž	778	778	7	8	S	18	8	8				L			8	8	8	8	2	#	4					1															Raw	H	
8 6 8 3	288	7 8 8 7	2 7 83 28 7 83	5 597	2	5 8	8	792	791	2	8	708	78	7 92	15.0	715	715	6	ž.							7 93	ž	793	퀽	787	787	3	7	78	7.78	7 78	7	8	i s	8	8	8			8	8	6 07	8	8	8	8	8	9 27	9 37	-	=	580	2	8		5	i	13	8	730	7.30	78	ช	2	2	2	=		.	Ozon,	٥	ł
			767	1	П		Ì	T					1	ľ	1	712	- 1	ì	ï		1	ŀ	Ì	1	1	ĺ											Ī		Ì	Ì	1		T	Í	İ	T		Ī		Ī						Ì	1		Ì	Ī	Ť	Ť	Ť	Ī				1	1	1	Ì	1			Ŧ		
		= =		+		= =	-	=	_	ī	=	=		-	Н	+	Т	т	7	7	7	7	<u> </u>	<u>,</u>	1	<u>.</u>	2	2	8	8	8	8	8	8		=	15	1					<u> </u>	-	=	ā	ā	ā	ī		=	=	17	17	=	=	-	-	-		<u> </u>	1		1	-	13	=	=	-			+	i	┪	Eur	H	
17 2 2 2	2	2 2	~ ~	<u>.</u>		+	Ē	•	-	•	•	•	•	_	2		-	7	1	200	1	1	1	†	1	7	7	7	-	-	-	^	5	5	2	2	"	10	1	1	1	1	1	1	-	10	-	0	<b>پ</b>	۲	-	12	2	2	~	7	7	2	7	+	1	+	1		2	2	2	2	9	-	-	7	1	+	2	1	Ĭ
	-			4	Н	+	Ļ	ŀ		-	L		Ц			-	4	1	+	1	+	ļ	1	1	1	1	-	-	-	-	_	_	-			_	L	<u> </u>	T	1		1	I T	ŀ	L	L	L	L			L	L		Ц	-	1	1	+	+	+	+	ļ	ļ	-	-			+	+	+	+	+	1		O. Meto		a series
		Щ				1	ļ	L	L				L					4	1	1	1	1	1	1	1	4											L	L	-		-		ļ	-	ļ	L	Ļ	L	_	L	-	L				-	1	1		1	1	1	ļ	_				4	-	1	1	1	4		Ě	1	
		Ш			Ц		L			L	L									1																		L	ļ	1	L	L	L	L	L	L	L	L	L	L		L										1		L						1	1	1			Rew		7
	Š	5	åğ	5 5	5	2	5	8	15.5	130	70	75	30	=	2.5	å	5		4	0	:	:   :		2		5	8	\$	235	5	2	ő	25	5	910	Š	145	15		1	10	1		130	15	3	25	5	25	5	120	5	27.5	2.5	5	5	5	-		-	1	1	1 2	å	3	3	5	5	3	6	5	4	4	4	Ožav.	Ž	ormad o
	Ш			+	Н	+	$\downarrow$	Ļ	L	L	L					4	1		+	1	ļ	1	+	+	1	4	-	4	-	_		_	_	_		_		-	ļ	+	-		L	L	L	L	Ļ	L	L	L	L				-	4	1	+	1	1	+	+	+	ļ	Ļ	_		4	+	+	1	4	1		ž	_	-
0 7 3	20	5 5	5 5	5 7	5	5	-	25	20	20	15	15	10	17	7	5	5	=	-	3		•	:	:	3	2	2	5	35	2	5	25	20	5	27	24	20	22	1	1	1	-	1	1	5	12	ā	20	23	20	=	5	=	15	5	2	2	2	-	- -	-	1	:	70	5	-5	2	ē	7	5	1	-		Ž	doss	Ozone	
					П	1	Ī			Ī							-	1	T	1	T		Ī	Ī	T													Ī	Ī	Ī	Ī		T	Ī					П	Ī		ĺ											T			П			1	1	1	1	}	Į	residual	Clo	
$\left  + \right  +$	+	+	+	+	Н	+	+	L	L	L	-				Ц	+	+	+	+	+	+	$\dagger$	Ŧ	+	+	+	4	1	-	-	-	-			_	L.	L	H	H	H		-	-	t	+	-	H	$\vdash$		_	-	<u> </u> 			+	-	1	+	+	+	$\dagger$	+	+					+	+	+	1	+	ī	1	i i	[	
222	-	11	- 5	: :	=	:	:	5	85	•	5	85	64	15	6.5	5	=									2	122	17.2	5	122	122	123	2	123	12.2	2	122	177					2	2	171	12	121	122	122	122	122	122	122	122	12.2	22	=	2	2	177				12.2	12.2	123	173	123	122	123	172	121	E cord	T I	7	Contact	
	Ц	Щ			Ц	1	1	L								4		1	-	1	1	1	1	1	1	1		4		_						_	L	ļ	1	1			L	ļ	-		L	_		L	L	L				1		1	1	1	1	1	1	L	L			4	-	-	1	-	3		L		
						1	L						Ц				1	1	1		1	1		1	1											L	L	L	1	1			L		L	L				L	L	L			Ц				1	1	1	1	1	1	L								_	-	ž	)	
																																																														İ												1 te	i en e	Otavio	Ozemet
0 0 1 0		0 20	2 0	2 2	90	8 8	2025	2	068	085	9.65	20	920	950	0 25	2	8		2	2 2	2 6					0	0 3	016	20	2	017	923	2	017	0.07	0.67	0.47	073	8			1		2	2	030	015	107	072	80	0 4	20	ŝ	ê	8	8	015	000	0	015	2 2	1		100	8	9	0.25	019	70	ŝ	2	=	2	1	residual posidual	02000	On Condi
0 0 0	2 - 2	0 0	0 0	9 9	0	9 0		0	0.31	9	022	0.25	9	0.7	00	-		3					;	+			8	9	-	9	00	9	9	å	0	2	8	01	00	9	9			0	9	00	å	0	0 [	00	00	00	00	å	٥	å	å	à	á i	<u>.</u>	1		+		0 2	0.0	9	60	0 %		8	9	9	1	losida	Ozen	674
4000	9 0	0 0	0 0		6	0 0		١			2	0	2		9	-						<u> </u>		<u> </u>	2		2	2	١	~	0	9	ء ھ	ă	9	9	0				  -				9	٥	â	٥	٥	٥	12			ā	ā	<u>ة</u> اه	ā	â	ā i	š ,		  -			-	٥	٥	ě		2		١	e P	=	1954	00	
0024	7 2	X &	-	28	=	200	=	۲	24	۳	=	24	8	2	8	=	ē	1	1	-	1	1	5 8	1	-	8	8	8	8	2	2	E	ă	ö	=	2	8	8	18	12		=	18	7	8	8	200	12	2	8	8	8	8	8	8	8	8	8		5 1	3 5	* k	15	-	8	2	2	ä	7	8	4	1	2	٥	7	2	
8 2 2	2 2	5 2	2 0	8 8	007	2	8	033	2	×	100	0 23	8	010	8	2	8	2	3	8 8	3 8	3 8	3 8		8	8	8	8	8	8	8	8	8	8	8	ŝ	8	900	8	8	9	9	2	8	8	901	910	0	100	2	20	8	200	0100	010	9	8	8			3 5	1	1	100	8	000	001	900	2	8	8	ន	2	2	Sides.	1	
284	220	200	88	20 0	8	8 0	8	027	900	0.32	8	0 10	9	8	8	8	8	8	3	8 8	3 8	3 8	3 8	3	3	8	8	8	ŝ	8	8	8	8	8	8	8	8	2	200	2002	2		2	8	2	9	004	9	8	982	002	8	-0010	-0010	800	8	å	900	400	4	3		2	9	801	9100	001	A 010	9	8	8	8	2	1	Feeddu	Ozene	
A 0 0 0	2 0	0 0	8 8	9 0	90	5 5	0		00	02	00	00	9	00	00	8	9	3	1		,	+	;	+	+	9	8	9		9		8	9	80	2		9	9	90	2		١	2	0	90	A	90	-	9	ē	2	00	9	ė	å	á	à	à l	6	3			e		9	ě	å	å		9		+	ç	I	7	020	
1 기기	10	2 =	r 8	4	*	١	12	٦	*	-	đ	ď	đ	đ	đ	٥	9	1	1	4	1,	١	١	1	3	6	6	5	6	đ	ಕ	٥	9	٥	٥	8	18	15	10	12	14	1	٦	٦	1	ĕ	Z	O.	=	×	12	12	=	ð	ŏ	ĕ	취	ă	ă i	\$  <sup>3</sup>	1	1	1	1	ä	á	ă	ă	-	7	٥	1	×	٥	E	į	

,	Ozene	Personal	ī	<u>ت</u>	20	20	631	3	640	950	200	30	27	ž	8	-	=	20	037	¥	3	2	2	5	033	Xi O	g	9.25	023	120	20	0.72	0.63	20	0.78	87	9	0 (5	0 19
Condition	Ozone	To section i	¥	₹ 5	3	950	86	2	9/0	2	0 52	20	80	12	X	80	ş	7	8	80	2/0	2	150	290	350	2	*	2	š		350	25.0	92.0	23	850	30	0.47	٤	59.0
Ozenaflen Cenetti			der C																																				
ľ	ᄂ	ī	-		-		-	-	-	-		-	-		-	-	-	$\vdash$	-		-			-	-					-	_		-	-			-		_
	Centact	1	(Province)	selector)	•	-	7.0		6.5	8.4	-	7.0	:	7 20	6.4		7.0	7	3	7.9	7.9	6.5	-	4.5	5.2		88	7	4	5.5	¥.	8.8	5 9	6.5	6.5	6.4	59	• 5	-
	L	١.	•	(You co									L					Ĺ	L																_		_		_
	Ozome	cesidens	Ě		L		L	L				L		L		L	L																						
	Ozem	98 CJ8	T.		1 2	=	15	=	=	2	-	5	-	20	20	=	-	2	=	15	-	2	2	-	~	-2	-	-	12	12	=	15	=	20	-	-	=	2	33
		¥																																					_
Bromate	2	Ozon.			•	•	20	35	250	9	125	2	2	120	X	30	-	9	S	9	80	=	2	100	•	•	2	•	•	9	Ŷ	0	140	215	120	120	9	9	5
Ľ		X																																					
		Ħ.			,																													ĺ					
Temperature	1	Ore			Γ																																_		_
-		N. S.			17.8		17.8	17.8	3	16.2	16.2	2	162	162	162	159	159	15.9	159	15.	200	121	127	13	6 33	101	86	500	70	10.2	60	-	117	=	•	ž	121	19.5	2
		ž						Γ	18									Ī				7.05	2	202	1 70	1.78	7.87	7.76	7.83	177	27.0	88			178	8	35.		_
Ł	-	Olem.			17.9	8	Ţ	g	7.87	28.9	8	/89	8	:	8	77	8	2	7	8	2	828	16.0	8	8	8	=	8 15	122	20	212	921	7.86	8	828	37	27.2	3	6 52
		ž				Ī			787	8	8	_	8		<del></del>							33	2	8	8	8	=	51.5	122	4 07	612	181	33	*	6.28	<b>8</b> 37		85	
Γ		#																																					_
Turbidity	EL M	Ozea			Γ																																		
		Raw							20													190	8	2		13	-	30	14	22	13	0.77			890	60	=	52	35
ľ		Ä										Ī			Γ	Γ																						П	_
Bramide	Trace	9 0 0			0.42	14	0 41	0.42	20	SS	33	250	33	N	2	150	25	200	25	653	950	620	930	R			ž		0.31	0.31	150	920	83	8	9. Q	20	6 27		7.0
		P.				Ī																																10	ž
	150	#			Γ																																		_
Atkalen	A MS CM	Kaw Otes. F.																																					L
	Ē	à							2					Ĺ		Ĺ					Ŀ	r	2			22	2		ш	2	æ	7	2		2	8		8	8
		1	_		Ĺ	Ĺ	Ĺ		0.033			Ĺ	L	L	L	L	L	Ĺ	L	L		0033				9000	9000	180	0 032	6000				Ĺ		9000			Ĺ
Wall	2 Com	Ozea			L	L	L	L	200		L	L	L		L	L		L	L	L	L	900			L	8	8	1	900	087	90.00	900	L	L	0.047	900	0.008	Ц	L
	f .	٤.			•	1	Ł		١.			•			1		•			4		1-1	•			-	1		-							1	_	أحا	_

| 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 110294 | 1

S/15/94 3 25	6/14/94 3 22							5/19/94 3 66			Γ	5/16/94		T	1,000	T	107.04 A R.7	T		Ī	100 5	Ī	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	OF C. CRICKE	T	11/18/93 2.94	11/17/93 3.05			11/3/93 3 45		Wex	1_	Date		WATER QUALITY DATA: CONVENTIONAL		6. Indicate with an "X" if data reported as "Fift." are from samples collected after sedimentation only:		Diologue state and A.J	dicate with an 'Y'	Describe level of study:		Source water ID:	Source water:		Study ID:	outily so:
2.6	2.46	2 08	231	2 31	2 31	2.31	2.73	2.57	2 68	2 57	2.5/	25/	2.57	7 57		2	2 40	257	77.5	2	23	105	0.7	718	7.40	0.92	0.78	1.52	2.14	248		Till.	mg/L)	100		A: CONVE		la reported a										
0 1 18	ī	T			T	7		- 1			T	Т	ī	Т	Т	Т	Т	Т	Т	2 13	0 123	0 123		3 5	1	Т	0 118	0.112	0.113			Nan	(1/cm)	UV-Z54		NTIONAL		S "FIR." are		],	×							
0 059	9	0048	0045	0.045	0.045	Q.	000	0.050	0 056	0053	0.053	93		2 2	2 9	2 9	2	0	0.057	2	0028	000	000	000	2 0			0.0238	0 0346	0 0532		7.	=======================================	254				from sam		Full-scale	Pilot-scale	Bench-scale		SE L	Sou		P.	
78	à	11	70	70	70	70	20	85		95	5		1 2	200		2 3	3		23	3	2 :	2	25	2 2	2 8	20	82	8	85	83		,,,,,,	(mg/L	2				ples colls				2		State Project Water	South Bay Aquaduct		Pilot Study 93-94	_
																																100	(mg/L as Lacos)	Alkanniny				cied affer						Water	uaduci		3.94	
75	18			53		Ī					Ī		-						51	1	1	Ī	1		Ī	T	21			2		R S	1		$\dagger$	-	9	sedimenta		filtration.	affer co	- F	-	-	1	-		
13	E					١				1		12	1				1	1	1			1	T	T	T	T	2	Ī			+	- 10 m	ı		$\mid$		after sedi	tion only:		<u>.</u>	paquiation	data sheet		/Slate	(River		(Optim	
133		13	13	3	3	3	28	26	20	29	67	1		315	1	¥!:	31:	2	150	3 3	8	81	22	3:		18	5	2	122	17	+	t	mg/L as C	Hardness	-		mentation			_	Rocculat	FM. re		(State Project water, blend of, etc.)	(River, lake, groundwater,		(Optimization Study 9/95, etc.)	
			-		-	_						1	-		1				1	1	1			1	1		L					Raw	accus accus	2	-		and filtrat		1	-	on sedim	ers to dat	-	t Hend of	dwaler, elc)		y 9/95, etc	
																																					ion:				affer coaquiation, flocculation, sedimentation, and	in this data sheet, "Fill." refers to data collected		ekc)	٦		٥	
500		560	170	170	170	170	670	500	530	150	1	100		45	200	5	630	550	ğ	236	170	170	35	4	3	220	220	230	150	170		1		l a							١		1	Ī				
																									T								19/6	Browne														
296	<u> </u>	<u> </u>	8	120	28	8	_			!	1	+	1	1	1	1		8	1	1	1	-	-	1	1	<u> </u>	l		-		1	<u> </u>  .		$\frac{1}{1}$	+				1	1	1	-	1	1	$\frac{1}{1}$			
13	1	1					5	69	9	18	1	5 8	318	5 3	ار	72	2	3	-	3	2	72	57	5)			=	75	5)	6.1			וווים רוארו	Chiotian		-	×						1	1	1			
																																		3 8														
		2 2	2.	235	2	22	2.7	2	26	~		2 2		2 2	2	2	2	2	2	2	23	23	2	21	3 12			23	123	2:				_	T									T	Ť	Sources	4. If bler	_
	T	Γ	Γ							Ī			Ī		Ī	T															Ì	Ť	(mg/L)	100	1				1	1		Ì	1	$\dagger$	50	ources and proportions:	If blended source water indicate	
	T	Т		250 966				73 54	ľ	1	1	2001	1	5 57		1	İ	-1	737	1	- 1	- 1	ł	1	20	1	١.		ĺ	237 2.9	+	<u> </u>			+				1	+	-	1	+	$\dagger$	Source	ortions:	e water in	
Г	T	0 072				٦				Γ	Γ	2 0	T	T	Ţ	3	I	1	0 10	T		1	T	000	1	T	3 17	Γ					F 12	Moldiny			r			1			1	1			dicate	_
04						•	u		7	-								7											Ī		Ì		22	Ì	T				j				j	Ť	25			_
6.2	2	: =	7.6	7.8		Ì				2	l	T	T	2 2	I	T	T	787	7.50		7.75	7	-	758	1	122	7.42	7.48	7.58		4	+	╬	3	-	-			1	1		1	1	+	+		$\prod$	-
145		716	6 23	6 23	23	6.23	. 3	7.08	7.28	8	18	8 8	1 2	3 -	7	77	6.78	2	2	5	5 52	540	2	1		6.24	5 53	5 52	8	7.98		1		1	+		-		+	-	1		+	1	+			_
16.2		1	14.5	14.5	14.5	14.5	16.8	18.5	18.5	16.2	100	100		3 6	17.8		2	5	125		7	17.7	18.7	3	# 1 i	1/3	16.4	18.8	18.7	18 7			Dag.	due	1													
												Ī																				Ţ	500	- superature														

6
2
2
×
п,

Uffilty ID:												H								
										1	+	1	1			+	1	1		
. Study ID:											-									
										1	1	1	+		1	+	1	1		
C SOUTE WE	İ									1	$\frac{1}{1}$	-	+			+		-		
3. Source wa											<u> </u>		-			$\mid$	l			
										-	_	-	<u> </u>		Indicate coagulants studied:	pulants stuc	lled:	$\frac{1}{1}$		
5. Describe I										-					Q	oagukan	Chemical formula	ormula	Units	
indicate wit											-	-			F	Alum	K(rOS)ZIY	100	Z E	
											<u> </u> 		<u> </u>		7	erric Chi	Fects	-	mor	
İ											-				-		-			
I. Indicate w															7					
											-	-	<u> </u>							
WATERO															TREATMENT CONDITIONS	NT COND	TIONS			
											_		4				-	-		
Date			Chła	Chlorination conditions	SIL.						1	Disinfection By-product				Coada	Coagulation Conditions	itions		
		Fittered								MHLL		HAAS	-	-	Coagulant	Dose	Acid	Base	Coag.	Coag.
	Indicate disinfectant(s)	nfectani(s)	Chlorine	Ammonia	dudvoni	bubation time	Incub.	H	Residual	집		(trg/L)			Ω	ž	adjusted? a	adjusted?	Ηd	temp.
	used with	X. uz	#30p	dose		(h)	lemp.		FREE	Raw			Fift. Raw Fill	_1	(see apove)		3,5	(KR)	=	(deg. C)
-		CHIOFATHING	Img Cale	Img who will		CHIOLEUM	+	1	(mig Cital)	1		1			1	5	-		,	1
11/3/83	,	,	2.6	8 9	0.23	124	25 25 25 25 25 25 25 25 25 25 25 25 25 2	1	90	1	8 2	196		218		3 8	2 2	z	90	\$   \$
11/18/03	\ \	< ×	2.4	0.33	0.25	12	20 10 25	20.8	-		1	12	. 5	25.0	-	\$ 5	2 >	2 2	8 5	
11/17/93	×	×	2.4	0.39	0.25	72	20 10 25		1.17		=		157	2	-	2	<b>&gt;</b>	2	5.53	
11/16/93	×	×	2.4	0.35	0.25	72	20 10 25	-	1.05	-	=	1=	15	2	-	9	>	z	8 24	186
11/3/93	×	×	2.3	0.69	0.17	72	20 10 25	8.8	2.07		ň	24	1	29.3	2	15	2	z	6.73	10.0
11/3/93	×	×	23	0.57	0.17	72	2010.25	-	1.72		~	1	5	15	2	18	z	z	6.59	2
11/4/93	×	×		0.55	21.0	72	20 10 25	1	165		20	=	-	23	2	2	z	z	7.06	19.5
11/4/93	×	×		0 69	0.17	2	20 10 25	1	207	1	=	=  }	2	5	2	2	z	z	63	2
11/15/03	×	×		0.36	0.25	2	20102	-	6	1	2 1	=	•	9 9	2	8	- -  :	z	5 45	2
11/16/03	<b>*</b>	×   >		0.35	0.25	12	2002	5.67	96	1	3 8	103	2	20.3	,	2 5	- >	z 2	5.49	18 6
2/15/04	×	×	2	0.67	0.00	72	20 to 25	1	2	1	2	F	2	382	-	150	·z	2		128
4725794	×	×	2	0.39	0.25	12	20 to 25	6.71	1.16		28	==	-	20.3	2	22	z	z	8.66	17.5
4127/94	×	×	2	0 32	05.0	12	20 to 25		70.0		7	×		23.7	2	23	z	≂	6.77	17.1
4/28/94	×	×	2	0.33	0.50	72	20 10 25	-	-		22	=	9	22.1	7	23	z	z	2 84	16.5
\$72794	×	×	2	0.33	2	72	20 0 25		66.0		2	2	0	24.5	7	23	z	z	6.76	12
5/16/94	×	×	2	0.33	0.25	2 5	20 02		- 6		29 5	7	,,	8 8	7	13 15	z	z	8	2
2/16/04	(×	×	1	F. 0	3 8	12	20 to 25	1	250		212	3/2	2 0	2 8	,,	3 5	2 2	2 2	2 2	
5/16/94	×	×	2	0.10	280	72	2010 25	1	0.3		26		2	28.7	2	R	z	z	2 08	133
5/17/04	×	×	2	0.27	0.50	12	20 10 25		0.82		88	2	21.3	25.1	2	23	z	z	7.39	180
5/19/94	×	×	2	0.28	0.50	72	20 to 25		0.85		95	7	•	25.5	2	23	z	z	7.14	187
5/24/94	×	×	2	0.24	0.50	72	20 to 25		0.72		22	×	14	24.5	2	3.6	z	z	68.9	2
3/1/94	×	×	2	0.38	0.25	72	20 10 25	-	1.15		₽	-	1.5	15	7	43	z	z	6.54	15.1
3/1/84	×	×	2	0.33	0.50	72	20 to 25	1	-		8	-	15.2		2	43	z	2	6.54	151
3/1/04	×	×	2	0.27	8	7,7	2010 25		80		2	=	25	187	2	Ç	2	z	6 54	15.1
201784	×	×	2	0.22	2 00	12	2010 25	6 23	0 65		8	-	2	22.3	2	5	z	z	6.54	15.1
6/13/84	×	×	2	030	0.25	2,	202		0.89	1	8	1	2	8	2	8	z :	z	707	2
6/14/94	× >	κ,	7	0.29	200	2)	2 2 2		100	T	1	r) [	21.	210	7	8 5	z	2 :	2	8
0/15/0	χ,	۲,	,	30	200	77	500	2			-	1	97	3	,	315	z	z	41.1	9
O/1D/W4	×	×	2	U.1/	76.3	7,7	20.00	1	100	-	-	٩		3	1	77	- -	z	6 62	0.81

4 25	273	·	Γ	392	·	T	T	151	<del></del>	<del></del>	7	T	1000		1000	500	<b>FII</b>		+11	111	110		na	181	τ		151 0	9110	1		5 18	SIE		16/91/9
99 7	213		l	192	t	ļ	1	152	·	1	1	1	003			022	E11	1		1	19		09 Z9	84	+			811.0	<del> </del>	<del> </del>	224	3 25		16/51/9
£\$ \$	112	i	1-	592			<del> </del>		-			<del> </del>	072			081	1			111	95		85	187	<del> </del>			1110	<del> </del>	<del> </del>	90 Z	3 22		V5/11/9
57	593	ļ —		£92				114			1	1	330				SIL			511	88	<del>                                     </del>	69	ii	1			1210			412	3.2		P6/E 1/9
18 9	242			538			1	15			1	1	015			081	RŽI			128	87	<del></del>	li.	68	-	1		921.0	1		213	3.69		2/54/84
15	714			192				69					1		200	OBI	021	1		150	07	1	ii -	58		1		1110	1		61.2	38 C		16/61/5
76 7	117			398				69					350		530	180	150			150	99		99	10			0120	281.D			96°Z	37.5		16/11/5
LSS	546			241				OS					Ē			091	6Z1		138	158	67		61	58			8120	0.142	2.24		£	16.E		16/91/5
15 3	530	ļ		182	ļ	<b> </b>	<u> </u>	121					055			300	121			121	29		85	18				191.0			3.05	99 1		215/94
69 8	582	<b> </b>	<b> </b>	280	<b></b>	<u> </u>	<b> </b>	11/		<u> </u>	ļ		061		0\$\$	061	921			156	19		69	18	1			0.193			3 08	85 7		1/28/84
18 1	288	ļ		274		<b></b>	<del> </del>	ET	-	<b></b> -	ļ	<b> </b>	920			061	121		121	121	09		19	58	J	ļ		881.0	<del> </del>	ļ	80 E	197		101751
16 5	102		ļ	272	ļ	L	ļ	DL				ļ	370		055	OLS	124		124	154	65		65	18	<del> </del>	<u> </u>	0.209	181.0			3 06	9 }		15/52/7
99 6	212	<b> </b>		512	<b> </b>				· <del> </del>			- <del> </del>	GET			300	101		101	101	95	ļ	ES	DΖ	<b> </b>			1110			2.18	50 €		16/11/C
15.1	233			512		<del> </del>	<del> </del>				ļ		140			041	113			£11	E+		77	07	<del> </del>			292 0			56 2	28 S		75/1/E
1011	521	<del> </del>		112			<del> </del>	·	·		ļ		001			200	\$!!			511	<u>/S</u>		09	£8	<del> </del>		0.293	0.215	157.1		99 Z	(28 )		115/184
	233	l		8ZZ		<del> </del>		Z9	·			ļ	<del> </del>			150	101		101	211	20		97	11/	<del> </del>		<u>'</u>	051.0	<b></b>			20 S		56/11/01
	233	ļ		827	····	<del> </del>		29	<del> </del>	<b> </b> -	<del> </del>	1	}		720	150	101		201	701	58		<u> </u>	59	<del> </del>		1/10	021.0	<del> </del>		)8'Z	205		10/14/93
	112	<del></del>		378	i	<del>                                     </del>	<del>                                     </del>	29		i	<del> </del>	<del> </del>				150	701	<del> </del>	201	201	99		59	59	<del> </del>			051.0	1	·	20	ZOS		10/1/83
	220			621		l		ZC	1		50	t	ł			06	211			211	23		79	96	<del>                                     </del>	[I		960 0	1	ļ ——	59 C	27.5		10/13/93
89 5	220			641		1		25	1	l	\$ 6		t			06	žii —			zii	cc	<b> </b>	78	96	1	1		960'0	1	l	3 88	3 45		10/13/93
2 45	DOZ	l		841				25	1		50	1			520	06	911			911	29		61	96	<b></b>	1		901 0	1		CO E	19 €		10/15/83
205	00Z	l		841		I		25	1		50						911			911	29		6 <i>L</i>	95	1			901.0				79.E		10/15/83
6/ 6	161			LLI				23			50	1			160	06 06	ZOI			105	19		19	63	1			0.102				3.48		ERITION
61.6	161			LLI				23			50				199	05	Z01		ZOI	201	19		29	C6			091.0	501.0			25.2	3 48		10/1/93
67.9	261			081				20			50					06	60 t		601	100	15		19	76				860 O			161	3.6		10/8/83
	ZBI	<u> </u>		ETI	l			31			\$ 0				082	0.8	011			011	0/		99	96			081.0	501 0			5 69	3 26		10/2/93
	5/1			168			ļ	0C			5.0	<u> </u>	<u> </u>			OB	102		501	901	125		65	148	.	\		101.0	<u> </u>	<b> </b>	5 23	2 62		ERING!
	81	<b> </b> -	<b></b>	5.82	<b> </b>		<del> </del>	91		<del> </del>			<u> </u>	l	740	DŞ				87	SI		21	43				851.0			21	25 2		16/1/6
1:	69	ļ		1.52			<del> </del>	91			ļ	<del> </del>	ļ			<del>-</del> :		ļ		11	41	l	81	0>	<del> </del>	<del> </del>	\$11.0	BS1.D	<del> </del>	ļ	90 1	5 31		E5/92/1
15	is			197	<b> </b>		<del></del>	32		<del> </del> -	<del> </del>		ļ			071		ļ	36	38		<u> </u>	41	8£	├			****	<del> </del>	<del> </del>	CE.I	278		8122183
	520			988	<del> </del>	├		{aı	┼	<del> </del>	ļ		.	ļ		550	<b> </b>	·		121	5 9	<del></del>	89	64	+		9710	0.043		<del> </del>	61.E	82.8		2/56/93
	062	}		012	<del> </del>	<del> </del>	<del></del>	<del> </del>	-}		<del> </del>	<del> </del>	061			230	130		051	130	25	<del> </del>	89	51	-	-		1100			50 E	98 5		£6/\$Z/\$
01	220			524		<del> </del>		<del> </del>	-	<del> </del>	<del> </del>	·	01	ļ		091							67		· <del> </del>	·	I			·	2.37	3 28		£6/81/5
																			INII	icni	116									1				
11					ļ —		<del> </del>	<del> </del> -	<del> </del>	<del> </del>	ļ	·					701			501	13-	<del> </del>	184	29	<del> </del>	<del> </del>	150.0	750.0	\Z	<del> </del>				
11				332		-	_	1-	1	_	1		011			0/1	ZD3			011	13			89			noo	2200	ζ.	<u> </u>	59 Z	15 €		26/11/5
																	70;				13						7.00	220 0	ζ.			321	втотВ	
	597			338									011	000		0/1			011	ott			100	89	170.0				Z		59 Z	stati s	втотВ	£6/11/5
	598		192	538				ц					011	260		110	511		911	SII	96		65	11	1200		621.0	121 0	1 35		59 Z 21 Z	3 S I	втотВ	16/E1/9
5 7	69Z		192	538 563 563				11/					010	320		021 095 095	<u>511</u>		911	S11	95		100	17	920 0		EZ1 0	121 0	Z 1 22 1 4 69 8		59 Z	35 25 35 35 35 35 35	втотВ	76/C1/9 76/C1/9
5 ¥ 15 5			192	538									011 011	260 260 180 180		110	511		511 511	SII	96		65	11			EZ1 0	121 0	Z ZC 1 69 1 98 1		59 Z 21 Z	3 S I	втотВ	16/E1/9
5 P 15 S 15 S	592 518		19Z 19Z	522 522 522 541				05					010	180		021 095 995 057	511 511 621		211 211 211	511 511 621	95 95 11 61		65 65	11 11 25	0 05e		EZ1 0 EZ1 0 91Z 0	121 0 121 0 145	1 25 1 25 1 69 1 82 5 54		59 Z 21 Z	3 5 E E E E E E E E E E E E E E E E E E	втотВ	16/01/9 16/01/9 16/01/9 16/91/5
5 P 25 S 25 S 26 S 26 G	548 548 548		267 267 263 263 283	522 523 523 541 541				0S 0S					011 040 050 050	090 087 087 085		021 260 260 420 420	621 621		911 911 911	6ZL 6ZL 6ZL	95 85 74		65 65 65	#9 #1 #1 #1 #6 #6	0 050 0 052 0 031		815 0 621 0 621 0	0 151 0 151 0 145 0 145	2 1 25 1 8 6 8 8 1 8 2 5 4 1 8 2 5 4 1 8 2 2 5 2 5 4 1 8 2 2 5 2 5 2 5 2 5 2 5 2 5 2 5 2 5 2 5		2 12 2 13 2 13 2 13 2 13 2 19 2 19 2 19 2 19 2 19 3 19	2 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	втотВ	16/11/8 16/11/8 16/1/8 16/1/8 16/1/8 16/1/8 16/1/8 16/1/8 16/1/8
5 P 25 S 25 S 26 S 26 S	248 248 248 294 294 284		267 283 283 283 283 283	\$32 \$23 \$23 \$41 \$41 \$15 \$15 \$15 \$15 \$15 \$15 \$15 \$15 \$15 \$1				05 05 01					011 020 020 020 020	180		021 095 995 057	511 511 621 621		511 511 521 521	SI ! SI ! 6Z ! 6Z ! FZ !	95 11 61 95		65 65 64 65	12 12 14 56 56 58	0 052 0 031 0 032 0 033 0 033		8120 8120 8120 6210	121 0 121 0 21 0 21 0 21 0 21 0 181 0 181 0	201 691 881 727 1 22 1 22 2 24 1 22 1 22 2 3		2 12 2 13 2 2 13 2 2 2 2 2 2 2 2 2 2 2 2 2 3 2 3 2 3 3 3 3	15 C 25 25 26 26 26 26 26 26 26 26 26 26 26 26 26	втотВ	16/11/6 16/11/9 16/11/9 16/91/5 16/91/5 16/52/1 16/52/1 16/51/5
5 F 15 S 15 S 16 G	592 548 548 548 543 543		267 283 283 283 283 248 248	\$120 \$22 \$21 \$41 \$41 \$15 \$15 \$12 \$12 \$12 \$12 \$12				05 05 01					010 020 020 020 010 011	090 087 087 085		200 110 110 110 110 110 110 110 110 110	511 511 621 621 721		911 911 911 921 921 921	SII SII SII 6ZI 6ZI 7ZI 7ZI	95 95 95 96 97 98 98		65 65 64 65	## ## ## ## ## ## ## ## ## ## ## ## ##	0 050 0 031 0 033 0 033 0 033 0 053		605.0 815.0 815.0 621.0 621.0	0 151 0 151 0 145 0 145 0 181 0 181 0 181	1 25 1 69 1 82 1 82 2 55 1 22 5 35 1 22 5 35 1 22 5 35 1 22 5 35 1 22 5 35 1 22 5 35 1 22 5 35 1 22 5 35 1 22 5 35 1 22 5 35 7 35 7 35 7 35 7 35 7 35 7 35 7 35		59 Z 21 Z 21 Z 2 C C 90 C 90 C	15 C 2	втотВ	16/11/9 16/11/9 16/11/9 16/91/5 16/91/5 16/91/5 16/5/2/1 16/1/16
6211 165 165	598 548 548 594 594 543 543		267 267 263 263 263 263 263 263 263 263	\$12 \$22 \$22 \$24 \$34 \$35 \$32 \$32 \$32 \$32 \$32				05 05 01					011 020 030 030 030 030 030 030 030 030 030	090 087 087 085		110 260 260 260 260 260 260 260 260 260	511 511 621 621 721 721 701 711		671 511 671 671 671 671 671 671	SI   SI   SI   SI   SI   SI   SI   SI	95 95 14 64 95 65 95 Ct		66 65 65 66 65 65 65 65 75	07 07 18 07 77 26 18 17 17	0 052 0 031 0 032 0 033 0 033		602.0 815.0 621.0 621.0 621.0	0 151 0 151 0 165 0 165 0 181 0 181 0 111 0 282 0 512	1 25 1 69 1 82 2 55 1 22 2 5 2 5 1 22 2 5 1 21 1 21 1		21 Z 21 Z C C C 90 C 90 C 81 Z	15 C 2 C 2 C 2 C 2 C 2 C 2 C 2 C 2	amo18	16/11/6 16/21/8 16/21/8 16/31/5 16/31/5 16/31/6 16/31/6 16/31/6 16/31/6
67.1 99.6 12.2 12.2 12.2 12.2 12.3 12.3 13.4 14.1 15.2	248 248 248 284 284 242 242 243 243		267 267 267 283 283 283 248 248 250 250 250 250 250 250 250 250 250 250	\$12 \$22 \$22 \$24 \$34 \$32 \$32 \$32 \$32 \$32 \$32 \$32				05 05 01					011 020 020 020 020 021 021 021 021	090 087 087 085		200 120 120 120 120 120 120 120 120 120	511 511 621 621 721 721 721 721 731		511 511 511 521 121 121 121 121 121	SII 511 621 721 721 721 721 721 721 721 721 721 7	95 85 74 64 95 65 95 C7		65 65 65 69 69 19 05	68 68 68 68 68 68 68 68 68 68 68 68 68 6	0 050 0 031 0 033 0 033 0 033 0 053		602 0 602 0 602 0 602 0 602 0	0 151 0 151 0 165 0 165 0 181 0 181 0 181 0 181 0 505 0 505	201   69   69   69   69   69   69   69   6		65 Z 21 Z 23 Z C C 90 C 90 C 90 E 81 Z 85 Z 99 Z	15 °C  2 °C	Bromas	PS/C1/9 PS/C1/
5 P 25 S 25 S 26 S 26 S 26 C P 29 6 20 C	598 548 548 594 594 543 543		567 567 563 563 563 563 563 576 576 576 576 576 576 576 576 576 576	\$12 \$27 \$27 \$21 \$31 \$31 \$31 \$32 \$32 \$32 \$32 \$32 \$32 \$32 \$32 \$32 \$32				05 05 01					011 020 020 020 020 021 001 001	090 087 087 085		200 200 120 120 120 120 120 120 120 120	511 511 621 621 721 721 701 711		511 511 521 721 721 721 721 731 731 731	SII SII SII SII SII SII SII SII SII SII	95 95 14 64 95 65 95 Ct		66 65 65 64 69 89 05 95	#9  /// /// 56 56 18 19 0/ 0/ 0/ 58 5/ 29	0 050 0 031 0 033 0 033 0 033 0 053		605.0 815.0 815.0 621.0 621.0	0 151 0 151 0 165 0 165 0 181 0 181 0 111 0 282 0 512	201   69   69   69   69   69   69   69   6		5 5 2 2 13 7 2 13 7 2 0 2 0 2 0 3 0 0 2 18 7 3 0 0 5 18 7 5 18 7 6 0 0 6 0 0 7 18 7 8 18	15 C 2 C 2 C 2 C 2 C 2 C 2 C 2 C 2	Вголя	PERCLIP PERCLIP PERCLIP PERCLIP PERSLI
15 5 15 5 16 5 16 5 16 9 17 1 19 6	248 248 248 284 284 242 242 243 243		567 567 563 563 563 563 563 576 576 576 576 576 576 576 576 576 576	\$12 \$22 \$22 \$24 \$34 \$32 \$32 \$32 \$32 \$32 \$32 \$32				05 05 01					011 020 020 020 020 021 021 021 021	090 087 087 085		200 120 120 120 120 120 120 120 120 120	511 511 621 621 721 721 721 721 731		511 511 521 721 721 721 721 731 731 731	SII 511 621 721 721 721 721 721 721 721 721 721 7	95 85 74 64 95 65 95 C7		65 65 65 69 69 19 05	68 68 68 68 68 68 68 68 68 68 68 68 68 6	0 050 0 031 0 033 0 033 0 033 0 053		602 0 602 0 602 0 602 0 602 0	0 151 0 151 0 165 0 165 0 181 0 181 0 181 0 181 0 505 0 505	201   69   69   69   69   69   69   69   6		65 Z 21 Z 23 Z C C 90 C 90 C 90 E 81 Z 85 Z 99 Z	15 °C  2 °C	Bromas	PS/C1/9 PS/C1/
19 5 15 5 16 5 16 5 621 1 99 6 11 1 9	248 248 248 284 284 242 242 243 243		567 567 563 563 563 563 563 576 576 576 576 576 576 576 576 576 576	\$12 \$27 \$27 \$21 \$31 \$31 \$31 \$32 \$32 \$32 \$32 \$32 \$32 \$32 \$32 \$32 \$32				05 05 01					011 020 020 020 020 021 001 001	090 087 087 085		200 200 120 120 120 120 120 120 120 120	511 511 511 621 621 621 721 701 701 711 701 701		511 511 521 121 121 120 120 121 120 121 121 121 1	SII SII SII SII SZI SZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7	95 85 74 64 95 65 95 C7		66 65 65 64 69 89 05 95	#9  /// /// 56 56 18 19 0/ 0/ 0/ 58 5/ 29	0 050 0 031 0 033 0 033 0 033 0 053		602 0 602 0 602 0 602 0 602 0	0 151 0 151 0 165 0 165 0 181 0 181 0 181 0 181 0 505 0 505	201   69   69   69   69   69   69   69   6		5 5 2 2 13 7 2 13 7 2 0 2 0 2 0 3 0 0 2 18 7 3 0 0 5 18 7 5 18 7 6 0 0 6 0 0 7 18 7 8 18	15 C 2 C 2 C 2 C 2 C 2 C 2 C 2 C 2	Broma	PERCLIP PERCLIP PERCLIP PERCLIP PERSLI
11	972 972 973 974 974 974 974 974 974 974 974 974 974		267 267 267 268 268 268 268 276 276 276 276 277 277 277 277 277	\$12 \$22 \$22 \$21 \$21 \$21 \$21 \$21 \$21 \$21				05 05 01 02					011 020 020 020 020 020 021 021 021 021	090 091 097 097 055 055		110 200 200 200 200 200 200 200 100 100	511 511 621 621 721 721 721 721 721 721	.0020	511 511 511 521 721 721 721 721 721 721 721 721 721 7	SII SII SII SII SII SII SII SII SII SII	95 85 71 61 65 95 65 95 CP 25 25		66 66 66 69 69 69 75 77	### ### ### ### ### ### ### ### ### ##	920 0 920 0 1E0 0 0 0 0 0 0 0 920 0		CO 0 CO 0 CO 0 CO 0 CO 0 CO 0 CO 0 CO 0	121 0 121 0 20 1 20 1 20 1 20 1 20 1 20	20 1 69 1 69 1 69 1 60 1 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7		65 Z 21 Z 21 Z C C 90 C 90 C 90 E 11 Z 65 Z 99 Z 60 C 21 Z 65 Z	15 C 2 C 2 C 2 C 2 C 2 C 2 C 2 C 2	Brooms	PERCLIP PERCLIP PERCLIP PERCLIP PERSLI
19 5 15 5 16 5 16 5 621 1 99 6 11 1 9	202 202 202 203 203 203 203 203 203 203	Ozon,	267 267 267 263 263 268 276 276 276 276 276 276 277 277 277 277	\$12 \$27 \$27 \$21 \$31 \$31 \$31 \$32 \$32 \$32 \$32 \$32 \$32 \$32 \$32 \$32 \$32	in the second se	-10020		05 05 01 02	EW		ilias	West	011 020 020 020 020 021 001 001	090 097 097 095 055 055	Juas	200 200 120 120 120 120 120 120 120 120	511 511 511 621 621 621 721 701 701 711 701 701	CZcor.	011 511 511 521 721 721 721 721 701 011 011	SII SII SII SII SZI SZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7	95 85 74 64 95 65 95 C7		66 65 65 65 65 65 65 69 69 69 64	#9 #9 #9 #9 #9 #9 #9 #9 #9 #9 #9 #9 #9 #	920 0 920 0 1E0 0 0 0 0 0 0 0 920 0		ES 0 ES 0	121 0 121 0 20 1 20 1 20 1 20 1 20 1 20	201   69   69   69   69   69   69   69   6	- uozo	65 Z (1 Z	15 C 2 C 2 C 2 C 2 C 2 C 2 C 2 C 2	Вгота	PERCLIP PERCLIP PERCLIP PERCLIP PERSLI
15 5 16 5 16 5 16 5 16 5 16 7 17 1 19 6 17 1 19 6 17 1 19 1 11 1	972 972 973 974 974 974 974 974 974 974 974 974 974	JA.) Ozon,	267 267 267 263 263 268 268 270 270 270 270 270 270 270 270 270 270	\$12 \$22 \$22 \$21 \$21 \$21 \$21 \$21 \$21 \$21	- Wild	(1/1)	βω)	05 05 01 02	1913	(WN-E)	HN Buu)	weß	011 020 020 020 020 020 021 021 021 021	090 081 081 095 055 055	juas sil)	110 200 200 200 200 200 200 200 100 100	511 511 511 621 621 621 721 701 701 711 701 701	(2002)	511 511 511 621 721 701 611 611 611 611 611 611 611 6	SII SII SII SII SZI SZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7	95 85 71 61 65 95 65 95 CP 25 25	Cacco	65 65 65 65 65 65 65 77 77 95 67 74 74 74 74 74 74 74 74 74 74 74 74 74	#9 #9 #9 #9 #9 #9 #9 #9 #9 #9 #9 #9 #9 #	920 0 920 0 1E0 0 0 0 0 0 0 0 920 0	(111	#### (1/10)	121 0 121 0 20 1 20 1 20 1 20 1 20 1 20	20 1 69 1 69 1 69 1 60 1 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	. (7/	13 Z 2 13 Z 2 13 Z 2 C 2 09 C 90 C 9	15 C 2 C 2 C 2 C 2 C 2 C 2 C 2 C 2		EBIT 175  PERC 178  PERC 1
15 5 16 5 16 5 16 5 16 5 16 7 17 1 19 6 17 1 19 6 17 1 19 1 11 1	972 972 973 974 974 974 974 974 974 974 974 974 974	Ozon,	267 267 267 263 263 268 268 270 270 270 270 270 270 270 270 270 270	\$12 \$22 \$22 \$21 \$21 \$21 \$21 \$21 \$21 \$21	EIK	(1/1)		05 05 01 02	W4	(WN-E)		weA	011 020 020 020 020 020 021 021 021 021	090 097 097 095 055 055	juas sil)	110 200 200 200 200 200 200 200 100 100	511 511 511 621 621 621 721 701 701 711 701 701	CZcor.	511 511 511 621 721 701 611 611 611 611 611 611 611 6	SII SII SII SII SZI SZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7	95 85 71 61 65 95 65 95 CP 25 25	Cacco	66 65 65 65 65 65 65 69 69 69 64	#9 #9 #9 #9 #9 #9 #9 #9 #9 #9 #9 #9 #9 #	920 0 920 0 1E0 0 0 0 0 0 0 0 920 0	(111	ES 0 ES 0	121 0 121 0 20 1 20 1 20 1 20 1 20 1 20	20 1 69 1 69 1 69 1 60 1 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	. (7/	65 Z (1 Z	15 C 2 C 2 C 2 C 2 C 2 C 2 C 2 C 2	smo18	PERCLIP PERCLIP PERCLIP PERCLIP PERSLI
11	972 972 973 974 974 974 974 974 974 974 974 974 974	JA.) Ozon,	267 267 267 263 263 268 268 270 270 270 270 270 270 270 270 270 270	\$12 \$22 \$22 \$21 \$21 \$21 \$21 \$21 \$21 \$21	'MES	(1/1)	βω)	05 05 01 02		(WN-E)	HN Buu)	WeB	011 020 020 020 020 020 021 021 021 021	090 081 081 095 055 055	juas sil)	110 200 200 200 200 200 200 200 100 100	511 511 511 621 621 621 721 701 701 711 701 701	(2002)	511 511 511 621 721 701 611 611 611 611 611 611 611 6	SII SII SII SII SZI SZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7	95 85 71 61 65 95 65 95 CP 25 25	Cacco	65 65 65 65 65 65 65 77 77 95 67 74 74 74 74 74 74 74 74 74 74 74 74 74	#9 #9 #9 #9 #9 #9 #9 #9 #9 #9 #9 #9 #9 #	920 0 920 0 1E0 0 0 0 0 0 0 0 920 0	(111	0 123 0 123 0 129 0 129 0 200 0 0 0 0	MEH (20 0 151 0 0 151 0 0 151 0 0 0 151 0 0 0 151 0 0 0 151 0 0 0 0	2 1 2 1 2 2 1 2 2 2 2 2 2 2 2 2 2 2 2 2	) (7) 3:	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	15 C	scrift.	FENT INS  PENT I
15 5 15 5 16 5 16 5 16 7 1 99 6 11 1	972 972 973 974 974 974 974 974 974 974 974 974 974	JA.) Ozon,	267 267 267 263 263 268 268 270 270 270 270 270 270 270 270 270 270	\$12 \$22 \$22 \$21 \$21 \$21 \$21 \$21 \$21 \$21	EIK EIK	(1/1)	βω)	05 05 01 02	Elli.	(WN-E)	HN Buu)	weß	011 020 020 020 020 020 021 021 021 021	090 081 081 095 055 055	juas sil)	110 200 200 200 200 200 200 200 100 100	511 511 511 621 621 621 721 701 701 711 701 701	(2002)	511 511 511 621 721 701 611 611 611 611 611 611 611 6	SII SII SII SII SZI SZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7	95 85 71 61 65 95 65 95 CP 25 25	Cacco	65 65 65 65 65 65 65 77 77 95 67 74 74 74 74 74 74 74 74 74 74 74 74 74	#9 #9 #9 #9 #9 #9 #9 #9 #9 #9 #9 #9 #9 #	920 0 520 0 100 0 520 0 520 0 520 0 520 0 520 0	(w \$\$?	0 123 0 123 0 129 0 129 0 200 0 0 0 0	MEH (20 0 151 0 0 151 0 0 151 0 0 0 151 0 0 0 151 0 0 0 151 0 0 0 0	2 1 2 1 2 2 1 2 2 2 2 2 2 2 2 2 2 2 2 2	) (7) 3:	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	15 C	scrift.	EBIT 175  PERC 178  PERC 1
15 5 15 5 16 5 16 5 16 7 1 99 6 11 1	972 972 973 974 974 974 974 974 974 974 974 974 974	JA.) Ozon,	267 267 267 263 263 268 268 270 270 270 270 270 270 270 270 270 270	\$12 \$22 \$22 \$21 \$21 \$21 \$21 \$21 \$21 \$21	EIK	(1/1)	βω)	05 05 01 02	EW.	(WN-E)	HN Buu)	weA	011 020 020 020 020 020 021 021 021 021	090 081 081 095 055 055	juas sil)	110 200 200 200 200 200 200 200 100 100	511 511 511 621 621 621 721 701 701 711 701 701	(2002)	511 511 511 621 721 701 611 611 611 611 611 611 611 6	SII SII SII SII SZI SZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7	95 85 71 61 65 95 65 95 CP 25 25	Cacco	65 65 65 65 65 65 65 77 77 95 67 74 74 74 74 74 74 74 74 74 74 74 74 74	#9 #9 #9 #9 #9 #9 #9 #9 #9 #9 #9 #9 #9 #	920 0 052 0 031 0 00 0 0 0 0 0 0 0 0 0 0 0 0 0 0	tati-scs	10 (21 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	MEH (20 0 151 0 0 151 0 0 151 0 0 0 151 0 0 0 151 0 0 0 151 0 0 0 0	######################################	NT) NEMLIC	2 28 2 1 2 1 2 1 2 2 2 2 2 2 2 2 2 2 2 2	west	scrift.	FENT INS  PENT I
15 5 15 5 16 5 16 5 16 7 1 99 6 11 1	972 972 973 974 974 974 974 974 974 974 974 974 974	JA.) Ozon,	267 267 267 263 263 268 268 270 270 270 270 270 270 270 270 270 270	\$12 \$22 \$22 \$21 \$21 \$21 \$21 \$21 \$21 \$21	- HE	(1/1)	βω)	05 05 01 02	EIN	(WN-E)	HN Buu)	west	011 020 020 020 020 020 021 021 021 021	090 081 081 095 055 055	juas sil)	110 200 200 200 200 200 200 200 100 100	511 511 511 621 621 621 721 701 701 711 701 701	(2002)	511 511 511 621 721 701 611 611 611 611 611 611 611 6	SII SII SII SII SZI SZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7	95 85 71 61 65 95 65 95 CP 25 25	Cacco	65 65 65 65 65 65 65 77 77 95 67 74 74 74 74 74 74 74 74 74 74 74 74 74	#9 #9 #9 #9 #9 #9 #9 #9 #9 #9 #9 #9 #9 #	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Full-scs Full-scs 254 [m]	0 123 0 123 0 129 0 129 0 200 0 0 0 0	MEH (20 0 151 0 0 151 0 0 151 0 0 0 151 0 0 0 151 0 0 0 151 0 0 0 0	(7X)  AMAL+O  1 69 1  2 1 7 1  2 1 7 1  2 1 7 1  3 1 6 1  4 1 6 1  5 1 7 1	VET) AENJUC ANGURU	2 28 2 13 2 13 2 19 2 19 2 19 2 19 2 19 2 19	west	scrift.	FENT INS  PENT I
15 5 15 5 16 5 16 5 16 7 1 99 6 11 1	972 972 973 974 974 974 974 974 974 974 974 974 974	JA.) Ozon,	267 267 267 263 263 268 268 270 270 270 270 270 270 270 270 270 270	\$12 \$22 \$22 \$21 \$21 \$21 \$21 \$21 \$21 \$21	WES	(1/1)	βω)	05 05 01 02	ESS	(WN-E)	HN Buu)	west	011 020 020 020 020 020 021 021 021 021	090 081 081 095 055 055	juas sil)	110 200 200 200 200 200 200 200 100 100	511 511 511 621 621 621 721 701 701 711 701 701	(2002)	511 511 511 621 721 701 611 611 611 611 611 611 611 6	SII SII SII SII SZI SZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7	95 85 71 61 65 95 65 95 CP 25 25	Cacco	65 65 65 65 65 65 65 77 77 95 67 77	#9 #9 #9 #9 #9 #9 #9 #9 #9 #9 #9 #9 #9 #	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	tati-scs	10 (21 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	MEH (20 0 151 0 0 151 0 0 151 0 0 0 151 0 0 0 151 0 0 0 151 0 0 0 0	(7X)  AMAL+O  1 69 1  2 1 7 1  2 1 7 1  2 1 7 1  3 1 6 1  4 1 6 1  5 1 7 1	NT) NEMLIC	2 28 2 13 2 13 2 19 2 19 2 19 2 19 2 19 2 19	west	scrift.	FENT INS  PENT I
15 5 15 5 16 5 16 5 16 7 1 99 6 11 1	972 972 973 974 974 974 974 974 974 974 974 974 974	JA.) Ozon,	267 267 267 263 263 268 268 270 270 270 270 270 270 270 270 270 270	\$12 \$22 \$22 \$21 \$21 \$21 \$21 \$21 \$21 \$21	WE STATE OF THE ST	(1/1)	βω)	05 05 01 02	- W-3	(WN-E)	HN Buu)	wen	011 020 020 020 020 020 021 021 021 021	090 081 081 095 055 055	juas sil)	110 200 200 200 200 200 200 200 100 100	511 511 511 621 621 621 721 701 701 711 701 701	(2002)	511 511 511 621 721 701 611 611 611 611 611 611 611 6	SII SII SII SII SZI SZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7	95 85 71 61 65 95 65 95 CP 25 25	inily (Sacos)	65 65 65 65 65 65 65 65 65 65 65 65 65 6	######################################	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Bench-s Full-sca Full-sca	(1) (2) (2) (3) (4) (4) (4) (4) (4) (4) (4) (4) (4) (4	121 0   121	(X) (X) (X) (X) (X) (X) (X) (X) (X) (X)	VC) AEMILO ANIED NO. Per	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	west	PUNAUD	Part In Street I
15 5 15 5 16 5 16 5 16 7 1 99 6 11 1	972 972 973 974 974 974 974 974 974 974 974 974 974	JA.) Ozon,	267 267 267 263 263 268 268 270 270 270 270 270 270 270 270 270 270	\$12 \$22 \$22 \$21 \$21 \$21 \$21 \$21 \$21 \$21	ME	(1/1)	βω)	05 05 01 02	EW.	(WN-E)	HN Buu)	Me 5	011 020 020 020 020 020 021 021 021 021	090 081 081 095 055 055	juas sil)	110 200 200 200 200 200 200 200 100 100	511 511 511 621 621 621 721 701 701 711 701 701	(2002)	511 511 511 621 721 701 611 611 611 611 611 611 611 6	SII SII SII SII SZI SZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7	95 85 71 61 65 95 65 95 CP 25 25	inily (Sacos)	65 65 65 65 65 65 65 65 65 65 65 65 65 6	#9 #9 #9 #9 #9 #9 #9 #9 #9 #9 #9 #9 #9 #	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Bench-s Full-sca Full-sca	(1) (2) (2) (3) (4) (4) (4) (4) (4) (4) (4) (4) (4) (4	121 0   121	(X) (X) (X) (X) (X) (X) (X) (X) (X) (X)	VET) AENJUC ANGURU	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	west	PUNAUD	FENT INS  PENT I
15 5 15 5 16 5 16 5 16 7 1 99 6 11 1	972 972 973 974 974 974 974 974 974 974 974 974 974	JA.) Ozon,	267 267 267 263 263 268 268 270 270 270 270 270 270 270 270 270 270	\$12 \$22 \$22 \$21 \$21 \$21 \$21 \$21 \$21 \$21	NI d	(1/1)	βω)	05 05 01 02	M3	(WN-E)	HN Buu)	west	011 020 020 020 020 020 021 021 021 021	090 081 081 095 055 055	juas sil)	110 200 200 200 200 200 200 200 100 100	511 511 511 621 621 621 721 701 701 711 701 701	(2002)	511 511 511 621 721 701 611 611 611 611 611 611 611 6	SII SII SII SII SZI SZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7	95 85 71 61 65 95 65 95 CP 25 25	inily (Sacos)	65 65 66 66 66 66 66 66 66 66 66 66 66 6	### ##################################	eved was colored was colored was colored was colored was colored was colored was colored was colored was colored was colored with colored was colored	(State Pr Bench-s Priot-sca Full-sca Full-sca (m)	221 0 0 (221	121 0   121		VENTIC	1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	west	: CI Tablew TIJAUD acrel T	EBILIS  PERLIP P
15 5 15 5 16 5 16 5 16 7 1 99 6 11 1	972 972 973 974 974 974 974 974 974 974 974 974 974	JA.) Ozon,	267 267 267 263 263 268 268 270 270 270 270 270 270 270 270 270 270	\$12 \$22 \$22 \$21 \$21 \$21 \$21 \$21 \$21 \$21	EIN	(1/1)	βω)	05 05 01 02	EW	(WN-E)	HN Buu)	weF	011 020 020 020 020 020 021 021 021 021	090 081 081 095 055 055	juas sil)	110 200 200 200 200 200 200 200 100 100	511 511 511 621 621 621 721 701 701 711 701 701	(2002)	511 511 511 621 721 701 611 611 611 611 611 611 611 6	SII SII SII SII SZI SZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7	95 85 71 61 65 95 65 95 CP 25 25	inily (Sacos)	65 65 66 66 66 66 66 66 66 66 66 66 66 6	######################################	eved was colored was colored was colored was colored was colored was colored was colored was colored was colored was colored with colored was colored	(State Pr Bench-s Priot-sca Full-sca Full-sca (m)	221 0 0 (221	121 0   121		VC) AEMILO ANIED NO. Per	1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	west	: CI Tablew TIJAUD acrel T	Part In Street I
15 5 15 5 16 5 16 5 16 7 1 99 6 11 1	972 972 973 974 974 974 974 974 974 974 974 974 974	JA.) Ozon,	267 267 267 263 263 268 268 270 270 270 270 270 270 270 270 270 270	\$12 \$22 \$22 \$21 \$21 \$21 \$21 \$21 \$21 \$21	WE .	(1/1)	βω)	05 05 01 02	EW.	(WN-E)	HN Buu)	Me 5	011 020 020 020 020 020 021 021 021 021	090 081 081 095 055 055	juas sil)	110 200 200 200 200 200 200 200 100 100	511 511 511 621 621 621 721 701 701 711 701 701	(2002)	511 511 511 621 721 701 611 611 611 611 611 611 611 6	SII SII SII SII SZI SZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7	95 85 71 61 65 95 65 95 CP 25 25	inily (Sacos)	est constant of co	11 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	opeci we color of the color of the color opeci we c	(Paver, 1s (Sizie Pr Bench-r Phol-sci Full-sca Phol-sci	221 0 0 (221	Mes (101) (1	25   1	VENTIC  Vention  Say Aquet  Say A	1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	west	:Of ranksw TIJAUO permit	1, Source 1, Sou
15 5 15 5 16 5 16 5 16 7 1 99 6 11 1	972 972 973 974 974 974 974 974 974 974 974 974 974	JA.) Ozon,	267 267 267 263 263 268 268 270 270 270 270 270 270 270 270 270 270	\$12 \$22 \$22 \$21 \$21 \$21 \$21 \$21 \$21 \$21	NIS	(1/1)	βω)	05 05 01 02	1813	(WN-E)	HN Buu)	Meg	011 020 020 020 020 020 021 021 021 021	090 081 081 095 055 055	juas sil)	110 200 200 200 200 200 200 200 100 100	511 511 511 621 621 621 721 701 701 711 701 701	(2002) (2002)	511 511 511 621 721 701 611 611 611 611 611 611 611 6	SII SII SII SII SZI SZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7	95 85 71 61 65 95 65 95 CP 25 25	inily (caces)	est constant of co	### ##################################	opeci we color of the color of the color opeci we c	(Paver, 1s (Sizie Pr Bench-r Phol-sci Full-sca Phol-sci	221 0 0 (221	Mes (101) (1		VENTIC  Vention  Say Aquet  Say A	1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	west	:Of ranksw TIJAUO permit	EBILIS  PERLIP P
15 5 15 5 16 5 16 5 16 7 1 99 6 11 1	972 972 973 974 974 974 974 974 974 974 974 974 974	JA.) Ozon,	267 267 267 263 263 268 268 270 270 270 270 270 270 270 270 270 270	\$12 \$22 \$22 \$21 \$21 \$21 \$21 \$21 \$21 \$21	EIN	(1/1)	βω)	05 05 01 02	EW	(WN-E)	HN Buu)	West	011 020 020 020 020 020 021 021 021 021	090 081 081 095 055 055	juas sil)	110 200 200 200 200 200 200 200 100 100	511 511 511 621 621 621 721 701 701 711 701 701	(2002) (2002)	511 511 511 621 721 701 611 611 611 611 611 611 611 6	SII SII SII SII SZI SZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7	95 95 95 95 95 95 95 95 95 145 75 11 11 11 11 11 11 11 11 11 11 11 11 11	in My	26	12	alon Stu oped we oped we cale oped we	(Opdiniz) (Plater, Is Sanch-s Banch-s Phol-sc: Full-scs Tull-scs	221 0 0 (221	### ### ### ### ### ### ### ### ### ##		Pilot Pilot Person Pers	1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	west	:Of ranksw TIJAUO permit	Contract  Contra
5 F LS S LS S 18 S 18 S 18 S 18 S 18 C 18 L 19 6 11 L	972 972 973 974 974 974 974 974 974 974 974 974 974	JA.) Ozon,	267 267 267 263 263 268 268 270 270 270 270 270 270 270 270 270 270	\$12 \$22 \$22 \$21 \$21 \$21 \$21 \$21 \$21 \$21	"NE	(1/1)	βω)	05 05 01 02	- E.W.	(WN-E)	HN Buu)	Me 5	011 020 020 020 020 020 021 021 021 021	090 081 081 095 055 055	juas sil)	110 200 200 200 200 200 200 200 100 100	511 511 511 621 621 621 721 701 701 711 701 701	(2002) (2002)	511 511 511 621 721 701 611 611 611 611 611 611 611 6	SII SII SII SII SZI SZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7ZI 7	95 95 95 95 95 95 95 95 95 145 75 11 11 11 11 11 11 11 11 11 11 11 11 11	inily (caces)	26	12	alon Stu oped we oped we cale oped we	(Opdiniz) (Plater, Is Sanch-s Banch-s Phol-sc: Full-scs Tull-scs	221 0 0 (221	### ### ### ### ### ### ### ### ### ##	25   1	Pilot Pilot Person Pers	1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	west	:Of ranksw TIJAUO permit	1, Source 1, Sou

8/16/94	6/14/94	20139	HEN 255	5/19/94	5/17/94	2 2 2 2	200	12/19	1/25/94	3/14/94	FVIR	2/15/94	107794	2010	10/14/9	CENTINGS	10/13/93	10/12/93	10/12/93	107793	10/6/9/	10/5/93	10/4/93	9/1/93	8/26/93	1725/93	118793	5/26/93	5/25/93	5 5			6/13/94	6713794	5/16/94	5/16/94	125/94	750	2 2	1000	2259	5/18/93	5/11/2		1		Date	ļ	WATER	W. 750	T			J. Source		Z. Source		Study !	UNINY ID
1 58																								2	1 1		2	4.2	ال		,		1	=	214	214	202	200	1 2	2 2	, .	=	2		JEG.	2	lurbidity			T	T							I	Ī
						T				Ĩ		1		T					1	Ī	1	T																T							0201	1	N N			I	I	$\prod$							
0 037	0.04	004	0 056	0 058	000	9	27	0.058	005	0.087	0 077	0 0	0 6	2 5	313	0.128	0.128	0.065	0.065	0.058	000	0 054	0.04	0 02	0	0.05	0 997	0.21		9		Ĺ	6200	2	0.067	990	005	0		200	2	2	D 08		r an						I							I	
798	8.29	8.1	1.12	- 56	871	2		7.64	787	72	76	7.59	7.15			7.83	7.93	7.6	7.6	7	2 0	7.8	17.	7.47	7.6	7.3	7.4	6.8	2	7.			0		5.04	8 01	7.87	7.87	728	7	7 0	7.8	7.8		72.4														
6.79	Ī	Г	6.83		T	T	1	0.00	Г	П	П		Т			7		$\overline{}$		- F	8 0	7	1	1	_		7	9						1	}	- 1	İ	i	1	1	1	8	П		TUBC			Γ	Γ	T	T	Ī		Γ		$\prod$			
6 79	Г	ı	6.83	ı	- 1	Т	Т	T	Т	Г	5.4	T	T	Т	7	7,16	1 1		- 1			1			1 3	1	1 1		8 33	1	1	Ť	1	6.8		[	- 1	1		ı	1	6 56		7	OZOII.		3	-	1	T	1	T	T	T	İ	П	7	1	1
79 704	1	$\overline{}$	1	1	- 1	1	1	1	1	1	1 1	- 1	- 1	- 1									2 844	1	0.35	ı	821	- 1	T	5.56	†	t	T	6 87	Г	1	-1	7	Т	1	T	6.56	П	+	-	٦			$\dagger$	$\dagger$	†	†	$\mid$	T	$\vdash$	П	†	†	$\dagger$
1	Π	П			Т	Т	T	Т	Т	ī	П	П	T	Т	Т	Т		7	1	-	1	Γ	Т	Т	Г	Г	Γ	٦	T	55	$\dagger$	$\dagger$		1	-		Т	T	Т	T	T	Τ	П	+	1	+	+	$\dagger$	T	$\dagger$	$\dagger$	t	l	-	-	Н	$\dagger$	†	$\dagger$
182	1			- 1	- 1		1	ŀ	1	l	1	- 1	1	-	1	[	1 1		- 1	- 1	- 1	1	1	1	ł	1		П	87	2 2	T	t	Т	1	Ī.		ſ	1	T	Т	T	21		$\dashv$	-	4	1	-	+	$\dagger$	+	$\dagger$	<u> </u>	$\vdash$	ŀ	H	+	+	+
5 5	12	20	2.0	-	8	77	7 4		12	14.2		28	<u>تا:</u>	2	3 =	9	1.6	5	=	9		0	9	12	6	3	9	6.7	7.8	-	-	$\perp$	20	9	7.7	1.7	72	7.7		T	1	21.5	9.2		15	1000	- Charledon	-	+	+	+	+	+		-	H	$\dashv$	+	+
-	_	_			1	+	+	-	-	-	Ц	-	+	+	1	-				+	1	-				L	<u> </u>		-	_	+	1	-	ļ ,.	L		+	+	+	+	+	<u> </u>	Н	$\dashv$		2 5	1	-	+	+	+	+	+	+		Н	+	+	+
20.5	21.9	20.8	8	197	9	6	5	10		-	16 6	=	5 3	3	3 5	18	20	9	8	2	2   1		0	100	17.72		25 8	<b>5</b>	-	21.8	+	<u> </u> 	1	20.8		H	-	Т	Ī	5	Т	21.8	1		1	÷	1	1	+	+	+	+	+	-	-	$\dashv$	4	+	+
$\perp$	<u> </u>	-			-	+	+	1				-	 	+	+	-			+	+	<u> </u>	<u> </u>	  -	H		L				1	1	<u> </u>	5	100	24	24	2	2	22	+	-   5	15	2	-	200			-	$\dotplus$	+	+	+	H	-	<u> </u>	$\frac{1}{1}$	+	+	+
$\mathbb{H}$	-		Н		1	+	+	+	-	L	Н	+	+	+	+	1			+	+	+	H	<u> </u>	T	<u> </u>	L	L	$\dashv$	_  =	+	1	1	+	-	-		-	$\dagger$	+	+	+	H	Н	+				F	+	+	+	+	+	<u> </u>	-	H	$\frac{1}{1}$	+	+
22	-	3.5	2	2.1	2.7	24	4	3 2	1	2.2	<u>                                     </u>	<u>- </u>	+	+	+	+			1	+	$\frac{1}{1}$	+	+	+	-		L	2	1	5	+	+	+	-	<u>                                     </u>		+	+	+	$\frac{1}{1}$	†	_			19.	7		-	t	+	+	+	+	+	$\frac{1}{1}$	H	+	+	$\dagger$
2.1	3.2	32	N	21	20	29	<u></u>	1 2	1	26	2	N	N .	77	2 5	-	<u> </u>	_	17.4	۵.	1		<u>: -</u>	<u>. _</u>	1	22	_		35	<u> </u> .	╬	$\frac{\perp}{1}$	Т	112	Г	29 1	2	2	76	<u>راد</u> اد	, 0	: <u> </u>	-		<del>-</del>	<u>" </u> 	BIELLOUIS	<u>'</u>  -	+	$\frac{1}{1}$	+	+	<u> </u>	$\frac{1}{1}$	-	Н	1	+	+
$\parallel$	_			-   	+	+	$\frac{1}{1}$	+	-			+	+	1	+	+			-	+	$\frac{1}{1}$	<u> </u>	-	L	L	L		4	1	+	+	+	990	9	8	500	9	=	1	318	1	╀		i	724			ŀ	Ŧ	+	+	+	H	+	T	H	+	+	+
$\mathbb{H}$	<u> </u>				+	+	+	+ T	<u> </u>	-		1	+	+	+	+			4	+	+	ŀ	1	-			L		1	+	+	$\frac{1}{1}$	-	+	L.		1	+	+	1	1	  -	H		Settl. Ozor	200	5	ŀ	$\dotplus$	$\frac{1}{1}$	+	+	+	H	H	H	$\dashv$	+	+
$\mathbb{H}$	_	-			4	$\downarrow$	+	-	+	H	-	-	+	+	+	+			4	+	+	+	$\perp$	<del> </del>	L	L			4	+	+	1	+	1	_		_	1		+	<u> </u>	$\perp$		H	4			-	$\downarrow$	$\downarrow$	+	+	1	+	<u> </u>	H	$\dashv$	+	+
+	L	_			1	+	+	1	+	L		1	+	1	1	Ļ			4	+	 	1	l	1	ŀ	L			1	1	+		5150	8	8	300	8	570	2 2	318	3 8	ē	1	$\dashv$	7	1	<u> </u>	+	$\downarrow$	+	+	$\downarrow$		<u> </u>		$\sqcup$	4	+	+
																															-		>	×	×	×	×	×	×	×,		×	×	chlorine	used with an 'X'	5													
Ħ					1	$\dagger$	$^+$			T		1	Ì	†	1	t			1	$\dagger$	Ť	T	$\dagger$	t	ļ	-			1	İ	1	Ť	Ť	Ť	-		i	t	i	†	$\frac{1}{1}$	Ì		chlo	À	2		-	T	$\dagger$	$\dagger$	Ť	T	Ť	1	П	İ	İ	Ť
							1											İ											İ	ļ			^	(IX	×	×	×	×	×  '	×   '	1	×	×	chloramina	X				L										
																																												(mg CI2/L)	dosa														
H	<u> </u>			7	1	1	1	+	+	$\vdash$		1	+	+	+	+			1	1	1		$\vdash$	Ť	<u> </u>	<u>L</u> 			+	1	$\dagger$	÷	Т	T	Ī	П	ī	Т	ī	Т	ī	25			Ţ	٦		ŀ	╁	$\dagger$	$\dagger$	Ť	+	t	t	H	$\dashv$	$\dagger$	$\dagger$
																																		10	051	0 53	047	8	8	3	2	8	0.73	TIN-CHN Per	dose		COMMISSION COMMISSIONS												
$\parallel$				1	1	$\dagger$	$\dagger$	$\dagger$		h		1	1	1	$\dagger$	t			+	1	1	t	t	l	r	-			1	t	1	Ť	1	1			- 1	-1	-	1	П	1	l I			1	000	-	t	†	$\dagger$	$\dagger$	$\dagger$	$\dagger$		H	1	T	$\dagger$
	L																									L							65	200	2	083	280	2	2	2 3	3 8	0083	083	chlorine	9	1	SOOM												
																																	ioa	168	168	168	168	2	2 2	2 3		168	168	chlos amine	(h)	1													
-	H	-		+	-	$\dagger$	+	+	-	-	H	+	-	+	+	-			+	+	+	-	+	-		_		-	+	1	-	+	-	18	20	20-	2	8	2 3	3 3	1 2	8	20	me (deg. C)	1	5		-	$\dagger$	+	+	+	+	-		H	1	+	+
$\parallel$	L		Н	1	+	+	+	<u> </u>	_	-		+	+	+	+				+	+	$\frac{1}{1}$	<u>L</u>	1	1		L	-	+	1	+	+	+		Г	1		Т	Т	Т	Т	Т	ī		П	7	7		F	+	+	+	+	<u> </u>	+		$\parallel$	$\dashv$	+	+
				1	+	+	+	+	+		H	+	+	+	+	+		-	+	+	+	-	-	-	-			+	4	1	+	1	1,6	5 67	6	365	5 79	92	200			38.0		9	1	$\dashv$		-	+	+	+	+	+	+	-	H	$\dashv$	+	1
																																	-		1.5.	1 55	-		6			1 97	211	(mg CIZ/L)	7.00	a idea													
						1		Ī				j	1	1		$\prod$						İ										Ī	ľ				Ĭ	1	Ĵ			Ī	Ī	_	Z)	Ť	1	T	Ţ	†	Ť	Ť	Ī	Ī			1	†	1
				Ĭ																Ī																									3	-	-		$\prod$	I	T	$\underline{\mathbb{I}}$	T						

6/16/94	6/15/94	21.0	\$67.179	2	2100	2/16/94	72/94	4/28/94	4/27/94	4/25/34	3/14/94	3/1/94	2/15/94	1/27/54	10/14/93	10/14/93	10/14/93	10/13/93	10/13/93	10/12/93	10/12/93	10/7/93	10/7/93	10/5/93	CESSO	10/193	8/1/93	8/26/93	8/25/93	8/18/93	5/26/93	2/25/33	5/18/93	S/11/93			3	200	2107	2/16/34	* C 2.1	1000	2	2	21/31	21.50	5750	SALIA				_	Date		WATER					a. applica		9000	Rouge	, transfer	2	Unitely ID:
							Γ	Ī	Γ	T		T																									]	Ī		Ī		T	T		T	T				Ozon.	Ž	E				Ī				T	1					
			1	T		T	Ī			Ī		Ī		T	Ī									1						Γ	Γ			Γ		Γ			2	2					2	إر	Ι.	]_	Ī	F.H.	: !						T	Ï		Ī	Ī	T	Ī	Ī	T	Π
П		1		1	1		T			T		Ī	T	T		Ī	Γ								1						İ				Γ	Ī	1	Ī	Ī	T	Ī	T	T			T	T	T		Raw				Γ		T	T			Ī	T	T	T	T	T	Г
	1	1	1	+	Ť	Ť	Ì	Ť		T	T	T	Ì		T	r	r	l		_				1	1			-					Ì	l	T	İ	T	T	İ	T	T	Ť	İ	1	Ť	T	$\dagger$	T	t	Set.		_		_	<u> </u>	İ	İ	T	T	Ť	T	Ť	Ť	T	Ť	T
Ħ	1	1			1		T	T		T		T	1	-		T	T	l					1	1	1							İ			T	T	1	İ	T	Ì		Ť	Ì	1	T	1	†	T	1	Ozon.	(hg/L)	BAAH		l			$\dagger$		1	İ	T	Ť	†	T	T	T
П		1	1	1	$\dagger$	1	T	İ		T	Ì		T	T	T	r	r							1	1				r			İ	T	T			1	<u></u>	: 5		; ;		;	3	=   =	,	<u>.</u>	90.5	;	-	1 1		Disinfection		-	T	T	Ť	T	T	T	T	Ť	T	T	
	1	1	1	1	†	Ì	1	T	Ì	Ì	Ì	Ť	Ì			r	T	-						1		1					Ì		T	T	T	1	f	Ť			-	1	1	1		1	1	ni u	+	Raw	-	r	on By-p	H	-	t	1	Ì	1	†	$\dagger$	Ť	†	Ť	t	Ħ
H			1		†		$\mid$	T			t	t	t	r	l	İ	l						1	1	1	1						İ	T	<del> </del>			t	+	1	T	T	t	t	t	T	†	†	t	-	10		Ļ	By-products	-	l	T	t	Ť	1	Ť	t	Ť	$\dagger$	t	t	T
П	1		1	Ť	1	1				T		Ť	T	İ			T	r	╁	-					1	٦					r		T	T	f	T	t	T	1	T	T	T	T	†	Ť	Ť	$\dagger$	Ť	T	M. Ozon.	1,18	BYYH				T	T	Ì	T	t	t	†	†	t	t	T
П	7	†	1	†	$\dagger$	†	t	t		t	-	1	t	-	r	-	-	H					1	1	1	1					-	ļ	İ		r	T		+	+		ă	- - - - - - - - - - - - - - - - - - -		1		<b>,</b>	<u> </u>	07.0	!	ı. Fin.	, ,			-	-	t		t	+	t	$\dagger$	+	Ť	$\dagger$	t	T
Н	1	†	+	+	$\dagger$	t	t			r	t	t	İ	r	T		-						1	1	1			_	H	İ	-					T	ľ	9 9			Ť	14		7		1	1	7) 0	+	Raw	-	<u> </u>		-			t	t	t	$\dagger$	+	t	$\dagger$	$\dagger$	$\dagger$	Ħ
H	1	1	+	+	$\dagger$	+	T	T	l	t	+		-		-	-		-	-			1	1	1	1	1		_	-	-	-	T		İ		+	t	$\dagger$	İ	t	+	$\dagger$	+		Ť	i	+	+	+	Sett	Ę.			-		+	T	T		t	t	+	$\dagger$	+	t	$\dagger$
П	†	1	1	$\dagger$	†		İ	-	İ	_		$\frac{1}{1}$	T	T	İ	-			-	-		1		1	1					-	-	ĺ	İ	l	H	r	t	$\dagger$	t	t	t	İ	†	+	$\dagger$	+	†	+	$\dagger$	Settl. Ozon.	CIAL	XOT			-	t	ŀ	H	$\frac{1}{1}$	t	Ť	t	t	t	t	+
H	+	+	+	$\dagger$	Ť	+	t	l	$\dagger$	<u> </u>			-	r	-	H	-					1	1	+	+	1		_			-		-	H	┝	H		t	+		$\frac{1}{1}$		+	+	†	$\dagger$	$\dagger$	+	t	FIR.					<u>L</u>	-	-	-	t	+	t	$\dagger$	t	†	$\dagger$	
	1	1	İ	T	T	Ī	T																	j	1			-				-			r	T	1	3	-		_	,		٠,	3	3	1	3/2		-	ð	Coagul			TREAT		Ť	Ī	İ	Ť	Ť	Tipul Calva	-		T	Ī
H	+	+	+	Ŧ	+	+	-	-	-	-	-			-	_	_						-	1	1	1	+	1	_		_	-	-	<u> </u>	L	-	-	+	1	1	1	H	+	+	+	<u> </u>	<del> </del>	$\frac{1}{1}$	+	+	3		12		_	MENT	L	┝	<u>  .</u>		<u>.</u>  -	- 5	1	-	+	+	لــــ
																												_									2	3/2	818	2	12	3 2	3 2	3 2	5 5	318	3 2	3 2			1 1	Dose	ΨI		REATMENT CONDITIONS				Femc Cino	2	aguran.	ID Cooniant	-to attack			
																																						z	z	z	2	2	  - 	٤	2	٠	2	z		(NILA)	adjusted?	Acid	alion Cond		ONS				_	2	f	- 1				
l	1																					1			Ì										-		T	Ì		Ī	İ	Ì	İ	†	İ	İ	Ť	T		(N/A)	adjusta	Base	tions				T		25	NZ(SCI)S	Emusos reputado	d Community	Ť	İ	T	T
H	+	+	1	+	1	+	<u> </u>	L		-	-	<u> </u> 	-	L		H				-	-	1	+	+	+	+	-	_	_	_	_	<u> </u>	L		H	-	$\vdash$	-	<u> </u>		$\vdash$	-	1	1	+	+	$\frac{1}{1}$	ł		- 1						L	╀	L	<u> </u>	+	╀	+	Ť	1	t	H
Ц	1	1	1	1	1	L				L		_									-			1	1			_			_					L	9	0	704	100	6 69	9	100	3	2		100	100	1	9	포	ģ					L		100	9	S		1	-	1	
																																					19.0		17.7	177	17.2				1		1	192		C GPD	temp.	Coag.														
0.9	210			3.05	200	0.9				9	0.9	9	12		22	2.6	2.2	26	16	0,7	27	-7	0	27	17		0	7.7	_	0.7	•	3.6	21	16					0		ĺ									(mg/L)	dosa	Bzons														
0 19	5 5	3		2	02	0	0	0.2		0	9		0.2	0.2	9.0	12	90	_	0.7	ام		2			9	0,0	02	=	0.2	0 1		1.3					T	1	1	Ī							T	0.7		[mg/L	residua	Ozone	oz.					Ī	T	T	T	T	T		Ī	
9 12	1	1	1	1							П							1	١	-	1	T	1	Ţ	1	1	1																						-	(min) ()	I ima	Contac	malion Co			-		-	-	-	+	t	T		$\dagger$	
H	+	+				1,1		6	on.	-	6	6	6	5				5		+				+			5			6	_		6			-		Γ	Ī	Γ	Γ	Γ	Ī	T	Ī	T	Ī		-	-	모	:t Ozon	nditions			-	-			-	-	+	$\frac{1}{1}$	-	t	
10.1				7.05	Γ													5 98 19 3		7	5.99		20	-	T	T	T		1				6 56 21 5			L		İ			l		1					5 4 19 2	-	(deg. C)		•			<u> </u>	ŀ	-	_		-	<del> </del>	1	+	+	-	H

Utility ID:		r 1	<u> </u>		SCVWD			(ACWD, C	CWD, EB	MUD, MV	VO, SC	WO)		Γ	T	T				,													_ ¬
						<u> </u>																											
i, Study IO;				P	lot Study	r		(Operaza	lion Study I	9/95, etc.				<b> </b> -		<del> </del>																	
2. Source wat	ter:		South E	ay Aquad	luci - San	Luis Res	ervoir	(River, lak	e, groundw	ater, elc	)																						
3. Source wat	ter ID:		Sta	e and Fe	derai Wa	ar Projec	35	(State Pro	jeci water,	blend of	etc	<u> </u>		<b> </b> -																			
					T																												
5. Describe le (indicate with		ty:	×	Bench-s Pilot-sca					, "Filt." rel , Nocculati																								
Inicicata Mith	*** ^;			Full-scal			filtratio		, noccuian	1	Harita	1011, 20	i'—																				
								L	I																								
6. Indicate W	NU NU Y. N	data report	90 33 FM					nd filtratio		-x-						<del> </del>																	
WATER OL	JALITY D	ATA: PR	-OZONI	Ē																												_	
Date	Time		TOC	<u> </u>	<del> </del> -	UV-254		<b>}</b>	Alkalinity	<del></del>		ardnes	<u> </u>		Bromide	L	<del> </del>	Ammoni			Chloride	L		TDS			Turbidity			-11			opera
			(mg/L)			(1/cm)		(mg	/L as CaC		(mg/	as Ca	CO3)		(µg/L)		(m	g NH3-N	I/L)		mg CIAL	)		(mg/L)			(NTU)	<u>'</u>		_ <u>pH</u> ()		- (	deg.
		Raw	Ozon.	Filt.	Raw	Ozon.	File.	Raw	Ozon.	FIN.	Fi aw	Total	E110	Raw	Ozon,	Fin.	Raw	Ozon.	Fitt.	Raw	Ozan.	FHI.	Raw	Ozon.	Filt.	Raw	Ozon.	Fift.	Raw	Ozon.	Filt. F	Raw	Ozon
					-						1147	9191	1111														ļ						
5/11/93 5/18/93		3.51 3.58		2.13	<u> </u>			68		48	110 105		108	0 17		0.16							236 234		220	11		0 05	78 78	7.8	6 64	20	20
5/25/93		5 88		2.97				79		52	130		131	0 23		0.10							270		220 292		<b> </b>	0 05	68	7.8 8.8	6.66	21 18.7	18.1
11/17/93		3 05 3 44		2.06 1.91			0 029	62 64		59 53	105		105	0 22		0 23				71			238		262	10 13		0.074	7.42		7.88	16 4	
1/5/94		3 27		1 83			0 030	69		-33	102		102	0.23 0.89	<del> </del>	0 14							235 236		223 243	2.45		0.17	7.48			13 5 12 8	
1/5/94		3 27		1.09			0.018	69		56	102			0 89		0 68							236		243	2 48		0 085	7 48		6.61	12 8	
2/15/94 3/1/94		4 82 5 57	ļ	2 05 2.46			0.033	83 70		42	115		115 113	0 16		0.12							219		248	7 37 9 68		0 134	7.59	7.02		12.5	12.5
3/14/94		3.09		1,49	0.114		0 018	70		53	107		107	0.2		0 14							243		250	1 429		0.083	7.28	7.23	8.43	12 9	14 3
4/25/94		4.6		2.19			0 027	81 81		59 51	124		124	0.55	0 55	0 37				70 70			272		283 285	5.94 5.94		0 047	7.87	7.18 7.16		16 9	17
5/16/94		3 97		2.1	0.142		0 028	95		75	129		129	0.45	0 48	0 32				50			241		247	5.57		0 071	8 04	7 85		16 2	17 2
5/16/94		3.97		1.79	0.142		0.023	95		7	129		129	0.45	0 45	0 24				50			241		248	5 5 7		0 069	8 04	7.85	6.8	16 2	17 2
	Bromate	Data																														-	
5/11/93		3.51		2.13				68			110			170		160							236			11		0.05	7.8	20	7.87	20	
5/13/93 5/18/93		4.17 3.58		1.85	0.028			70 52	<b> </b>		113		108	170		160							241 234		220	11 10		0.06	7.8	20 21	6 3 6 55	20	
5/19/93		3.55						63		37	111			160									233			9		0.03	7.3		6 03	22	
5/25/93 5/26/93		5.86 6.56		2.97	0.043			79 70		52 5.3	130		131	230 220		220							270 285		292 298	6		0.1	68	16.1 15.2		18 7	_
8/18/93		2.78			0.136			45	<u> </u>	3.3	45									16			88 6		53	21		D.176	7.4	23 8		22 9	
8/25/93		4.13 2.34			0.128			38			38			170		- 140				32 16			46 B 52.7		68 2	15 13		0 05	73	21.5		23	
9/1/93		2 52			0.128			43		18	48			740		530				16			58 2		68	22 8		0.02	7.47	24 8 23.7		## 23 위-	
10/4/93		3 <u>62</u> 3 <u>56</u>		<del> </del>	0.107			87		54	105		110	200 580		180 540		05		30 31			168 173		184 186	7,18		0.069	7.74	20	6.34	19	
10/7/93		3.48			0.102			93		50	102	<b>-</b>	102	460		0 46		0.5		33			177		197	7.2 9.79		0.052	7.94	18 8		18.2	-1
10/12/93		3.87 3.05		2.06	0 108			96 52		22 69	116		116	250 220		250 230		0.5		32			178		204	5.42		0.963	7.8	18 6		18.5	
12/6/93		3.27		1.95	0.115			58		55	103		103			160				69			238 244		262 252	10.13 1.6		0.074	7.42	15.8	7.86 1 6.68	16 4	
1/4/94 1/5/94		3 44 3 27		1.91	0.120			69 69		53 47	103		103			140							235		223	2 9		0.17	7.7		87 1	13.5	
1/5/94		3 27	<b></b>	1.09			1	69		56	102		_102	890 890		680	l					<u> </u>	238 236		243 243	2.45 2.48		0.092 0.085	7.48			12 8 12 8	
1/27/94 2/15/94		4.82		2 05	0 215			71		45	112	[	112	200 160		120							241		248	11 07		0 202	7.15	12 3	8 25 1	11 9	
3/1/94	<u> </u>	5.57		2 48	0 262			70		42	113	_	1113			140		- <del></del> -					219 235		248	7.37 9.68		0.134	7.59	12.5		12 5	
3/14/94		3.09		1.49				70		53	107		107	200		140							243		250	1.429		0 083	7 28	14 3	6.43	129	
4/25/94	<b> </b>	4.5		1.39		<del> </del>		81	<del> </del>	59 51	124		124	550 550	550 550	370				70 70			272 272		283 286	5 94 5 94		0 047	7 87	17 17		16.9	
4/27/94		4 87			0.168			82		58	127		127	530	540	430				73			274		287	7.97		0.058	7 84	16 9	6 77 1	17 1	
4/27/94		4 67			0 168			82 81	<b> </b>	58 57	127 126		127	630 550	540 550					73 74			274 280		290 291	7 97 8 69		0.06	7 84	18 9		17.1	
4/28/94		4.58			0.193			81		61	126		126	550	550	420				74			280		288	8 69		0.08	75	16 4	6.78 6.77	16	
5/2/94 5/2/94		4.56 4.56			0.161			81		63 60	127		127 127	560 560	570 570	570 480				72 72			281		289	5 3 4		0 081	8.13		6 67 1	17 6	
5/16/94		3 97		21	0 142			95		75	129		129	450	460	0 32				50			281		288 247	5 34 5 57		0 089	8.13	17 2		176	
5/16/94		3 97		1.79				95		7	129		129	450	460	0.24				50			241		248	5 57		0.069	8 04	17.2	68 1	16 2	
5/17/94 5/17/94		3.79			0.155			81	<del> </del>	- 61 62	120 120		120	530	560 560					69	·		266 266		- 277 277	4 92		0 042	- 8 71 8 71	18 3		18 5	1
5/19/94		3 86			0.141			85		71	120		120	500						69			261		271	5.4		0 092	8 56	18 7	7 05 1	18 5	_
5/19/94 5/24/94		3 88 3 89			0 141		1	85		70 75	120		120		550	05				89 54			261 238		271 245	5 4 8 84		0 089	8 56 8 12	18 7	6 98 1	16 5	
5/24/94		3 89			0.136			89		75	128		128							54			236		$-\frac{240}{247}$			0.051	- 8 12 8 12	19		16 6	
L		L		<u></u>		J			<u> </u>		ł	L	L			L																	

Utility ID:					1								1	1	<u> </u>	T''						l					T
1. Study ID:																											
						<b> </b>								İ												<u> </u>	
2. Source wa					ļ <u>.</u>				ļ				ļ		<b> </b>	ļ					ļ	ļ		L		ļ	
					ļ								<u> </u>		ļ					<b> </b>		ļ				<u> </u>	
3. Source wa													<b> </b>	<b> </b>	<b> </b>	]		ļ. <b></b>		<u> </u>				L			I
5. Describe I									<b> </b>				ļ		ļ	<del> </del>						<b> </b>			<b> </b> -		Coagulant
(indicate wit					ļ								ļ	<del> </del>	<b> </b>	<b> </b>						<del> </del>				10	Alum
futurare est					<del> </del>	<del>  </del>							<del> </del>		<b>}</b>	<b>}</b>	<b> </b>	11		<b> </b> -	}	<b> </b> -		<del> </del>	<del> </del>	<del> ;</del>	Ferric Chio
					ļ								<del> </del>	<del> </del>	<del> </del>	· <del> </del>		<del>   </del>					<b></b>		<b> </b> -	<del></del>	T CHIC CHAO
I. Indicate w																<del> </del>	<del>                                     </del>				<del></del>		ļ	<del></del>	<del> </del>		
															<b> </b>	·								-			<del>                                     </del>
WATER Q																										TREATME	NT CONDI
													[			ļ						<del> </del>				1	1
Date	TR.		Bromate		<del></del>				!	L	Chlorinati	on conditions		<del></del>	·		1	<del></del>		Disinfe	tion By	-produc	ts		·	1	Coagu
			(µg/L)			HPC					Fi	ltered					1	TTHM		Ι	HAA5		<u> </u>	HAAS		Coagulant	Dose
	Fin.	Raw	Ozon.	Fitt.		FU/mL)		Indicate dis	infectant(s)	Chlorine	Ammonia		ation time	incub.	PH	Residual		(hā\r)			(µg/L)			(µg/L)		1D	
					Raw	Ozon.	Fift.		th an 'X'	dose	dose		h)	temp.		ļ	Raw	Ozon.	FIN.	Raw	Ozon.	Fin.	Raw	Огол.	Filt.	(see above)	
	أيسيسأ							chlorina	chloramine	(mg C12/L)	(mg NH3-N/L)	chlorine	chloramina	(deg. C)	0	(mg CIZ/L)				<u> </u>	<u> </u>	<b> </b>	<b> </b>				
5/11/93			4.1				13851	<del>-</del>	X	2.5 2.5	0 67	0 083 0 083	168	20.25	6 94		<b> </b>		19	<u> </u>	<u> </u>	21.01		<b> </b> -	40.01		20
5/18/93 5/25/93	22 2		16 3 18.7	13.5 13.3	<del> </del> -	<b> </b>	192 5700	X	×	2.5	0.70	0 083	168	20-25 20-25	5 84 6 4	2 07	I		16	<b></b>		11.07			20.07 34.1	2 2	20 30
11/17/93	17.8			13.7	<b> </b>	1	3,00	<del></del>	<del></del>		0.00	0.000		20-25						<del> </del>	<del> </del>	10.1			33.1	2	30
1/4/94				5,8	l		1400	<del></del>	<del>- x</del>		0.33	0 083	168	20.25	8.7	<u>-</u>			<u>.</u>		<del> </del>					1-2	25 15
1/5/94	15.5			14 5			15390	×	×		0.33	0 083	168	20-25	6.8				56 5			57.5			114	2	<u>`</u>
1/5/94	15.5			14.4			14250	X	×		0 33	0 083	158	20-25	6.7	1			38.5			39 5			78	2	
2/15/94	اببا	ļ	2.4	5 3	820		5700	X	X	2	0.50	0 083	168	20-25	6 3				23			24.5			47.5	2	30
3/1/94	18.7		2	2.4 6.8	2100		1900 4200	X	X	2	0.78 0.53	280 Q 280 Q	168	20.25	6 48 8 43	2.35	L	L	23			25.35			48.35	2	40
3/14/94 4/25/94	20.2 17.8	\	7.5 10.5	9.64	81		860	- <del>x</del>	- <del>x</del> -		0 52	0.083	155	20-25 20-25	6 59		ļ		21 46			22 6 47 55			43.6 93.55	2 2	26 21.5
4/25/94			10.5	6	81		3100	x	<del></del>		0 43	0 083		20-25	6 53				30	<del> </del>		31.3			61.3	2	21.5
5/16/94	18 7		18 5	13 6			1900	X	<del>-</del> x		0.51	0 083	168	20.25	6 85		<del>                                     </del>	1	37	ļ		38 52			75 52		21
5/18/94	18.2		18 5	7.1	1500		2400	X	×	2	0 52	0.083	168	20-25	6.8	1.55			32			33 55			85 55	2	21
																	1									·	
5/11/93			4.1	5.3																						2	20
5/13/93	20		12.1																							2	20
5/18/93 5/19/93	22 2		16 3 20	13.5										ļ						<b> </b>						2	20 20
5/25/93	22.9		18.7	13.3	<b></b>								<del> </del>	<del></del>		·					<b> </b>					2	30
5/26/93	17.3		16						i				<del> </del>					<u> </u>		ļ							5.3
8/18/93	24 9			1		-							<del></del>			}											20
8/25/93				4.2																						2	10
8/25/93				3.8																						2	20 10 10
9/1/93				13 8		ļ							ļ			ļ				<u> </u>						2	20
10/4/93				2.4 11.1	<b></b>					ļi			ļ		<b> </b>	<del> </del>	<b> </b>				<b> </b> -					2	20
10/7/93	20.9			12											<del> </del>	<del> </del>				<del> </del>				<u> </u>			20 20 20 20 25
10/12/93	20.7	<b></b>		<u>'</u> ;	l	1							<del> </del>		l	<del> </del>										- 2	20
11/17/93	17.8			13,7					l					† <del></del>		1	1			1	<del> </del>	· ·				2	25
12/6/93	17.4			69.7																						2	15
1/4/94	18.1			5.8		L									ļ											2	15
1/5/94	15.5		ļ	14 5		ļ		ļ		ļ			<u> </u>	\	<b> </b>	<b> </b>					ļ					2	
1/5/94	15.5 15			14.4	<del> </del>	<b> </b>	ļ	ļ					ļ		<del> </del>	I				<u> </u>	<b> </b>	<u> </u>		<b></b>		2	<u> </u>
2/15/94	13	<del> </del>	2.4	5.3	<b> </b>	1		<b></b>	<del> </del>				<del> </del>	<del> </del>		<del> </del>								<u> </u>			25 30
3/1/94	167		2	2.4		1			<u> </u>						<b> </b>	<del> </del>	1	<del>  </del>									
3/14/94	20 2		7.5										l		I	1	1									2	40 26
4/25/94	17.6		10.5																							2	21 5
4/25/94	17.5		10.5	6																						2	21 5 21
4/27/94	18.3		6.6	- 8 9		<b> </b>		ļ																		2	21
4/27/94	18.4	<del></del>	6.6 7.6	6.2	<del></del>				<del></del>				ļ			ļ				ļ						2	21
4/28/94	18.1	<b> </b>	7.5	33	<del> </del>	<del>  </del>		<del></del>	<b> </b>					<del> </del> -	<del></del>	<del> </del>		<del>  </del>							<del></del>	2	21 22 22 22 22
5/2/94	18 8		5.4				<b></b>	<del> </del>					<del> </del>	<del> </del>		<del> </del>	<del> </del>			<b> </b>							
5/2/94	187		5.4	2		1														l							22
5/16/94	18.7		18 5	13 6																						2	21
5/18/94	18.2		18.5	7.1																						2	21
5/17/04	195	ļ	6.3	4.3			ļ	l								<u> </u>										2	21
5/17/94	19.5		63			<b></b>	<b> </b>	<u> </u>	<u> </u>	ļi		ļ		<b> </b>	<b> </b>	ļ	<b></b>			<b> </b>	ļ	<u> </u>				2	21
5/19/94 5/19/94	19.7		20.4			1		<del> </del>	<del> </del>					ļ	<b> </b>		<b> </b>			<b> </b>	<b> </b> -					2	21
5/24/94			73		<del> </del>	<b> </b>		<del> </del>	<del> </del>			·	<del></del>	<del> </del>		<del> </del>				<del> </del>	├—					- 2	21 25
5/24/94	20 5		7.3	3.1		1		l		l					l	\ <del></del>	<b> </b>	ŀl		<b></b>							25 25
l		1				1			1	<u> </u>				1				1		<del> </del>						<del> </del>	
						*****						<del></del>												L'		t	

•
6
•
8
ä

National Columnia   Columnia	Steady ID.	_							
Chemical formula   Units   Units   Units									
Chenical formula   Units   Chenical formula   Units   Chenical formula   Units   Chenical formula   Units   Chenical formula   Units   Chenical formula   Units   Chenical formula   Units   Chenical formula   Chenical for									
Control   Cont									
Fed3   mgt	<u>ن</u> ن	nical formula	Units						
FeCLS		(D(SO4)3	тол						
Note		200	100						
Main   Main									
Marchellons	NON								
Acid   Base   Cong.	3	1					o Cole	- International	
Colorador   Colorado   Colorado   Colorador   Colora	Acid	Base	Coag.	Cosa	Ozone	Ozone	Contac	Ozone	Ozone
(MA)         (I)         (deg.C)         (mgL)         (mgL)         (min)         ()         (deg.C)           (A)         222         4         0.51         12.2         7.7         1.2         7.7         1.2	adjuste		$\sqcup$	temp.	asop	residual	time	H	temp.
Columbia   Columbia	S.			90.0	(mg/L)	(mb/r)		9	deg. C
6.72         2.2         4         0.52         1.0         1.2.4         7.6           7.68         17.7         3         0.43         18.24         1.6         1.2.4         1			984	Ģ.	3	0.43		7.8	~
7.00			6.73	22		0.52	1	7.8	2
7.15						0.71		9	18.
6.76			2			0.43	. 1		
6.72         14.4         1.6         0.36         12.24         7.05           6.3         12.7         3.1         12.4         7.15         0.36         12.24         7.15           6.5         17.3         3.5         0.40         12.24         7.16         7.16           6.6         17.3         3.5         0.40         12.24         7.16         7.16           6.6         17.3         3.5         0.40         12.24         7.16         7.16           7         17.5         2.5         0.4         12.24         7.16         7.16           8.6         17.2         2.5         0.4         12.24         7.56         7.16           8.7         17.5         2.5         0.4         12.24         7.56         7.16			67.13			0.15	- 1		
6.5 (17.3 ) 3.5 (12.4 ) 7.02 (12.4 ) 7.15 (1			0.70		•	90.0	200		
6.56         16.2         2.4         0.46         12.24         7.15           6.61         17.3         3.5         0.57         12.24         7.16           6.62         17.3         3.5         0.57         12.24         7.16           7         17.5         2.5         0.4         12.24         7.16           6.62         17.3         3.5         0.57         12.24         7.16           6.72         17.5         2.5         0.4         12.24         7.16           6.72         17.5         2.5         0.4         12.24         7.16           6.72         2.5         0.4         12.24         7.16           6.72         2.5         0.4         12.24         7.16           6.72         2.5         0.4         12.24         7.16           6.72         2.5         0.4         12.24         7.16           6.72         2.6         0.4         12.24         7.16           6.72         2.6         0.4         12.24         7.16           6.72         2.6         0.4         12.24         7.16           6.72         2.6         0.4         12.24		1	21.0			5 5	12.24	7.02	
6.63         15.7         2.3         0.45         12.24         7.23           6.63         17.3         3.5         0.45         12.24         7.16           6.63         17.3         3.5         0.57         12.24         7.16           6.63         17.5         2.5         0.4         12.24         7.16           6.73         2.2         0.4         12.24         7.16           6.73         2.2         0.4         12.24         7.16           6.73         2.2         0.4         12.24         7.16           6.73         2.2         0.4         12.24         7.16           6.74         1.2         2.5         0.4         12.24         7.66           6.75         1.2         2.5         0.4         12.24         7.66           6.76         1.7         1.3         1.2.24         7.56           6.75         1.2         1.3         1.2.24         7.56           6.76         1.7         1.3         1.2.24         7.56           6.78         1.7         1.3         1.2.24         7.56           6.78         1.7         1.7         1.7         1.7			2 2		3.4	0.32	17.74	7 16	
6 63         17.3         3.5         0.57         12.24         7.16           6 65         17.3         3.5         0.57         12.24         7.16           7         7.5         2.5         0.4         12.24         7.16           8 65         17.3         2.5         0.4         12.24         7.16           8 67.3         2.5         0.4         12.24         7.56           8 6.7         2.2         0.4         12.24         7.56           8 6.7         2.2         0.4         12.24         7.56           8 6.7         2.2         0.4         12.24         7.56           8 6.7         1.2         0.4         12.24         7.56           8 6.7         1.2         2.4         0.55         18.3         7.7           8 6.8         1.7         2.6         0.4         12.2         7.7           8 6.8         1.7         2.6         0.4         12.2         0.4           8 6.8         1.7         3.0         0.4         12.2         0.4           8 6.8         1.7         1.3         12.2         0.4           8 6.8         1.7         2.6			3 5		2.6	0.45	12.61	7.23	
Colored   Colo		-	2 2		3.5	0.57	17.24	7.16	-
6.64         17.5         2.5         0.4         17.24         7.65           6.64         19.7         17.5         2.5         0.4         12.24         7.65           6.29         2.5         0.4         12.24         7.65           6.29         2.7         1         0.52         1.8.36         7.6           6.20         2.7         1         0.52         1.8.36         7.6           6.20         2.7         1         0.52         1.8.36         7.6           6.20         2.7         1         0.52         1.8.36         7.6           6.21         2.7         1.1         0.52         1.8.36         7.7           6.22         2.7         1.2         1.2.24         2.6         1.7           6.12         2.7         1.2         1.2.24         2.7         1.7           6.12         1.2         1.2         1.2         1.2         1.2         1.2           6.13         1.2         1.2         1.2         1.2         1.4         1.7         1.2         1.2         1.4         1.7         1.2         1.2         1.4         1.2         1.2         1.2         1.2			2		3.5	0.57	12.24	7 18	
664         19.7         2.5         0.4         12.24         7.65           664         19.7         2.5         0.4         12.24         7.65           6.73         2.7         2.1         0.45         16.36         6.5           6.73         2.2         4         0.55         16.36         6.5           6.73         2.2         4         0.55         16.36         6.5           6.73         2.5         1.7         112.24         8.5         6.5           6.43         2.5         1.2         0.45         16.36         6.5           6.44         2.5         0.75         16.36         6.5         6.6           6.45         2.6         2.9         0.45         16.36         6.7           6.45         19.2         1.3         1.22.4         5.94           6.45         19.2         1.3         1.22.4         6.94           6.45         19.2         1.3         1.22.4         6.94           6.45         19.2         1.3         1.22.4         6.94           6.45         19.2         1.3         1.22.4         6.94           6.45         19.2			1		25	70	12.24	7.85	
6.64         19.7         3         0.43         18.36         7.6           6.29         20         3.1         0.65         18.36         7.6           6.73         2.2         4         0.65         18.36         6.8           6.74         2.2         4         1.3         18.36         6.8           6.04         17.2         6.3         0.71         18.3         6.8           6.04         17.2         6.3         1.2         1.2         6.8           6.14         2.4         2.5         0.4         18.36         6.8           6.27         2.4         2.5         0.4         18.36         6.8           6.28         17.2         2.5         0.4         18.36         6.8           6.36         18.2         1.5         0.3         17.2         6.9           6.36         17.7         3         0.4         17.2         6.9           6.56         17.7         3         0.4         17.2         6.9           6.57         18.7         1.2         0.4         17.2         0.4           6.58         17.7         3         0.4         17.2 <td< td=""><td></td><td></td><td>,</td><td></td><td>2.5</td><td>0</td><td>12.24</td><td>7.85</td><td></td></td<>			,		2.5	0	12.24	7.85	
6.6.4         19.7         3         0.43         18.36         7.5           6.2.9         2.0         3.1         0.63         18.36         7.5           6.2.9         2.0         3.1         0.63         18.36         7.6           6.2.9         2.0         3.1         0.63         18.36         7.6           6.2.9         2.0         4.7         1.2         1.2         7.6           6.2.1         2.2         4.7         1.2         1.2         7.6           6.2.1         2.2         0.45         18.36         7.7         1.6         7.7           6.2.1         2.2         0.45         1.2         1.2         2.4         0.45         1.2									
664         19.7         3         0.43         18.38         7.6           6.79         20         3.1         0.43         18.38         7.6           6.79         20         3.1         0.55         18.36         6.5           6.70         1.2         1.2         1.2         1.2         1.2           6.41         1.2         1.3         1.2.2         1.2         1.2         1.2           6.42         2.4         2.5         0.45         18.36         1.2         1			-				-		
6.29         20         31         0.65         16.36         6.5           6.04         17.2         2.2         4         1.5         16.36         6.8           6.04         17.2         6.5         0.4         18.36         6.8           6.04         17.2         6.5         0.4         18.36         6.8           6.14         2.6         0.4         18.36         6.8         6.8           6.15         1.5         0.3         12.24         6.3         6.3           6.26         1.6         0.3         1.22         5.94         6.3           6.36         1.6         0.4         1.2         6.0         6.0         6.0           6.37         1.6         1.5         0.4         1.22         6.0         6.0           6.36         1.6         1.6         0.3         1.22         6.0 <td< td=""><td></td><td></td><td>78.0</td><td>L</td><td>-</td><td>0.43</td><td>1</td><td></td><td>*</td></td<>			78.0	L	-	0.43	1		*
6.04         22.2         4         0.52         16.36         7.0           6.04         23         4.7         1.3         12.24         6.8           6.05         17.2         6.5         0.45         18.36         7.8           6.05         1.2         0.45         11.2         0.45         18.36         6.8           6.45         2.4         2.5         2.9         0.45         12.24         6.9           6.45         1.2         0.45         1.2         0.45         1.5         0.45           6.45         1.2         2.4         0.46         1.2         0.45         1.5         0.45           6.45         1.2         0.45         1.2         0.46         1.2         0.46         1.2         0.46           6.45         1.6         1.2         0.46         1.2         0.46         1.2         0.46 </td <td></td> <td></td> <td>8.29</td> <td></td> <td></td> <td>0.85</td> <td>1</td> <td></td> <td>×</td>			8.29			0.85	1		×
6 04         23         4.7         1.3         1.2.2         6.8           6 45         17.2         6.5         0.45         16.36         7           5.4         2.6         1.8         0.45         16.36         7           6.4         2.6         2.6         0.45         12.24         5.94           6.4         2.6         2.9         0.45         12.24         5.94           6.4         2.6         2.9         0.45         12.24         5.95           6.45         1.0         1.0         1.2         0.45         0.45           6.45         1.0         1.2         0.24         1.2         0.45           6.45         1.0         1.0         1.2         0.45         0.45           6.57         1.0         1.2         0.2         1.2         0.45         0.45           6.57         1.0         1.1         0.1         1.2         0.1         0.45         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1			6.73			0.52			21
665         172         6.5         0.77         16.36         6.8           5.43         24.5         1.5         0.5         12.24         6.9           5.43         24.5         1.6         0.3         12.24         6.0           6.32         2.6         1.6         0.3         12.24         6.0           6.45         1.6         0.4         1.22         6.0           6.58         1.6         1.5         0.23         1.7           6.57         1.6         1.5         0.23         1.7           6.76         1.7         1.2         0.4         1.2           6.76         1.7         1.0         1.2         0.4           6.76         1.7         1.0         1.2         0.4           6.76         1.7         1.0         1.2         0.4           6.76         1.7         1.0         1.2         0.4           6.76         1.7         1.0         1.2         0.4           6.76         1.7         1.0         1.2         0.4           6.76         1.7         1.2         0.4         1.2           6.76         1.7         1.2			90		4.7				
6465         172         6.5         0.45         18.36         7           5.4         25.6         2.9         0.45         12.24         6.9           4.5         25.6         2.9         0.45         12.24         6.5           6.45         1.5         2.4         0.46         12.24         6.5           6.45         1.9         1.5         0.43         12.24         6.4           6.57         1.6         1.5         0.24         12.24         0.45           6.57         1.6         1.1         1.07         12.24         0.45           6.57         1.6         1.1         1.07         12.24         0.45           6.6         1.7         1.2         0.12         1.2.4         0.45           6.7         1.7         1.4         1.5         0.12         1.2.4         0.12           6.7         1.4         1.5         0.12         1.2.4         1.5         0.12           6.1         1.1         1.2         0.12         1.2.4         1.5         0.12         1.2.4           6.1         1.1         1.2         0.1         1.2.2         0.1         1.2.2         <							П		
5.4         2.6         1.9         0.45         5.84           6.42         2.6         2.9         0.45         12.24         5.94           4.21         2.61         2.9         0.45         12.24         5.95           6.45         1.6         1.5         0.24         12.24         5.05           6.45         1.6         1.5         0.24         12.24         6.45           6.45         1.6         1.5         0.24         12.24         6.01           6.52         1.6         1.1         0.7         12.24         6.01           7.15         1.4         1.5         0.12         12.24         6.01           6.6         1.7         1.2         0.12         12.24         6.01           6.72         1.4         1.5         0.12         12.24         7.06           6.72         1.4         1.5         0.1         12.24         7.16           6.10         1.7         1.2         0.4         12.24         7.16           6.10         1.1         0.1         0.1         1.2         7.16           6.10         1.1         0.1         0.1         1.2         <			6.65						
5.4         2.5         2.9         0.45         12.2         6.0           6.32         2.6         1.5         1.22         6.0           6.43         1.5         0.4         1.22         6.0           6.44         1.6         0.4         1.2         0.4           6.54         1.6         1.5         0.2         1.2         0.0           5.57         1.8         1.1         1.0         1.2         0.0           6.16         1.7         3         0.43         1.2.2         0.0           7.6         1.7         3         0.43         1.2.2         0.0           6.18         1.7         3         0.43         1.2.2         0.0           6.18         1.7         3         0.43         1.2.2         0.0           6.18         1.7         4         1.6         0.4         1.2.2         0.0           6.18         1.7         4.2         0.4         1.2.2         7.0           6.18         1.7         3         0.4         1.2.2         7.0           6.18         1.7         4.2         0.4         1.2.2         7.0           6.23			5.43						
12   12   12   12   12   12   12   12			5.4						
6.55 192 15 0.24 1224 0.44  6.56 192 15 0.24 1224 0.69  5.52 192 12 0.12 1224 0.99  7.15 145 15 0.29 1224 0.99  7.15 145 15 0.99  7.16 145 15 0.99  7.17 142 15 0.16 1224 0.99  6.18 142 15 0.10 1224 0.99  6.19 12.1 0.10 12.24 7.16  6.10 12.1 0.10 12.24 7.16  6.10 12.1 0.10 12.24 7.10  6.10 1			4.21		ŀ		١		
6.45         196         15         0.23         12.24         0.45           5.57         19.6         11         107         12.26         6.09           5.57         19.6         11         107         12.26         6.09           7.66         17.7         3         0.43         12.24         7.50           7.16         17.7         3         0.43         12.24         7.50           6.18         17.7         1.6         1.6         1.22.4         7.50           6.18         1.15         1.6         1.2.2         7.16           6.18         1.15         1.2         0.47         1.2.2         7.16           6.18         1.15         1.2         0.47         1.2.2         7.16           6.18         1.15         1.2         0.47         1.2.2         7.16           6.18         1.17         3         0.40         1.2.2         7.16           6.18         1.17         3         0.45         1.2.2         7.10           6.19         1.17         4.85         0.5         1.2.2         7.10           6.10         1.17         4.85         0.5         1.2.2 <td></td> <td></td> <td>6.32</td> <td></td> <td>Ì</td> <td></td> <td>- (</td> <td></td> <td></td>			6.32		Ì		- (		
6.57         18.2         1.5         10.3         18.30         7.04           5.57         18.9         1.1         10.7         12.24         6.0           7.16         17.7         3         1.2.9         6.0           7.16         17.7         3         1.2.4         7.56           7.17         14.5         1.5         1.2.4         7.56           6.18         17.2         1.2         0.16         12.24         7.56           6.18         1.2         1.2         0.16         12.24         7.56           6.18         1.3         2.3         0.36         12.24         7.16           6.18         1.3         3.2         0.36         12.24         7.16           6.20         1.7         3.2         0.36         12.24         7.16           6.20         1.7         3.5         0.57         12.24         7.37           6.21         1.7         3.5         0.57         12.24         7.37           6.22         1.7         3.5         0.57         12.24         7.37           6.22         1.7         3.5         0.57         12.24         7.37			6.45		ĺ		- 1		
5.57         19.8         3.1         1.0         12.24         6.8           7.6         17.7         3         0.43         12.24         6.8           7.15         14.5         1.5         0.43         12.24         7.36           6.76         14.2         1.6         0.43         12.24         7.36           6.77         14.2         1.6         0.43         12.24         7.36           6.78         1.4         1.8         0.43         12.24         7.36           6.78         1.4         1.8         0.47         12.24         7.16           6.3         1.2         1.4         0.36         12.24         7.16           6.3         1.2         3.1         0.48         12.24         7.16           6.3         1.7         3.2         0.47         12.24         7.16           6.3         1.7         3.5         0.57         12.24         7.16           6.3         1.7         3.5         0.57         12.24         7.63           6.5         1.7         3.5         0.57         12.24         7.63           6.6         1.7         3.5         0.5			S						
7.502   174   1.4   1.2   1.2   4   1.5			5.57				1		
1,10   1,10   1,24		1	3.02						
7.15			8						
6.78 14.2 1.0 1.0 1.2 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0		+	7.14			1			
6.72 14.4 18 0.36 7.718 7.18 7.18 7.18 7.18 7.18 7.18 7.1			1				1		
6.18 13.4 3.2 0.47 12.24 7.16 6.51 12.7 2.3 0.46 12.22 6.51 15.7 2.3 0.46 12.22 6.53 17.3 3.5 0.57 12.24 7.15 6.63 17.3 3.5 0.57 12.24 7.16 6.63 17.3 3.5 0.57 12.24 7.16 6.63 17.3 3.5 0.57 12.24 7.16 6.65 17.1 4.65 0.5 12.24 7.16 6.65 17.1 2.9 0.27 12.24 7.63 6.65 11.1 2.9 0.27 12.24 7.63 6.65 11.1 2.9 0.27 12.24 7.63 6.65 11.1 2.9 0.27 12.24 7.63 6.65 11.1 2.9 0.27 12.24 7.63 6.65 11.1 2.9 0.27 12.24 7.63 6.65 11.1 2.9 0.27 12.24 7.63 6.65 12.1 2.2 0.2 12.24 7.63 6.65 12.1 2.2 0.2 12.24 7.63 6.65 12.1 2.2 0.2 12.24 7.63 6.65 12.1 2.2 0.2 12.24 7.63 6.65 12.1 2.2 0.2 12.24 7.63 6.65 12.1 2.2 0.2 12.24 7.63 6.65 12.1 2.2 0.2 12.24 7.63 6.65 12.1 2.2 0.2 12.24 7.63 6.65 12.1 2.2 0.2 12.24 7.63 6.65 12.2 0.2 12.2 12.2 12.2 1.2 1.2 1.2 1.2 1.2 1.		-	6,73		-	Ar. C	1		
6.3 12.7 3.1 0.32 7.7 7.02 7.02 7.02 6.3 1.5 7.03 0.4 1.5 7.5 7.03 0.4 1.5 7.5 7.5 7.03 0.4 1.5			8.18		*	0.47	13		
6.36   15.2   3.4   0.46   12.24   7.15     6.51   15.7   2.3   0.57   12.24   7.23     6.52   7.13   3.5   0.57   12.24   7.15     6.52   7.13   3.5   0.57   12.24   7.15     6.52   7.13   4.85   0.5   12.24   7.37     6.53   7.13   0.62   12.24   7.37     6.54   7.13   0.62   12.24   7.37     6.55   15.1   2.9   0.27   12.24   7.53     6.55   15.1   2.9   0.27   12.24   7.55     7.15   7.15   7.15   7.15   7.15     7.15   7.15   7.15   7.15   7.15     7.15   7.15   7.15   7.15   7.15     7.15   7.15   7.15   7.15     7.15   7.15   7.15   7.15     7.15   7.15   7.15   7.15     7.15   7.15   7.15   7.15     7.15   7.15   7.15   7.15     7.15   7.15   7.15   7.15     7.15   7.15   7.15   7.15     7.15   7.15   7.15   7.15     7.15   7.15   7.15   7.15     7.15   7.15   7.15   7.15     7.15   7.15   7.15   7.15     7.15   7.15   7.15   7.15     7.15   7.15   7.15   7.15     7.15   7.15   7.15   7.15     7.15   7.15   7.15   7.15     7.15   7.15   7.15   7.15     7.15   7.15   7.15   7.15     7.15   7.15   7.15   7.15     7.15   7.15   7.15						933			l
6 51   157   2.3   0.45   12.24   7.23     6 63   17.3   3.5   0.57   12.24   7.16     6 63   17.3   3.5   0.57   12.24   7.16     6 64   17.1   4.85   0.5   12.24   7.16     6 65   17.1   4.85   0.5   12.24   7.10     6 65   17.1   3   0.62   12.24   7.63     6 65   17.1   2.9   0.27   12.24   7.63     6 65   151   2.9   0.27   12.24   7.63     7   17.5   2.5   0.4   12.24   7.65     7   17.5   2.5   0.4   12.24   7.65     8   6 97   2.5   0.38   12.24   8.4     18   6 97   2.5   0.39   12.24   8.4     18   6 97   2.5   0.39   12.24   8.4     18   6 97   2.5   0.39   12.24   8.4     18   6 97   2.5   0.39   12.24   8.4     18   6 97   2.5   0.39   12.24   8.4     18   6 97   2.5   0.27   12.24   8.4     18   6 97   2.5   0.27   12.24   8.4     18   6 97   2.5   0.27   12.24   8.4     18   6 97   2.5   0.27   12.24   8.5     19   10   2.0   0.27   12.24   8.5     10   2.0   2.2   0.27   12.24   8.5     10   2.0   2.2   0.27   12.24   8.5     10   2.0   2.2   0.27   12.24   8.5     10   2.0   2.2   0.27   12.24   8.5     10   2.0   2.2   0.27   12.24   8.5     10   2.0   2.2   0.27   12.24   8.5     10   2.0   2.2   0.27   12.24   8.5     10   2.0   2.2   0.27   12.24   8.5     10   2.0   2.2   0.27   12.24   8.5     10   2.0   2.2   0.27   12.24   8.5     10   2.0   2.2   0.27   12.24   8.5     10   2.0   2.2   0.27   12.24   8.5     10   2.0   2.0   2.2   0.27   12.24   8.5     10   2.0   2.0   2.0   2.0     10   2.0   2.0   2.0		-	6.36		-	870			
0 00 00 00 00 00 00 00 00 00 00 00 00			6.51		2	0.45			
6 60   17.5   5.5   0.57   17.24   7.10     6 82   17.1   4.65   0.5   17.24   7.32     6 82   17.1   4.65   0.5   17.24   7.32     6 85   17   3   0.62   17.24   7.32     6 85   18.1   2.9   0.27   12.24   7.65     7 75   2.5   0.4   12.24   7.65     7 75   2.5   0.4   12.24   7.65     7 8   6.97   2.5   0.4   12.24   7.65     7 10   10   2.5   0.39   12.24   8.4     7 10   10   2.5   0.39   12.24   8.4     7 10   10   2.5   0.27   12.24   8.4     7 10   10   2.5   0.27   12.24   8.4     8 10   10   2.5   0.27   12.24   8.4     8 10   10   2.5   0.27   12.24   8.4     8 10   10   2.5   0.27   12.24   8.4     9 10   9 2 2   0.27   12.24   8.4     9 10   9 2 2   0.27   12.24   8.4     9 10   9 2 2   0.27   12.24   8.4     9 10   9 2 2   0.27   12.24   8.4     9 10   9 2 2   0.27   12.24   8.5     9 10   9 2 2   0.27   12.24   7.5			6.63		F	0.57			
6 8 2   7,1   4 8 5   0.5   12.24   7.32   7.32   6 8 5   17,1   4.8 5   0.5   12.24   7.32   7.32   6 8 5   17,1   4.8 5   0.5   12.24   7.32   7.			Coo		6	0.57			
6 82   17   4 85   0.5   12 24   7 32   6 85   17   3   0.5   12 24   7 32			6.82		*	0.5			2
6 65   17   3 0 052   12.24   7 63   6 65   11.2   12.24   7 63   12.24   7 63   12.24   7 63   12.24   7 63   12.24   7 63   12.24   7 63   12.24   7 63   12.24   7 65			6.82		-	90			2
6.65   17   2.9   0.62   12.24   7.63   6.65   15.14   7.64   7.65   12.24   7.			6.85			0.62			=
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0			6.85	-		0.62			9
6 65   16 1   20   027   12.24   7 85   12.84   12.8		<del> </del>	6.85				1		
17.5   2.5   0.4   12.24   7.85     18.8   6.97   2.5   0.30   12.24   7.85     18.8   6.97   2.5   0.30   12.24   8.4     18.8   6.97   2.5   0.30   12.24   8.35     7.19   19.1   2.6   0.27   12.24   8.35     8.80   19.8   2.2   0.27   12.24   8.35     8.80   19.8   2.2   0.27   12.24   7.5     9.80   19.8   2.2   0.27   12.24   7.5     9.80   19.8   2.2   0.27   12.24   7.5     9.80   19.8   2.2   0.27   12.24   7.5			6.85		2.9		1		
15   1/5   2.5   0.4   12.24   7.65   1.65					2.5				
18.8   6.97   2.5   0.50   12.24   8.4     18.8   6.97   2.5   0.36   12.24   8.4     7.19   19.1   2.6   0.27   12.24   8.35     6.80   19.8   2.2   0.27   12.24   1.5     6.84   19.8   2.2   0.27   12.24   7.5     7.19   7.19   7.2   7.2	L	<u> </u>	_		2.5		-		
16 0 0.57   2.5 0.36 12.24   8.4   1.5			18.8		2.5				l
7 110 161 2 0 0 27 12 2 6 35 15 2 6 35 15 2 6 8 8 15 15 2 6 8 15 15 2 6 8 15 15 2 6 8 15 15 15 15 15 15 15 15 15 15 15 15 15			48.8	L	2.5		ŀ		
7.19 10.1 2.6 0.27 12.24 8.35 6.80 198 2.2 0.27 12.24 7.5 6.86 198 2.2 0.27 12.24 7.5		-	7.10				1		
6 66 19 8 2 2 0 27 12 24 7 5 1 1 2 24 7 5 1 2 2			7 10						
8.86 198 22 0.27 12.24 7.5			20				L		
76.61			2				1		

## 

Drinking water regulations must balance health risks from microbial and chemical contaminants. Chlorination, the traditional method of controlling microbial risks, reacts with naturally occurring matter in water to produce Disinfection By-products (DBPs), which are suspected cancer-causing compounds. Pathogens such as viruses, *Giardia* and *Cryptosporidium* pose acute, short-term gastrointestinal health effects which, in the case of *Cryptosporidium*, can be life-threatening to those with weakened immune systems including infants and the elderly. As depicted in Figure 1, the ability to balance risks from pathogens and DBPs is controlled by a combination of source water quality and practical limitations of treatment technology.

EPA is currently developing parallel regulations for controlling DBPs (Stage 1 and 2 of the DBP Rule) and waterborne disease agents (Interim and Enhanced Surface Water Treatment Rule). Both of these regulations will require most water utilities to implement newer, more expensive treatment technologies. Enhanced coagulation and ozonation are considered best available technologies for complying with these regulations. More advanced treatment technologies such as filtration membranes and granulated activated carbon are extremely expensive and have potential environmental implementation ramifications. Given this, it is important to know the required source water quality which will allow current best available technology to perform within expected future drinking water standards. With the Delta providing the source water for all or a portion of the water supply for two-thirds of the state's population, its quality will be critical in future water treatment management decisions.

Traditional water treatment technology of filtration and disinfection with chlorine was acceptable until regulations requiring a reduction in DBPs forced many entities to begin

C-1

DRAFT 12/18/96

<sup>&</sup>lt;sup>1</sup> Prepared by California Urban Water Agencies

reducing chlorine contact time or use a combination of ammonia and chlorine (chloramines) which reduced DBPs. However, these methods cannot meet expected Stage 1 requirements for *Giardia*, DBPs, and total organic carbon (TOC) removal when using Delta water. Therefore, enhanced coagulation or ozone is required. Although enhanced coagulation, in combination with free chlorine, can control DBPs and *Giardia*, chlorination is ineffective against *Cryptosporidium*. Ozone disinfection is also very effective for controlling *Giardia* while limiting the formation of many DBPs, and can even disinfect for *Cryptosporidium*. However, as greater quantities of ozone are required for disinfection of *Cryptosporidium*, disinfection by-products of the ozonation process occur. Principle among these is the compound bromate, a DBP to be regulated in the DBP rule. Bromate is formed by the reaction of ozone with bromide, with higher levels of either constituent producing more bromate. Delta waters commonly contain bromide, borne by seawater mixing with Delta inflow on the tidal cycle.

Figure 2 depicts increasing Delta water quality constraints as drinking water regulations become more stringent. For example, assuming a 90-percent inactivation of *Giardia* (1 log), the water quality from the Delta would need to be 3.0-4.0 mg/L for Total Organic Carbon and the bromide concentration would have to be in the range of 50-250  $\mu$ g/L, depending upon the treatment technique. As additional disinfection requirements (2-log *Giardia*) are implemented, water quality required to allow ozone to meet these requirements must improve: TOC <3.0 mg/L and bromide <50-150  $\mu$ g/L. Finally, if inactivation of *Cryptosporidium* is required, then ozonation is the only effective option prior to implementation of membranes and GAC and would require a very low bromide concentration (<50  $\mu$ g/L) to comply with the anticipated standard for bromate.

# **Balancing Disinfection and Chemical By-Products**

- **➤** Disinfection
- Giardia
- Viruses
- Cryptosporidium

- ➤ Disinfection By-Products
  - THMs
  - H A As
  - Bromate



- **>**Treatment
  - Chlorination/chloramination
  - Ozonation
  - Enhanced coagulation
  - GAC
  - Membranes
- ➤ Source water quality

### FIGURE 2

# DELTA EXPORT WATER QUALITY AND TREATMENT CONDITIONS REQUIRED TO MEET REGULATORY SCENARIOS

	EXISTI	NG OR PROP	OSED REGUL	ATIONS			
	THMs* (ug/L)	HAAs* (ug/L)	BROMATE (ug/L)	TOC* (mg/L)	DISINFECTION ASSUMPTION	TREATMENT**	DELTA WATER QUALITY CRITERIA
1979 THM Standard	100	None	None	None	None	Chlorination/Chloramination	None
Surface Water Treatment Rule SWTR (1993)	-	-	-	-	0.5 log Giardia	Prechlorinated/Conventional	Br < app. 400 ug/L****
Stage 1 DBP Rule/Interim SWTR (2001-2003)	80	60	5 or 10	up to 50% reduction	0.5 log <i>Giardia</i>	Enhanced Coagulation or Ozonation	not analyzed
Stage 2 DBP Rule/ Enhanced SWTR (2003-2005)	40	30	5	up to 50% reduction	1 log Giardia	Enhanced Coagulation or Ozonation	TOC 3-4 mg/L Br <50-250 ug/L
Stage 2 DBP Rule/ Enhanced SWTR (2003-2005)	40	30	5	up to 50% reduction	2 log Giardia	Enhanced Coagulation or Ozonation	TOC <3 mg/L Br 50-150
Stage 2 DBP Rule/ Enhanced SWTR (2003-2005)	40	30	5	up to 50% reduction	l log Cryptosporidium	Ozonation***	TOC <3.0 mg/L Br <50 ug/L

<sup>\*</sup>THMs = Trihalomethanes, HAAs = Haloacetic acids, TOC = total organic carbon

<sup>\*\*</sup> Treatment assumes conventional filtration for ozone, enhanced coagulation options

<sup>\*\*\*</sup> Assumes ozone at pH 6.5

<sup>\*\*\*\*</sup>Based on results at Metropolitan Water District